

Drainage Strategy & SuDS Statement

DREW SMITH

GROUP



Land at Summer Lane
Pagham
Reserved Matters Application
Planning Update

July 2019

Document Control Sheet

Project name: Land north of Summer Lane, Pagham

Project ref: DSM/E4761

Report Title Drainage Strategy &
SuDS Statement

Doc. ref: TRS/E4761/17424

Date: 25th June 2019

	Name	Position	Signature	Date
Prepared by:	Terry Seymour	Director		June 2019
Reviewed by:	Leon Darrell	Principal Engineer		June 2019
Approved by:	Terry Seymour	Director		June 2019

Revision	Date	Description	Prepared	Approved
1	10/07/2019	Planning Issue	TRS	TRS
2	17/07/2019	Planning Issue	TRS	TRS

Contents

1.0	Introduction	2
2.0	Existing Site	3
	<i>Geotechnical</i>	4
	<i>Ground Conditions</i>	5
	<i>Hydrology</i>	5
	<i>Hydrogeology</i>	6
3.0	Flood Risk and Existing Surface Water Drainage	6
	<i>Existing Site Drainage</i>	6
4.0	Surface Water Management	7
	<i>Design Principles</i>	7
	<i>Sustainable Drainage Systems</i>	7
	<i>Surface Water Drainage Strategy</i>	8
	<i>Flow Control</i>	8
	<i>Water Quality</i>	9
	<i>Long Term Maintenance</i>	12
	<i>Exceedance</i>	12
5.0	Foul Drainage	13
6.0	Conclusion	13

Figures

Figure 1: Site Location	3
Figure 2: Site Topography	4
Figure 3: Extract of Flood Map from the EA's website	5

Appendices

Appendix A	Topographic Survey
Appendix B	Geotechnical Information (Extract)
Appendix C	Proposed Site Layout
Appendix D	Existing Drainage Regime
Appendix E	Proposed Surface Water Strategy
Appendix F	Micro Drainage Calculations
Appendix G	SuDS Maintenance Strategy

1.0 Introduction

Rogers Cory Partnership Limited have been instructed on behalf of Drew Smith to prepare a Surface Water Drainage Strategy and SuDS Statement to support the Reserved Matters submission associated with the redevelopment of the site referred to as the Land north of Summer Lane, Pagham, West Sussex per the current Outline Planning Notice (P/58/15/OUT).

This report outlines the development of the Surface Water Drainage and SuDS Strategy following on from the Flood Risk Assessment (FRA) produced by MJA Consulting (Report dated March 2015) which formed part of the outline planning submission.

The purpose of this strategy is currently not to seek to discharge the current planning conditions relating to the surface water and SuDS of the Outline Planning Notice (P/58/15/OUT) but rather to support the Reserved Matters application and to demonstrate that a surface water drainage solution can feasibly be delivered to support the detailed layout.

Further details, including detailed hydraulic calculations, detailed drainage layouts and associated drainage construction details will be developed and submitted as part of a separate and future Discharge of Conditions application.

The drainage strategy outlined and presented in this report build on the principles of the following:

- Flood Risk Assessment by MJA Consulting Limited (March 2015);
- Combined Geotechnical and Ground Contamination Risk Assessment by Ashdown Investigation Limited (September 2016);
- Geo-Environmental Report by Ashdown Site Investigation Limited (September 2016)
- Winter Groundwater monitoring Report by Wilson Bailey Geotechnical and Environmental (May 2016);
- BRE 365 Soakaway Testing by Geo-Environmental Limited (January 2019);
- Winter Groundwater Monitoring by Geo- Environmental Limited (June 2019);
- Existing Drainage and CCTV survey by DrainTech (March 2019)

2.0 Existing Site

The site is located north of Pagham, adjacent to Summer Lane (Refer to **Figure 1** below). The development is bounded to the north by an existing ditch and a new residential development, to the east and south by existing residential properties and to the west by existing farm lands

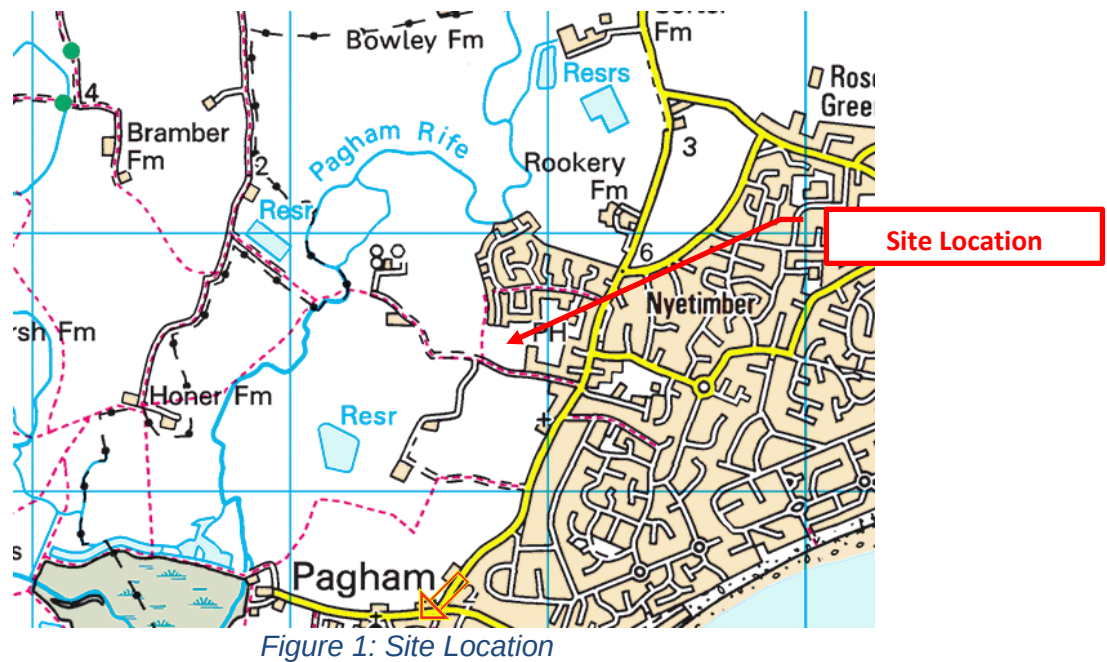


Figure 1: Site Location

The existing site proposed for development covers approximately 3.27ha of greenfield land comprising of open grassed fields. The approximate centre of the site is at Ordnance Survey (OS) Grid Reference 488830; 98552.

The application site generally falls in a westerly direction from the south eastern corner to the north west. An overview of the change in topography in this part of the wider site is presented as **Figure 2** overleaf. A copy of the topographical survey can be found in **Appendix A**.

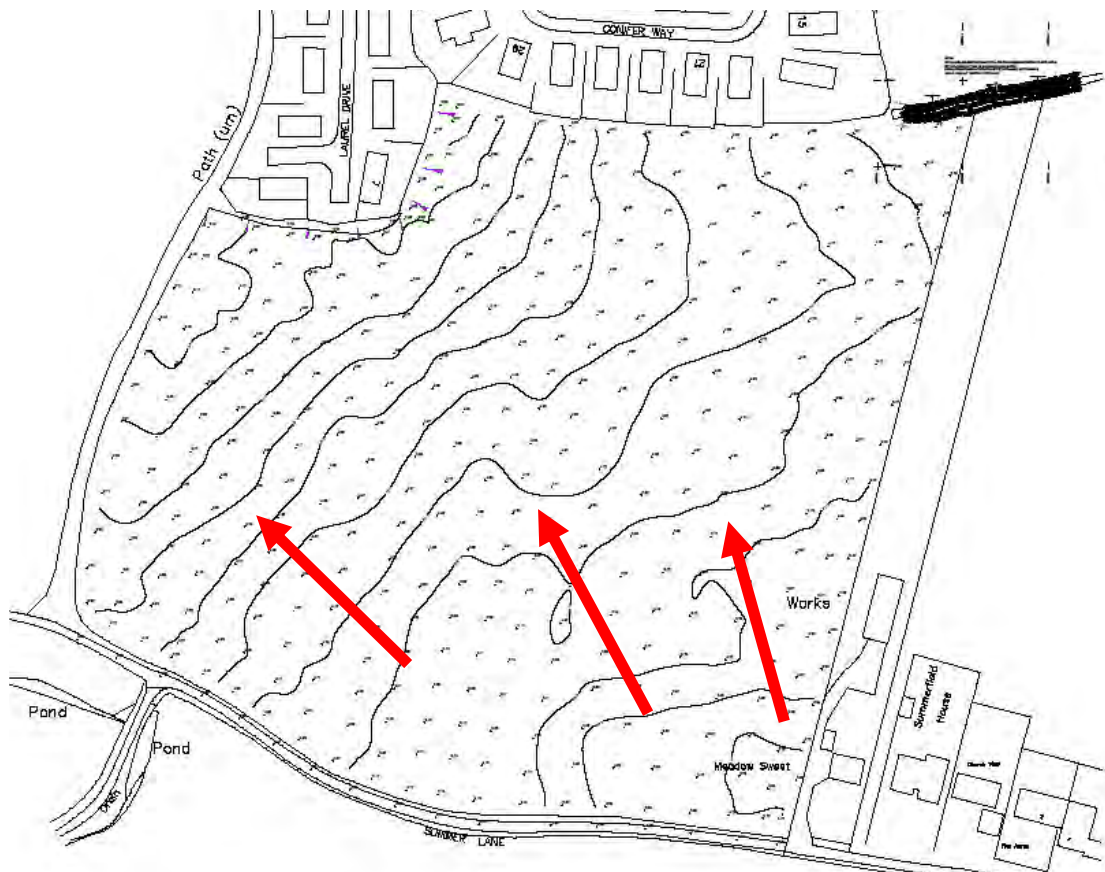


Figure 2: Site Topography

Geotechnical

The current review of the geotechnical aspects of the site are based on the following documents:

- Combined Geotechnical and Ground Contamination Risk Assessment by Ashdown Investigation Limited (September 2016);
- Geo-Environmental Report by Ashdown Site Investigation Limited (September 2016)
- Winter Groundwater monitoring Report by Wilson Bailey Geotechnical and Environmental (May 2016);
- BRE 365 Soakaway Testing by Geo-Environmental Limited (January 2019);
- Winter Groundwater Monitoring by Geo- Environmental Limited (June 2019);

Ground Conditions

BGS geological maps indicate that the site is underlain by the London Clay Formation with River Terrace Deposits superficial deposits.

Intrusive investigations carried out by Ashdown, Wilson Bailey and GESL indicate that the site consists of Topsoil up to 0.3mbgl. MADE GROUND was discovered up to depths of 0.2mbgl at TPO2, TPO4 and TP12 (ref. GESL report), River Deposits (Clay) ranged in depths between 0.1 to 3.0m plus below ground and River Terrace Deposits (Sand) ranged in depth between 1.10m to 3.0m plus below ground. The London Clay Formation was found at depths from 1.90mbgl.

Winter groundwater monitoring indicates the presence of shallow groundwater parts of the site varying from 0.00mbgl to 1.81mbgl. Winter infiltration testing to BRE 365 was carried out and indicated permeability rates ranging from 9.5×10^{-7} to 1.1×10^{-5} m/s.

A copy of the extracts from the GESL Ground investigation report is contained in **Appendix B**.

Hydrology

There is an existing ordinary watercourse which runs along the north western boundary of the site as well as along the south western side of the site.



Figure 3: Extract of Flood Map from the EA's website

Hydrogeology

Groundwater mapping published by the EA indicates that the site is located over a and Unproductive Stratum Bedrock and Secondary A Superficial Deposit designation respectively. The site does not lie within a groundwater source protection.

3.0 Flood Risk and Existing Surface Water Drainage

This report reviews the existing risk of flooding to the site and requirements for a compliant drainage strategy by interrogating the following information:

- Available topographic survey information;
- Arun District Council Strategic Flood Risk Assessment (SFRA);
- West Sussex LLFA Policy for the Management of Surface Water;
- Available mapping from the Environment Agency's website;
- Existing Southern Water sewer service records;
- MJA Consulting Limited Flood Risk Assessment (March 2015);

Based on a review of the EA's Flood Zone maps (see **Figure 3**), the development site appears to lie wholly within Flood Zone 1, considered to be at low risk from fluvial and tidal flooding.

The risk of flooding from pluvial sources has been assessed and based on the mapping information provided by the EA is deemed low for the site. Whilst there is a small localised area highlighted as high risk this is due to a localised low point in the site topography which would allow potential exceedance flows to accumulate. The risk to the future development could be mitigated through consideration of proposed finished levels in relation to these existing low points on the site to ensure such localised surface water flooding will not pose a risk to buildings or people, nor increase the risk of surface water flooding elsewhere.

It should be noted that as from April 2015, the Lead Local Flood Authority (LLFA) has now become a statutory consultee with respects to surface water drainage and risk of flooding from surface water, groundwater, reservoirs and sewers. As such West Sussex County Council (WSCC) and Arun District Council (ADC) will become a primary consultee during the Reserved Matter submission and discharging planning conditions relating to localised flood risk and the surface water drainage strategy.

Existing Site Drainage

A review of the existing topographic information and sewer records has been carried out to assess the existing surface water drainage regime of the site.

The majority of the surface water from fields within the development site appear to drain overland to the existing ditches located on the northern and western extents of the fields.

4.0 Surface Water Management

The surface water management section should ensure that there is no adverse impact on flood risk elsewhere as a result of a change in the surface water runoff regime from the re-development.

Design Principles

Key design principles in the following guidance documents steer the approach to managing surface water runoff at sites:

- Building Regulations hierarchy of drainage (H3);
- Interim Code of Practice for SuDS; and
- CIRIA best practice guidance, including the use of the 'SuDS management train'.

Building Regulations hierarchy of drainage outlines the preferred methods for the disposal of surface water with infiltration methods being the preferred option. If this is not possible the next favoured option is to drain to an existing watercourse. If neither of these options are feasible, the regulations state that rainwater discharge should be directed to a sewer.

The Interim Code of Practice for SuDS provides guidance about the hydraulic design criteria for Sustainable drainage systems. This in general refers to both peak rate of runoff and the volume of runoff, post development. Prior to mitigation measures such as the use of SuDS attenuation features, both the volume and peak rate of runoff may increase post development.

The design principles for surface water management extend beyond simple hydraulic criteria. CIRIA guidance promotes the use of the SuDS management train, a concept where SuDS techniques are used to treat, convey and store surface water runoff. This approach is considered as part of the SuDS selection methodology.

Sustainable Drainage Systems

To drain the development in a sustainable manner whilst complying with the requirements of the NPPF, the scheme should seek to adopt an appropriate form(s) of sustainable urban drainage systems (SuDS).

SuDS techniques comprise of implementation of permeable paving for parking bays and the use of attenuation basins and swales to convey and provide temporary storage of surface water run-off.

Surface Water Drainage Strategy

In view of the requirements of the NPPF, PPG, WSCC and ADC along with the design parameters and constraints associated with redeveloping this site, a surface water drainage strategy design has been devised and hydraulically modelled to demonstrate that the scheme can be suitably implemented without increasing the level of flood risk, when the surface water drainage system experiences a 1:100 year rainfall event (including 40% climate change allowance) and 10% allowance for urban creep

The surface water drainage scheme has been designed to ensure:

- A reduction in the pre development site discharge for peak storm events.
- Sustainable Urban Drainage systems are wholly incorporated within the scheme.
- Consideration is given for the improvement of water quality within the design.
- The designed drainage scheme can satisfactorily retain a critical 1 in 100 Year storm event with climate change.

All new parking bays will be designed as permeable paving to make use of the available infiltration at shallow levels, with an overflow provision to the new surface water network.

Run-off from the access roads and plots will be conveyed to a new below ground surface water drainage network which will direct flows from the eastern parcel of the development, via an existing ditch, which in turn is to be diverted into a new open ditch and swale system located on the western part of the site.

As there is an existing residential development which discharges into the ditch, which runs along the northern boundary of the site, the new swale and ditch system in the western side of the site has been modelled to account for the additional areas from the Crayfern Development to the north. An outline of the above proposal is provided in drawings DSM/E4761/001 in **Appendix E**.

It must be noted that the strategy layout and calculations presented at this stage is to demonstrate that the detailed layout can feasibly be drained in terms of surface water. The full details of the drainage layouts including construction details for permeable paving, swales and attenuation basins will be provided as part of the separate Discharge of Conditions application of the Outline Consent.

Flow Control

The hydraulic models of the proposed surface water network, incorporating the SuDS attenuation basins and flow control devices can be found in **Appendix F**.

The hydraulic calculations have been simulated under various scenarios up to and including the critical 1 in 100 Year storm event with additional 40% allowance for climate change and 10% allowance for urban creep.

Discharge from the site is proposed to be restricted to the Qbar rate of 7.9l/s for all storm events up to and including the 1 in 100 year plus climate change.

The simulations confirm that the storm can be managed and contained within the curtailment of the site, with small volumes of surface flooding, during peak storm events contained at surface in areas of low risk to people or property.

Two sets of calculations have been included in **Appendix F**. The first set demonstrates that the site provided full attenuation for all storm events for all run-off from the new development for all storms up to and including the 1 in 100 year plus 40% event. The second set includes the provision of the additional flows from the Crayfern Development, which activates the overflow provision at the final outfall from the site.

Catchment	Impermeable Development Area (Ha)	Q1 Year (L/sec)	Q30 Year (L/Sec)	Q100 Year Plus Climate (L/Sec)	Discharge Volume (m3) (360min Winter)
1	2.236 (includes 0.41ha)	4.6	7.9	7.9 (plus 5l/s overflow)	256.30

Table 2: Summary of Post Development Run-off with mitigation measures

Water Quality

It is important to address issues with regards to quality when considering surface water management. As part of the surface water is proposed to be discharge to the existing downstream watercourses, treatment is proposed as part of a SuDS Management Train in accordance with the recommendations of the SuDS Manual (CIRIA 753) and as required by the LLFA.

This SuDS management train will be achieved through the use of permeable paving, swales and attenuation basins.

Chapter 26 of the CIRIA SuDS Manual (2015) provides guidance on methods that should be used to design SuDS to meet the water quality design criteria and good practice design standards. Diffuse urban pollution is a significant factor in compromising groundwater and receiving water standards that are required under the EA Water Framework Directive. Chapter 4 of the SuDs Manual summarises factors, which influence pollution levels in urban run-off. This summary is presented in **Table 1 overleaf**:

Factors influencing pollution levels in urban run-off
The amount and type of pollution washed off a surface will depend on many things including: • Planning activities on, above and adjacent to the surface that affect the deposition of pollutants, their retention on the surface and the extent to which they are mixed with runoff (including pollution prevention strategies) • Unplanned activities (accidents and spillages) that can cause temporary unexpected high pollution concentrations • The surface location and type, affecting wash-off rates and contaminant movement mechanisms • The drainage path • The length of the dry weather period before the rainfall event • The intensity and the duration of the rainfall, and the associated flow velocities Any further pollutant transformations occurring during residence and conveyance within gullies, chambers, pipe or channel networks, gravels, soils and vegetation and quiescent bodies of water.

Table 1: Extract of Box 4.1 of the SuDS Manual (CIRIA 753)

Table 4.3 of the SuDS Manual classifies the pollution hazard level for residential sites, including residential car parks, low traffic roads as being “low” and thus only requiring a “Simple index approach” in terms of the requirements for the discharge to surface waters, including coasts and estuaries.

The SuDS Manual summarises the steps for the simple index approach:

Step 1 – *Allocate suitable pollution hazard indices for the proposed land use*

Step 2 – *Select SuDS with a total pollution mitigation index that equals or exceeds the pollution index*

Step 3 – *Where the discharge to a protected surface waters or groundwater, consider the need for a more precautionary approach*

The SuDS Manual describes “protected surface waters” as protected surface water resources, which include those designated for drinking water abstraction or for other environmental protection reasons

Table 26.2 of the SuDS manual notes the following pollution hazard indices for residential land use development:

Land Use	Pollution Hazard Level	Total suspended solids (TSS)	Metals	Hydrocarbons
Residential roofs	Very low	0.2	0.2	0.05
Individual property driveways, residential car parks, low traffic roads (eg. cul-de sacs, home zones and general access roads) and non-residential car parking with infrequent change (eg schools, offices) ie. Less than 300 vehicle movements/day	Low	0.5	0.4	0.4
Commercial yard and delivery areas, non-residential car parking with frequent change (eg hospital, retail), all roads except low traffic roads and trunk roads/ motorways	Medium	0.7	0.6	0.7

Table 2: Extract of Table 26.2 of SuDS Manual (2015)

Table 26.3 of the SuDS Manual provides details of the SuDS pollution mitigation indices for various types of SuDS components

	Mitigation indices		
Type of SuDS component	TSS	Metals	Hydrocarbons
Filter Strip	0.4	0.4	0.5
Filter Drain	0.4	0.4	0.4
Swale	0.5	0.6	0.6
Bioretention system	0.8	0.8	0.8
Permeable Paving	0.7	0.6	0.7
Detention Basin	0.5	0.5	0.6
Pond	0.7	0.7	0.5
Wetland	0.8	0.8	0.8

Table 3: Extract of Table 26.3 of SuDS Manual (2015)

As such the total SuDS mitigation index (figure 5) must be greater than the pollution hazard index (figure 4), furthermore when used in combination of two or more SuDS components, a factor of 0.5 is used to account for the reduced performance of the secondary or tertiary components associated with the already reduced inflow of concentration, therefore:

Total SuDS mitigation index = mitigation index₁ + 0.5 (mitigation index₂)

The use of the permeable paving for parking bays and the combination of the attenuation basins and swales will provide the minimum required level of SuDS mitigation index to the run off from the development.

Long Term Maintenance

Consideration will need to be given to the long-term maintenance of the proposed drainage structures. Permeable paving, swales, attenuation basins and all associated external pipework, chambers and manholes within the demise of each plot ownership boundaries will be the responsibility of the future occupants. Elsewhere, the surface water networks below the access roads and open space will be the responsibility of the Management Company. Details of the Maintenance Plan will be provided as part of the separate Discharge of Conditions application of the Outline Consent.

Exceedance

Whilst the drainage system has been designed to a very high standard (1 in 100 Year storm event including climate change), it is possible that a more extreme event will occur and that the design standard for the system will be exceeded. It is best practice to design the drainage system to shed water, primarily into landscaped and other areas, therefore reducing the risk of flooding areas of built development during extreme events.

A strategy for directing overland flows for the site will be confirmed using overland flow modeling and provided as part of the separate Discharge of Conditions application.

5.0 Foul Drainage

The proposed foul water discharge generated by the site has been calculated at 4.166l/s (based on 90 dwellings at 4000l/dwelling/day) in accordance with Sewers for Adoption 7th Edition.

In accordance with the approved Outline Consent, the foul water drainage will be conveyed via a new below ground foul sewer network through development and onto a new adoptable foul water pumping station to be located in the south western corner of the site. A new rising main will convey the pumped discharge to the Pagham wastewater treatment works (WWTW), located north west of the site. The final connection to the WWTW will be subject to a S98 Agreement with Southern Water.

All domestic foul drainage will be designed in accordance with Part H of the Building Regulations.

6.0 Conclusion

A surface water drainage strategy has been prepared and demonstrates that the development proposal can be successfully implemented and designed to withstand the impact of a 1:100-year rainfall event (including climate change), in accordance with the NPPF, PPG, WSCC and ADC requirements.

In view of this assessment, the report concludes that:

- i. The Development can be drained in a sustainable manner utilizing SuDS techniques;
- ii. The Development will satisfactorily manage and maintain a 1 in 100 Year storm event with an allowance for climate change;
- iii. The detailed drainage strategy generally follows the principles of the approved FRA and Surface Water Drainage Strategy and SuDS Statement;
- iv. The findings of this report identify the opportunity to promote the sustainable re-use of existing resources and potential to implement an appropriate SuDS strategy.

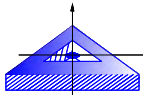
Appendix (A)

Topographic Survey



NOTES:
Coordinates based on OS grid determined from National GPS Network using OSTN02.
Levels based on OS datum determined from National GPS Network using OSGM02.
Detail on properties & road surrounding site produced from OS ProMap
Crown Copyright. All rights reserved. Licence Number 100020449

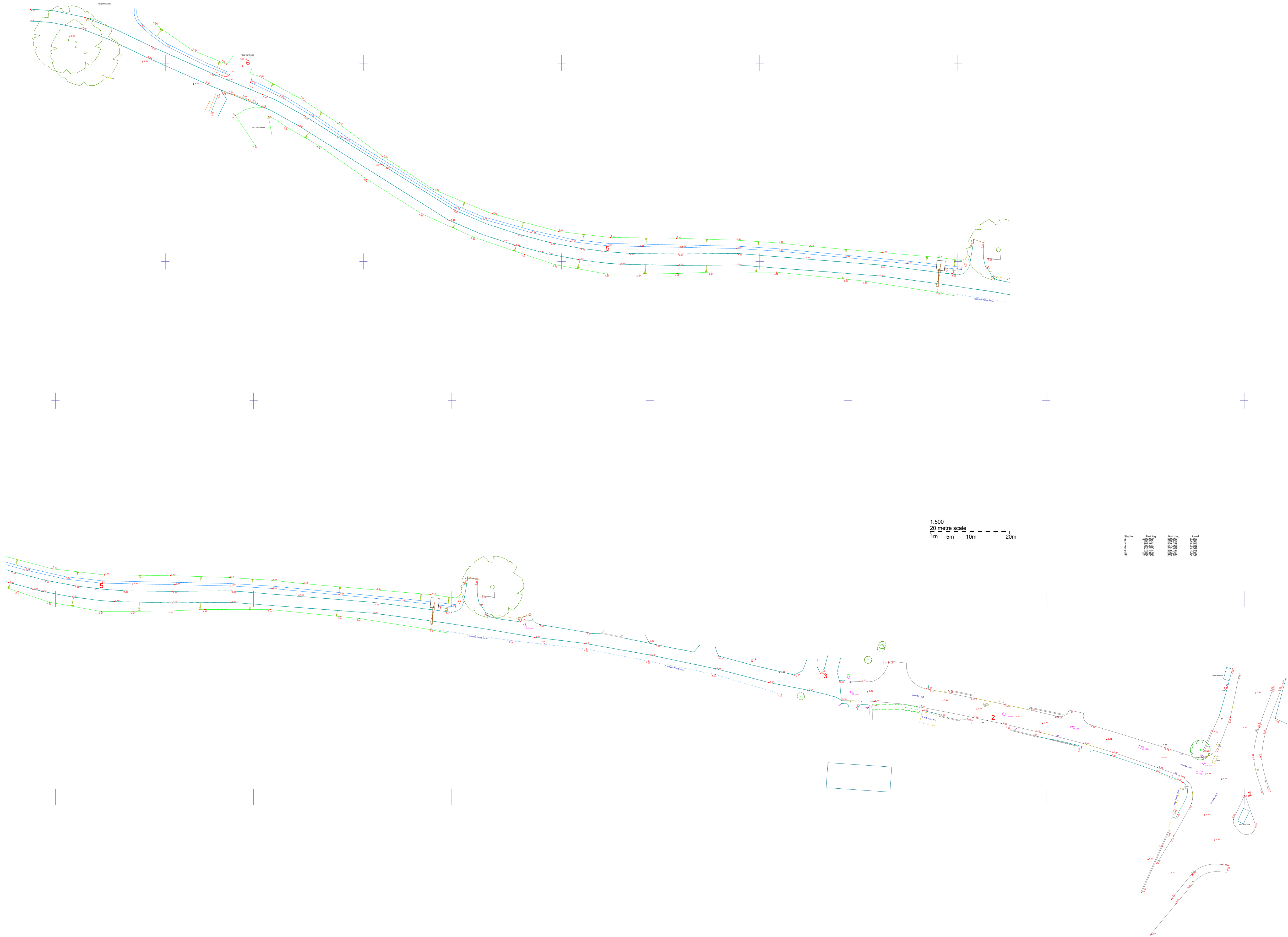
Geomatic Surveys		siteline Unit E, Woodside 34 Parham Drive Eastleigh SO50 4NU t: 023 8081 1081 f: 023 8081 1012 w: siteline.co.uk	
HANBURY PROPERTIES LTD		Client	
LAND NORTH OF SUMMER LANE SUMMER LANE, PAGHAM		Contract	
LEVEL SURVEY		Title	
657PG01		Drawing No.	
JULY 2012		Date	
1:500 (A1)		Scale	
TL		Surveyor	



ADA Solutions Ltd

Land And Measured Building Surveyors

33 Lower Wardown, Petersfield, Hampshire, GU31 4PA
Tel: 01730 266303 Mob: 07775 835531
Email: simon@adasolutionsltd.com



Address :

SUMMER LANE
PAGHAM ROAD
PAGHAM
WEST SUSSEX

Legend

CBF = Closed board fence
CH = Cill to Head height
CLF = Chain-link fence
F-C = Floor to Cill height
F-H = Fire Hydrant
FV = Foul water inspection cover
G = Gully
GV = Gas valve
JB = Junction box
IC = Inspection cover
P&W = Piled and wire fence
SDP = Soil down pipe
SP = Spring height
SV = Silt valve
SW = Storm water inspection cover
TAP = Water tap
TP = Telegraph pole
UTL = Unable to lift (inspection cover)
WM = Water meter

Symbols

⊗ = Floor level
⊕ = Structural ceiling height
⊖ = Suspended ceiling height

Drainage

Drainage details including pipe sizes and run direction between chamber have been taken from surface inspection only, therefore are assumed and cannot be guaranteed.

Survey control information

Survey levels are based on OSMB height of 5.96m (NE face of The Bear

Horizontal control is arbitrary only and referenced to survey station 7 at 500m east and 1000m north and rotated to north.

A 50 metre site grid is in place

GPS/GPRS control:

N/A

This survey has been carried out at an accuracy commensurate with the scale shown on the title block of the drawing. Enlarging the drawing by digital means will not increase the accuracy of the survey. Taking dimensions from the drawing is generally not recommended and measurements for design/construction should be taken from the digital version only.

Client : Langmead Children's Farm Partnership

Date : June 2014 Project : Topographical Survey

Drawing Number : 0614-HP2-T1

Drawn by : SA Checked : SA Scale : At A 1:500

SUMMER LANE - TOPOGRAPHICAL SURVEY

Appendix (B)

Geotechnical Information (Extract)

11th June 2019

Our ref: GE17671/SA01/190611



Daniel O'Shea
Drew Smith Limited
Drew Smith House
Mill Court
The Sawmills
Durley
Southampton
Hampshire
SO32 2EJ

Dear Daniel,

RE: Summer Lane, Pagham, Bognor Regis, PO21 4NQ – Winter Groundwater Monitoring

We are pleased to present the results of the winter groundwater monitoring undertaken at the above site.

Eleven windowless sample boreholes (WS01 to WS11) were drilled on the 11th and 14th January 2019 to allow the installation of monitoring standpipes for winter groundwater level monitoring. Spot monitoring of the groundwater levels within these standpipes was undertaken on eight occasions between 16th January and 25th April 2019. Three additional boreholes (BH03, BH08 and BH10) were drilled on 4th February 2019 immediately adjacent to WS03, WS08 and WS10 and installed with large diameter monitoring standpipes to allow the use of in-situ continuous groundwater dataloggers. Continuous groundwater level dataloggers were installed within BH03, BH08 and BH10 from 5th February to 11th March 2019. The exploratory positions were located in line with instructions from Drew Smith Limited and access constraints at the time of investigation.

The ground conditions revealed within the boreholes are recorded in Geo-Environmental's letter report (GE17671-SA02-190128) which also details the results of the soakage testing previously carried out at the site.

Background

It is understood that the site is proposed to be developed with a residential development and associated infrastructure. As such, winter groundwater monitoring was required to assist in assessing the suitability of underlying soils for drainage via soakaways and to inform the planning, design and construction strategies for the site.

The ground conditions revealed in the exploratory holes at the site comprised River Terrace Deposits of clayey sand and sandy gravelly clay overlying clay soils of the London Clay Formation.

Site Description

At the time of the investigation works the site comprised a section of a large arable field in the west with a grass paddock with areas of trees and scrub in the east. The site appeared generally level. The western field was accessed from the west end of Summer Lane via a gap in the hedgerow. Access to the paddock was afforded by a grass track in the south-eastern corner of the site.

Geo-Environmental Services Ltd
Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL
+44(0)1273 832972 www.gesl.net

Environmental Consultants | Geotechnical Engineers | Site Investigations

Geo-Environmental Services Ltd incorporated in England number 3214980 VAT number 679544479



Groundwater Monitoring

The results of the groundwater spot monitoring are summarised in Table 1.

Location	Minimum depth to groundwater (m bgl)	Maximum depth to groundwater (m bgl)
WS01	0.73	1.12
WS02	0.40	0.93
WS03	0.15	1.02
WS04	0.86	1.11
WS05	0.58	0.95
WS06	0.00	0.80
WS07	0.82	1.81
WS08	0.59	0.89
WS09	0.50	1.17
WS10	0.10	0.55
WS11	0.85	1.36

Table 1 Summary of groundwater depths from spot monitoring (January to April 2019)

The full results of the groundwater spot monitoring are presented within Appendix A.

Continuous groundwater level dataloggers were installed within BH03, BH08 and BH10 from 5th February to 11th March 2019. The results are presented graphically in Appendix B.

The results have been compared against rainfall observations recorded at Thorney Island weather station approximately 20 kilometres north-west of the site. During the monitoring period two periods of high precipitation occurred: a period of wet weather in the days surrounding 7th February where 13mm of rainfall was recorded; and wet weather between 4th March (16mm rainfall) and 10th March (10mm rainfall).

The groundwater levels over the monitoring period show groundwater at a peak during the first rainfall event, then reducing to a relatively steady level before peaking in response to the second rainfall event.

The time taken for the groundwater level in BH03 to recover following the February rainfall event was approximately 14 days with an approximate decrease of 0.40m. The levels in BH08 took approximately 13 days, dropping approximately 0.25m. Within BH10 the fall in water level took approximately 15 days for an approximate 0.30m drop in water level. The response to the March rainfall event starting on 4th March appears to be less than 12 hours for all of the boreholes with increases in water level of approximately 0.50m, 0.25m and 0.25m for BH03, BH08 and BH10 respectively. The data also shows some evidence of the potential tidal effect on groundwater levels with daily variance in levels of up to 0.05m on some occasions.

Conclusions

The monitoring undertaken indicates that the winter groundwater levels at the site are likely to interfere with the effective performance of conventional stormwater soakaways. As a result, on-site storage and attenuation together with alternative storm water disposal options should be considered.

Closure

We trust that we have interpreted your instructions correctly, and please do not hesitate to contact us should you have any queries.

Yours sincerely
For and on Behalf of Geo-Environmental



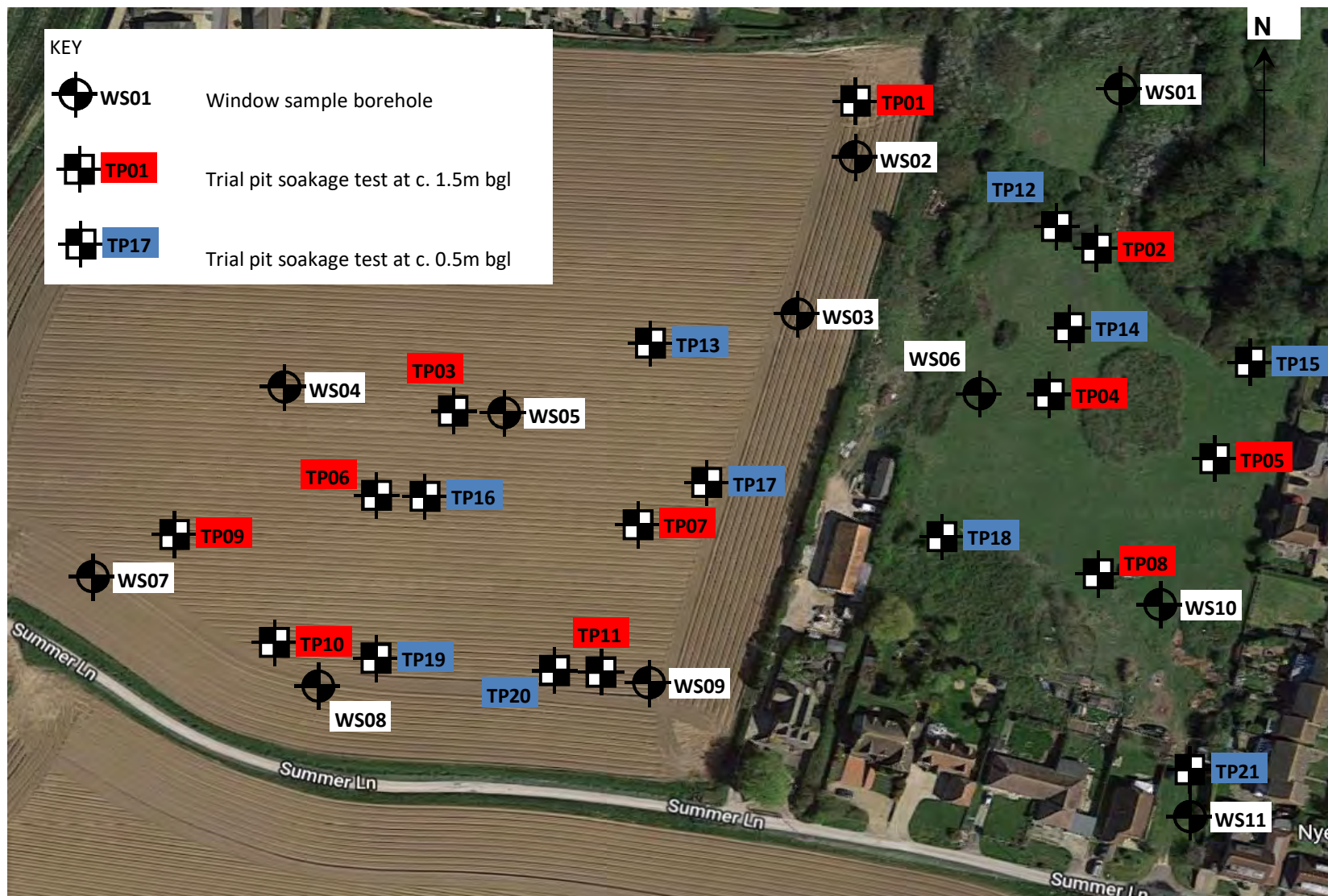
SHAUN ARMITAGE BSc (Hons), FGS
Senior Consulting Engineer
shaun.armitage@gesl.net

Enc	Figure 1	Site Location Plan
	Figure 2	Exploratory Hole Location Plan
	Appendix A	Winter Groundwater Monitoring Results
	Appendix B	Continuous Groundwater Monitoring Results





Project:	Summer Lane, Pagham, Bongor Regis, PO21 4NQ			Title	Site Location Plan	
Client:	Drew Smith Limited			Geo-Environmental Services Ltd Unit 7 Danworth Farm, Cuckfield Road Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net	 Geo-Environmental	
Ref No:	GE17671	Revision:	0			
Drawn:	SA	Date:	07/01/2019			
Figure:	1	Scale:	Not To Scale			



Project:	Summer Lane, Pagham, Bongor Regis, PO21 4NQ			Title	Exploratory Hole Location Plan	
Client:	Drew Smith Limited			Geo-Environmental Services Ltd Unit 7 Danworth Farm, Cuckfield Road Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net	 Geo-Environmental	
Ref No:	GE17671	Revision:	0			
Drawn:	SA	Date:	23/01/2019			
Figure:	2	Scale:	Not To Scale			



APPENDIX A

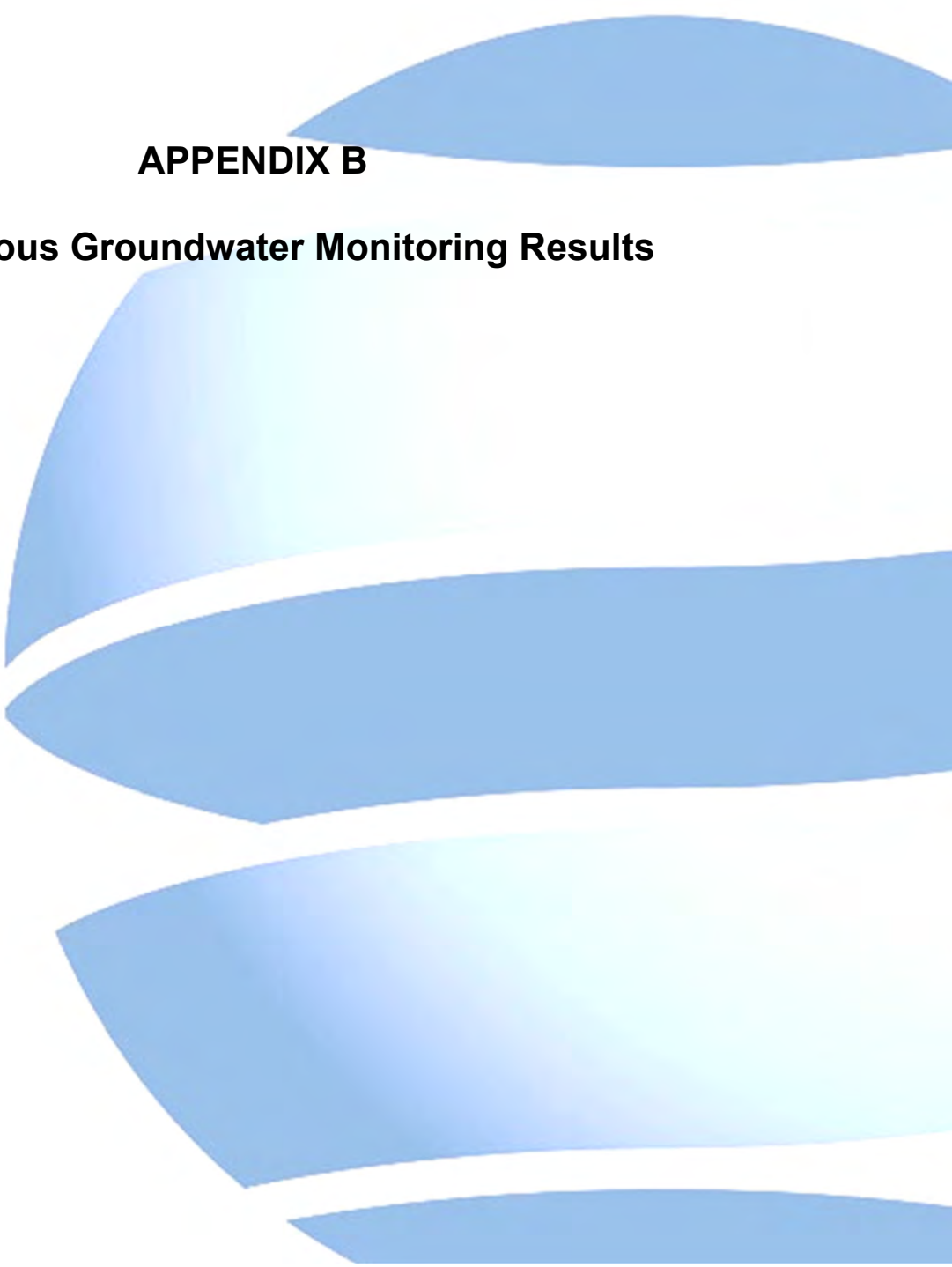
Winter Groundwater Monitoring Results

Project: Summer Lane, Pagham, Bognor Regis,
Ref: GE17671
Client: Drew Smith Limited

Location	Date	GWL (m bgl)
WS01	16/01/19	1.07
WS02	16/01/19	0.80
WS03	16/01/19	0.76
WS04	16/01/19	1.00
WS05	16/01/19	0.88
WS06	16/01/19	0.52
WS07	16/01/19	1.53
WS08	16/01/19	0.83
WS09	16/01/19	0.99
WS10	16/01/19	0.42
WS11	16/01/19	1.32
WS01	04/02/19	0.88
WS02	04/02/19	0.62
WS03	04/02/19	0.42
WS04	04/02/19	0.86
WS05	04/02/19	0.63
WS06	04/02/19	0.32
WS07	04/02/19	1.32
WS08	04/02/19	0.65
WS09	04/02/19	0.59
WS10	04/02/19	0.10
WS11	04/02/19	0.97
WS01	13/02/19	0.80
WS02	13/02/19	0.40
WS03	13/02/19	0.22
WS04	13/02/19	0.97
WS05	13/02/19	0.65
WS06	13/02/19	0.07
WS07	13/02/19	0.82
WS08	13/02/19	0.70
WS09	13/02/19	0.52
WS10	13/02/19	0.15
WS11	13/02/19	1.13
WS01	28/02/19	1.02
WS02	28/02/19	0.74
WS03	28/02/19	0.67
WS04	28/02/19	1.01
WS05	28/02/19	0.85
WS06	28/02/19	0.30
WS07	28/02/19	1.50
WS08	28/02/19	0.79
WS09	28/02/19	0.86
WS10	28/02/19	0.36
WS11	28/02/19	1.26

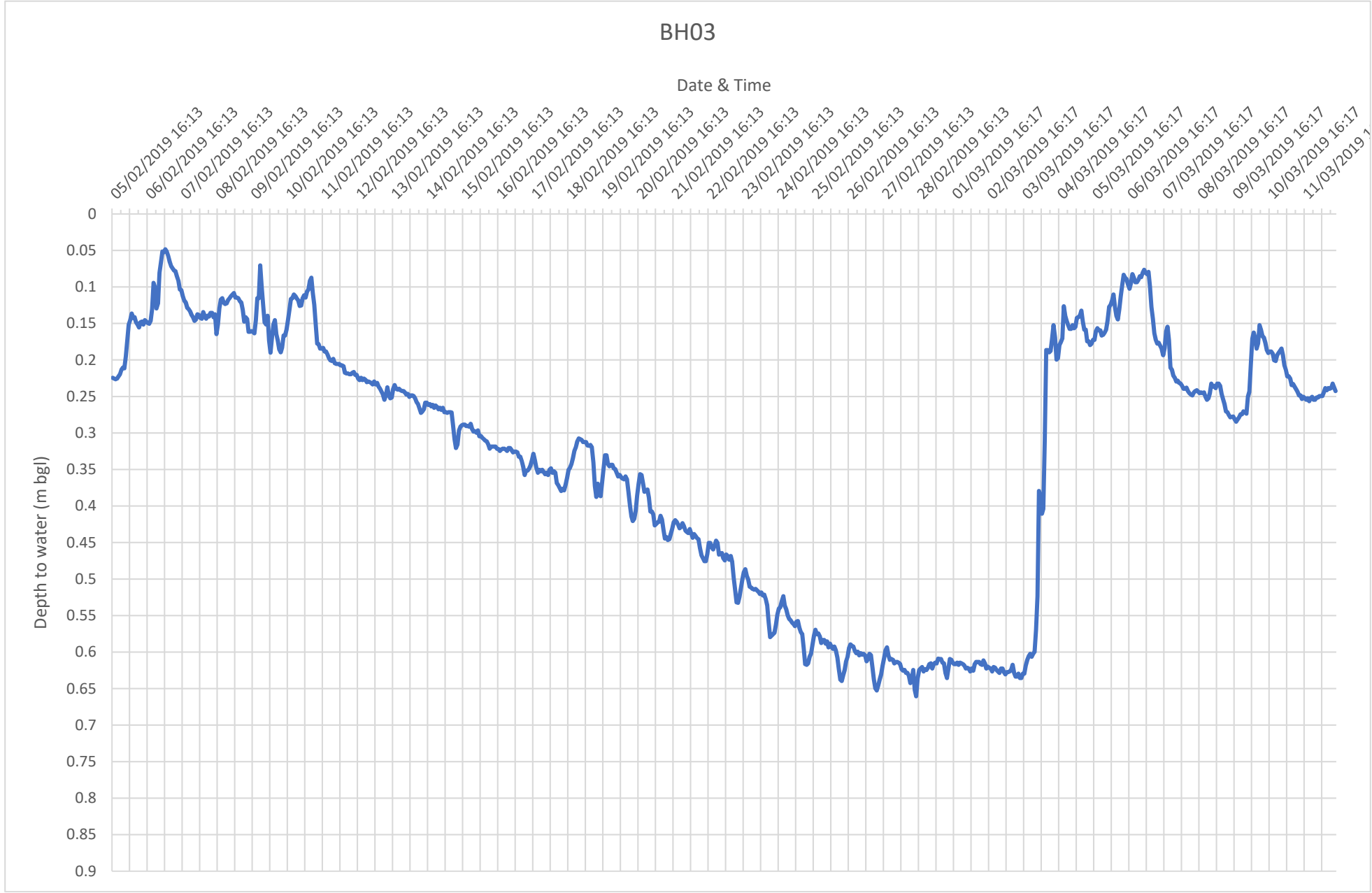
Project: Summer Lane, Pagham, Bognor Regis,
Ref: GE17671
Client: Drew Smith Limited

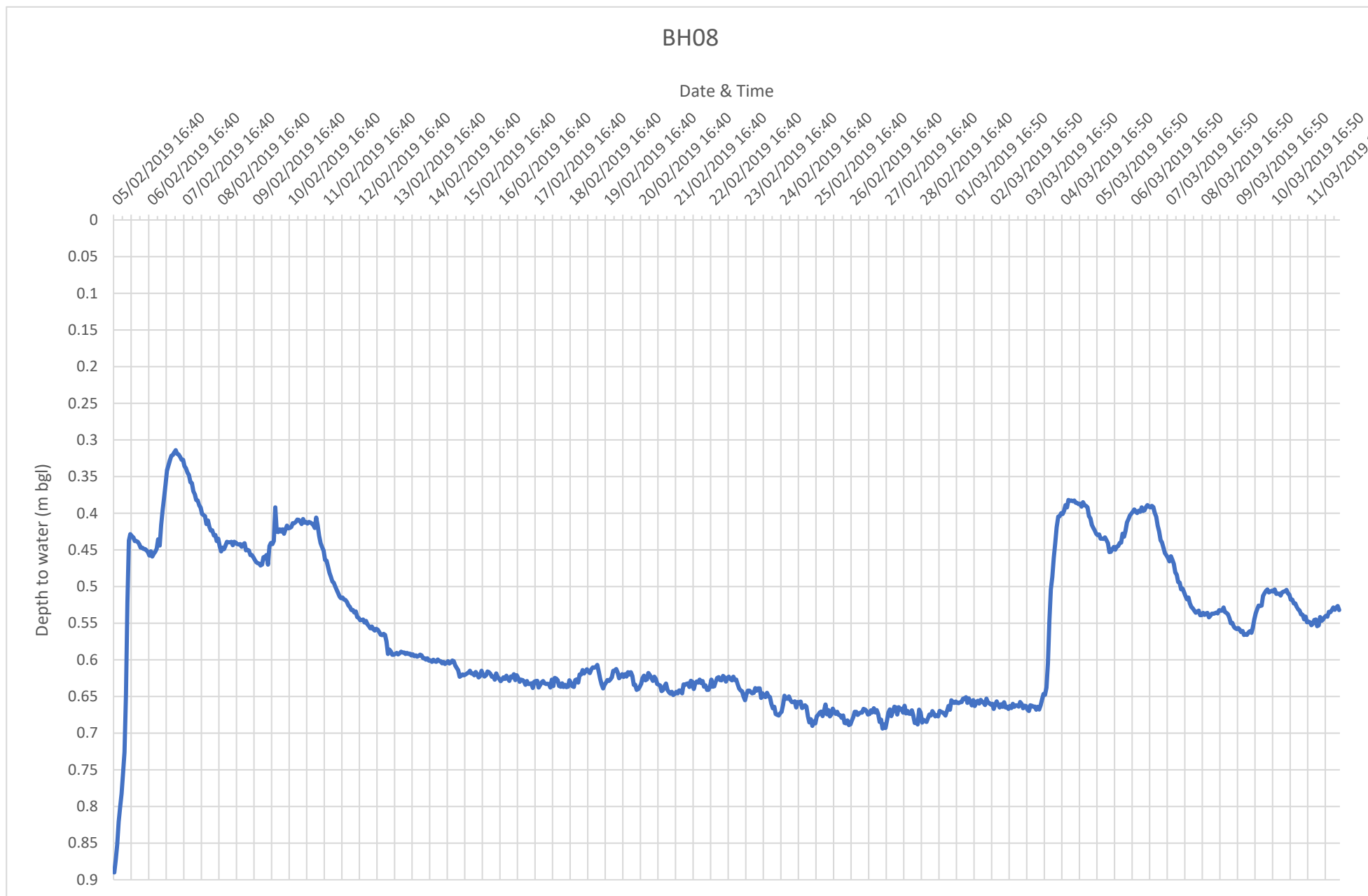
Location	Date	GWL (m bgl)
WS01	12/03/19	0.73
WS02	12/03/19	0.42
WS03	12/03/19	0.15
WS04	12/03/19	0.94
WS05	12/03/19	0.58
WS06	12/03/19	0.00
WS07	12/03/19	1.02
WS08	12/03/19	0.59
WS09	12/03/19	0.50
WS10	12/03/19	0.21
WS11	12/03/19	0.85
WS01	29/03/19	1.03
WS02	29/03/19	0.78
WS03	29/03/19	0.74
WS04	29/03/19	1.01
WS05	29/03/19	0.85
WS06	29/03/19	0.51
WS07	29/03/19	1.49
WS08	29/03/19	0.76
WS09	29/03/19	0.88
WS10	29/03/19	0.48
WS11	29/03/19	1.29
WS01	11/04/19	1.09
WS02	11/04/19	0.88
WS03	11/04/19	0.91
WS04	11/04/19	1.05
WS05	11/04/19	0.91
WS06	11/04/19	0.66
WS07	11/04/19	1.68
WS08	11/04/19	0.85
WS09	11/04/19	1.15
WS10	11/04/19	0.53
WS11	11/04/19	1.30
WS01	25/04/19	1.12
WS02	25/04/19	0.93
WS03	25/04/19	1.02
WS04	25/04/19	1.11
WS05	25/04/19	0.95
WS06	25/04/19	0.80
WS07	25/04/19	1.81
WS08	25/04/19	0.89
WS09	25/04/19	1.17
WS10	25/04/19	0.55
WS11	25/04/19	1.36
Max values		1.81
Min Vaules		0.00

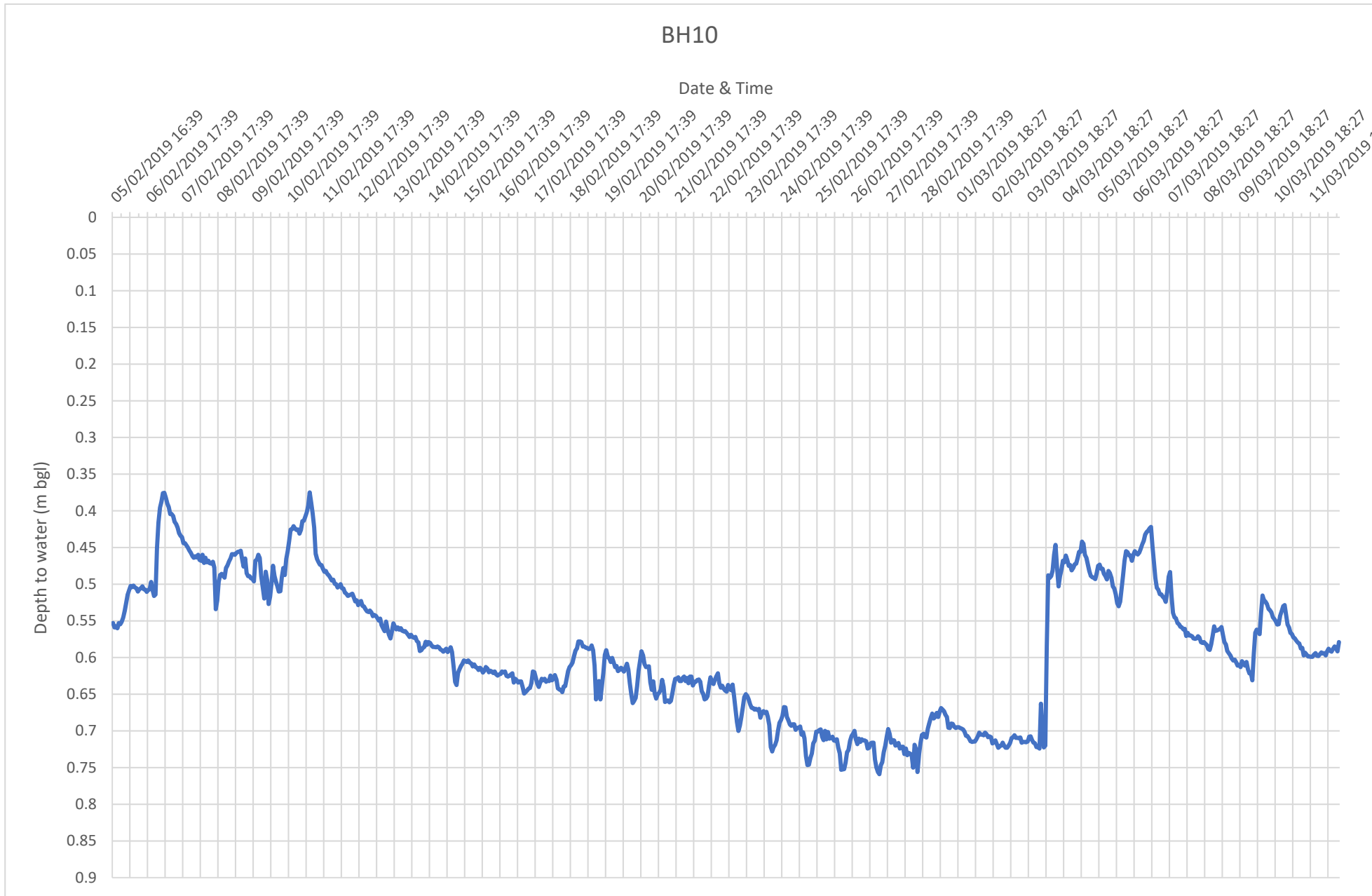


APPENDIX B

Continuous Groundwater Monitoring Results







28th January 2019

Our ref: GE17671/SA02/190128



Daniel O'Shea
Drew Smith Limited
Drew Smith House
Mill Court
The Sawmills
Durley
Southampton
Hampshire
SO32 2EJ

Dear Daniel,

RE: Summer Lane, Pagham, Bognor Regis, PO21 4NQ – Soakage Testing

We are pleased to present the results of the soakage testing undertaken at the above site. The soakage tests were undertaken broadly in accordance with BRE Digest 365 'Soakaway Design' BRE, 2016 with the testing limited to three consecutive days.

A geo-environmental engineer attended site on the 11th, 14th, 15th and 16th January 2019 to undertake the intrusive investigation. A total of twenty-one full scale soakage tests (TP01 to TP21) were undertaken within trial pits. Eleven windowless sample boreholes (WS01 to WS11) were also drilled during the works to allow the installation of monitoring standpipes for winter groundwater level monitoring. The exploratory positions were located in line with instructions from Drew Smith Limited and access constraints at the time of investigation.

Background

It is understood that the site is proposed to be developed with a residential development and associated infrastructure. As such, soakage testing is required to confirm the suitability of underlying soils for drainage via soakaways and to inform the planning, design and construction strategies for the site.

Published geological records indicate that the ground conditions were likely to comprise River Terrace Deposits overlying London Clay Formation.

Site Description

At the time of the investigation works the site comprised a section of a large arable field in the west with a grass paddock with areas of trees and scrub in the east. The site appeared generally level. The western field was accessed from the west end of Summer Lane via a gap in the hedgerow. Access to the paddock was afforded by a grass track in the south-eastern corner of the site.

Ground Conditions

The ground conditions encountered were relatively consistent with those anticipated from published geological maps, i.e. a thickness of Topsoil and/or Made Ground overlying River Terrace Deposits in turn overlying London Clay. A generalised summary of the encountered conditions is presented in Table 1.

Geo-Environmental Services Ltd
Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL
+44(0)1273 832972 www.gesl.net

Environmental Consultants | Geotechnical Engineers | Site Investigations

Geo-Environmental Services Ltd incorporated in England number 3214980 VAT number 679544479



Top (m bgl)	Base (m bgl)	Geology
0	0.10 – 0.30	TOPSOIL: Brown CLAY with varying proportions of silt and gravel with occasional or frequent rootlets. (All locations except TP02 and TP12).
0 – 0.10	0.10 – 0.20	MADE GROUND: Brown silty clay with rubbish and brown gravelly clay with brick. (TP02, TP04 and TP12 only).
0.10 – 0.30	1.90 – 3.00+	RIVER TERRACE DEPOSITS (CLAY): Typically CLAY with medium or high proportions of sand and gravel. Silty CLAY and CLAY with no secondary constituents occasionally encountered. The clay soils appeared visually desiccated to depths between 0.40m and 0.70m bgl. (All locations).
1.10 – 2.00	1.40 – 3.00+	RIVER TERRACE DEPOSITS (SAND): Thicknesses of clayey SAND, clayey gravelly SAND and gravelly SAND soils frequently encountered at depths greater than 1.50m bgl. (TP08, TP11, WS01 to WS06 and WS08 to WS11).
1.90 – 2.80	3.00+	LONDON CLAY FORMATION: CLAY or slightly sandy CLAY. (WS02 to WS04 and WS07 to WS11).

Table 1 Summary of Ground Conditions

Groundwater was encountered during the investigation as shown in Table 2.

Location	Depth to groundwater (m bgl)	Comment
TP01	1.50	Rose to 1.49m bgl
TP03	1.34	
TP05	1.50	Rose to 1.40m bgl
TP06	1.50	
TP07	1.38	
TP08	1.40	Rose to 1.33m bgl
TP10	1.60	
TP11	1.45	
WS01	1.65	
WS02	1.30	
WS03	1.30	
WS04	1.30	
WS05	1.30	
WS06	1.05	
WS07	1.30	
WS08	1.30	
WS09	1.30	
WS10	1.05	
WS11	1.50	

Table 2 Summary of Groundwater Strikes

For full details of the ground conditions encountered, reference should be made to the exploratory hole logs presented within Appendix A.

Soakage Testing

Soakage testing was undertaken broadly in accordance with BRE Digest 365 Soakaway Design in all twenty-one trial pits with the exception of TP03, TP06 and TP10 where the trial pit walls collapsed and testing was abandoned. Testing was undertaken in TP01 to TP11 at depths between 1.33m and 1.50m bgl, suitable for likely proposed

conventional stormwater soakaways. Testing in TP12 to TP21 was undertaken at depths between 0.44m and 0.70m bgl, suitable for any proposed permeable pavement.

During the testing in TP01 to TP11 and TP13-TP14 the fall in water level during the test period was insufficient to calculate a rate of infiltration. Test periods ranged between 20 and 48 hours, unless water levels were noted to be increasing during testing as in TP02, TP04 and TP05. Infiltration rates within the remaining shallow soils (TP12 and TP15 to TP21) ranged between $9.5 \times 10^{-7} \text{m/s}$ and $1.1 \times 10^{-5} \text{m/s}$, however in some instances the time taken to complete the tests was such that it was not possible to undertake three complete fillings in some locations. The results of the testing are summarised in Table 2 below. The full soakage test results are presented within Appendix B.

Location	Permeability (m/s)			Test Depth (m)	Comments
	Test 1	Test 2	Test 3		
TP01	-	-	-	1.49*	Insufficient fall in water to complete test
TP02	-	-	-	1.50	
TP03	-	-	-	1.34*	Trial pit collapsed during testing
TP04	-	-	-	1.58*	Insufficient fall in water to complete test
TP05	-	-	-	1.40*	
TP06	-	-	-	-	Trial pit collapsed during testing
TP07	-	-	-	1.38*	Insufficient fall in water to complete test
TP08	-	-	-	1.33	
TP09	-	-	-	1.35	
TP10	-	-	-	-	Trial pit collapsed during testing
TP11	-	-	-	1.45*	Insufficient fall in water to complete test
TP12	1.9×10^{-6}	-	-	0.63	Insufficient fall in water to complete test
TP13	-	-	-	0.70	
TP14	-	-	-	0.60	Infiltration ceased in Test 1
TP15	1.1×10^{-5}	4.9×10^{-6}	4.1×10^{-6}	0.55	Test 3 based on data extrapolation
TP16	1.4×10^{-6}	-	-	0.67	Based on data extrapolation
TP17	5.5×10^{-6}	1.8×10^{-6}	1.5×10^{-6}	0.60	Test 3 based on data extrapolation
TP18	1.2×10^{-6}	-	-	0.50	Infiltration ceased in Test 3
TP19	2.0×10^{-6}	1.9×10^{-6}	-	0.55	
TP20	1.7×10^{-6}	1.3×10^{-6}	9.5×10^{-7}	0.55	Test 2 & 3 based on data extrapolation
TP21	8.9×10^{-6}	9.1×10^{-6}	-	0.44	Infiltration ceased in Test 3

Note: *indicates test carried out at groundwater level

Table 2 Soakage Test Results

Winter Groundwater Monitoring

Groundwater level monitoring within the borehole standpipes installed in WS01 to WS11 is proposed to be undertaken between January and April 2019, the results of which will be reported under separate cover.

Conclusions

The testing undertaken indicates that the soils at the site are unlikely to be suitable for stormwater drainage via conventional soakaways owing to the presence of cohesive soils, clayey granular soils and the presence of groundwater. As a result, on-site storage and attenuation together with alternative storm water disposal options should be considered.

The shallow soils at the site were shown to be moderately permeable in the majority of locations tested therefore permeable paving may be an effective component in the site drainage scheme for storage and peak flow attenuation.

Closure

We trust that we have interpreted your instructions correctly, and please do not hesitate to contact us should you have any queries.

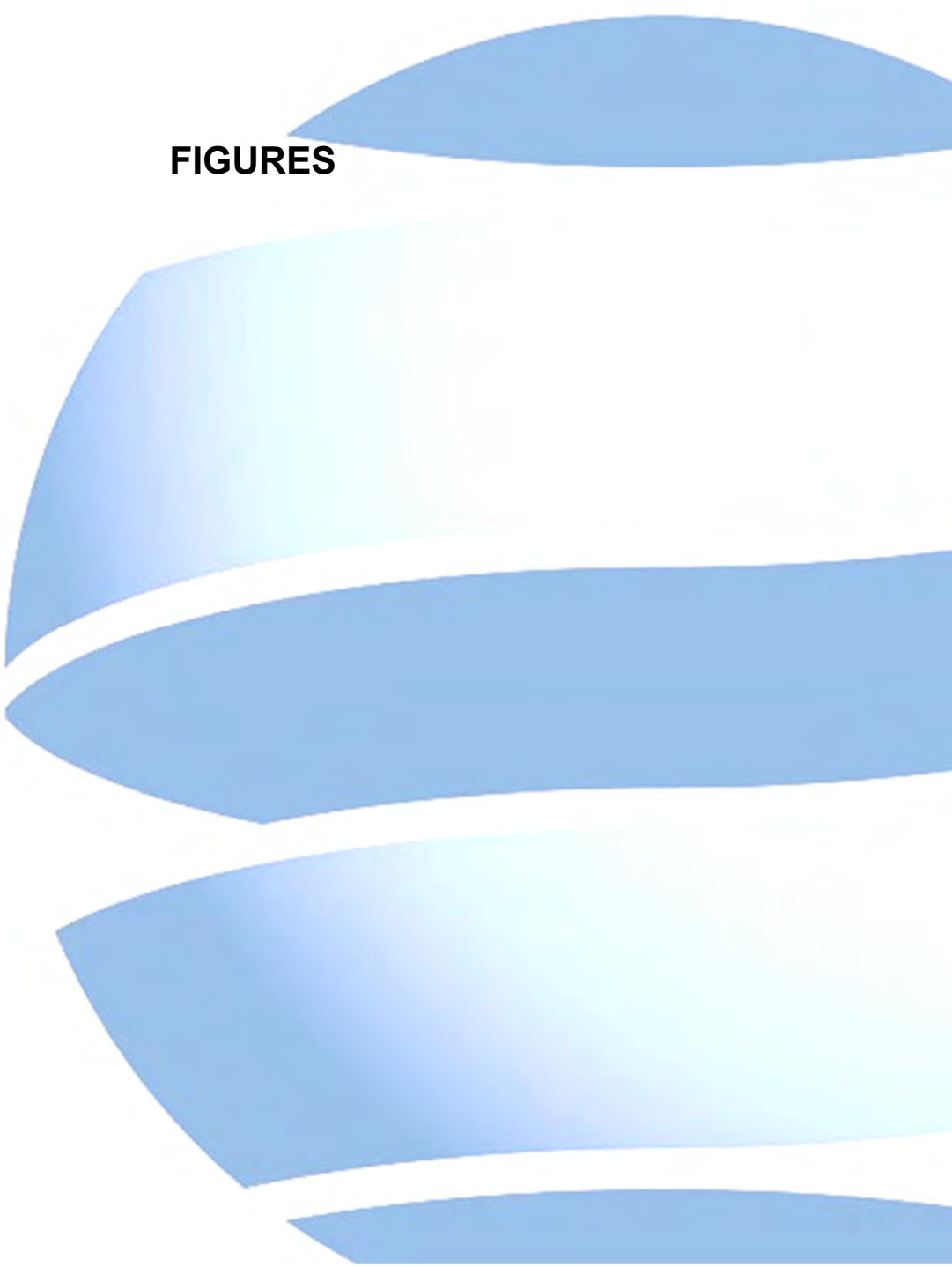
Yours sincerely
For and on Behalf of Geo-Environmental



SHAUN ARMITAGE BSc (Hons), FGS
Senior Consulting Engineer
shaun.armitage@gesl.net

Enc	Figure 1	Site Location Plan
	Figure 2	Exploratory Hole Locations Plan
	Appendix A	Exploratory Hole Logs
	Appendix B	Soakage Test Results

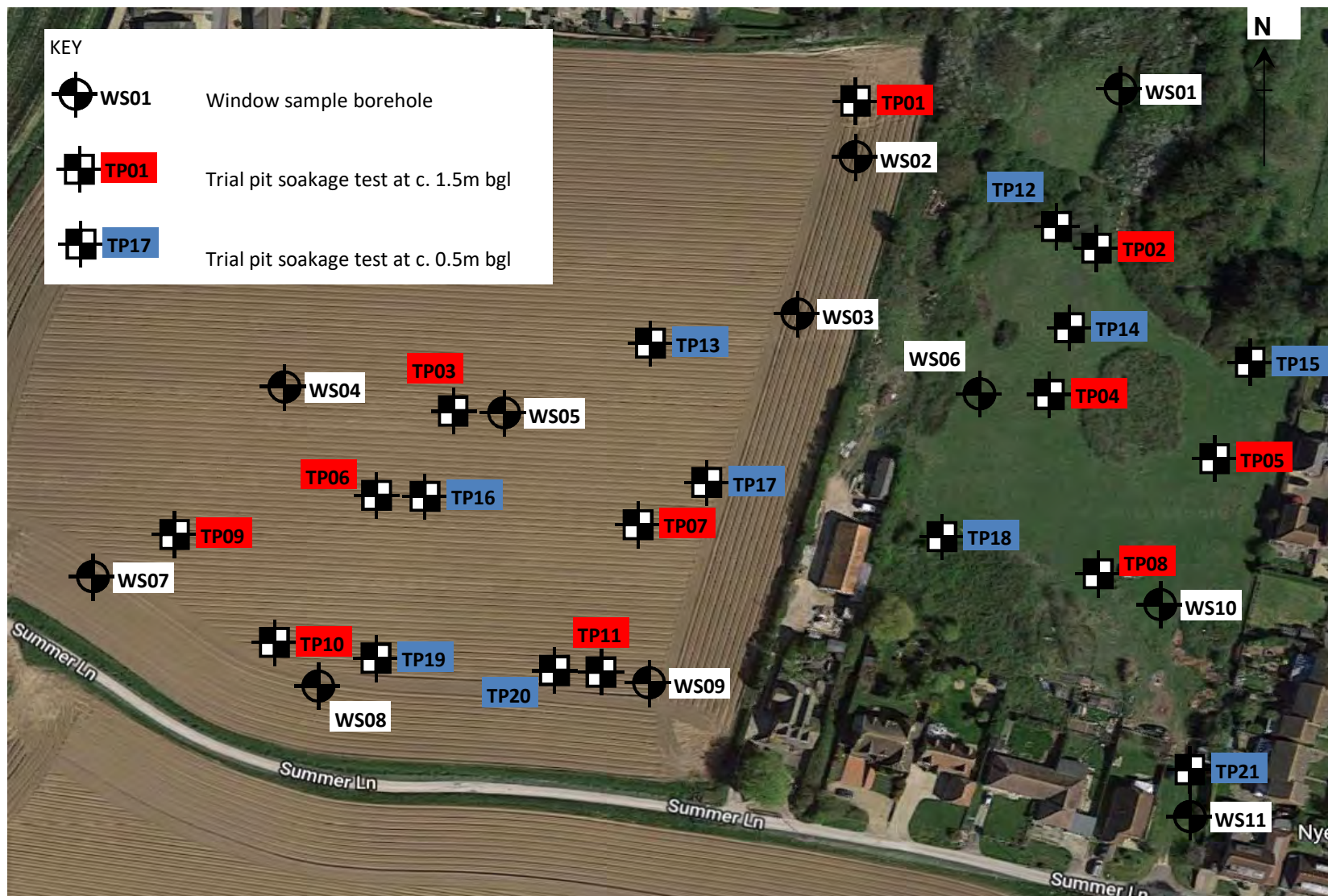


A decorative graphic on the right side of the page consisting of several overlapping, wavy, horizontal bands in various shades of blue, ranging from a light sky blue to a deeper cerulean.

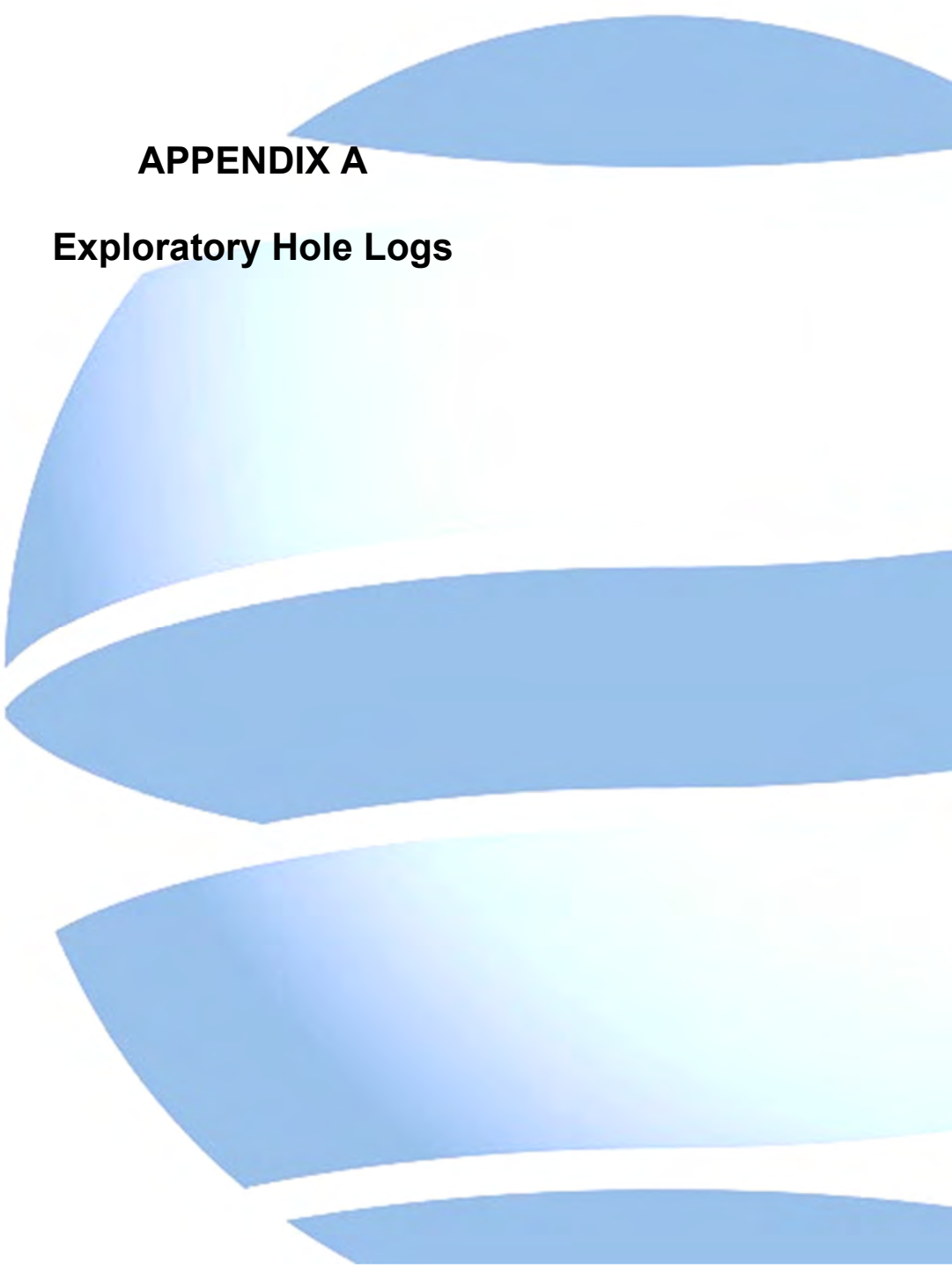
FIGURES



Project:	Summer Lane, Pagham, Bongor Regis, PO21 4NQ			Title	Site Location Plan	
Client:	Drew Smith Limited			Geo-Environmental Services Ltd Unit 7 Danworth Farm, Cuckfield Road Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net	 Geo-Environmental	
Ref No:	GE17671	Revision:	0			
Drawn:	SA	Date:	07/01/2019			
Figure:	1	Scale:	Not To Scale			



Project:	Summer Lane, Pagham, Bongor Regis, PO21 4NQ			Title	Exploratory Hole Location Plan	
Client:	Drew Smith Limited			Geo-Environmental Services Ltd Unit 7 Danworth Farm, Cuckfield Road Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net	 Geo-Environmental	
Ref No:	GE17671	Revision:	0			
Drawn:	SA	Date:	23/01/2019			
Figure:	2	Scale:	Not To Scale			



APPENDIX A

Exploratory Hole Logs



Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No

TP01

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 2.40

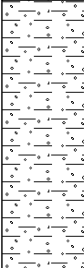
Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with frequent rootlets and roots up to 50mm. TOPSOIL	1
				0.50			Brown desiccated silty gravelly CLAY with occasional rootlets. Gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	
							Brown gravelly CLAY with two cobbles of subangular flint. Gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	
							Light brown sandy CLAY. Sand fine. RIVER TERRACE DEPOSITS	
				1.40		1.50	End of Pit at 1.50m	
							3	
								4
								5

Water Strikes		Remarks	Groundwater encountered at 1.5m bgl
Depth Strike	Rose to (m/bgl)		
1.50	1.49		
		Stability	Unstable







Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP02
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 2.30

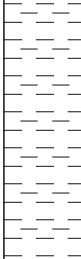
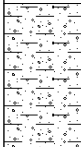
Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.10			Brown silty clay with roots and rubbish. MADE GROUND	1
							Brown CLAY. RIVER TERRACE DEPOSITS	
							Light brown and greenish brown mottled sandy gravelly CLAY. Sand fine, gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	
				1.00				
				1.50			End of Pit at 1.50m	2
								3
								4
								5

Water Struck		Remarks
Depth Struck	Rose to (m)	
		Stability Stable







Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP03
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions
(m):

2.20

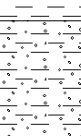
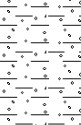
Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
▼				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
							Light brown and brown desiccated CLAY with occasional rootlets. RIVER TERRACE DEPOSITS	
				0.70			Light brown and blueish grey mottled very gravelly CLAY with one flint cobble. Gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	1
				1.50				
							End of Pit at 1.50m	
								2
								3
								4
								5
Water Strikes								
Depth Strike	Rise to (m bgl)							
1.34	0.00	Remarks Groundwater encountered at 1.34m bgl						
		Stability Unstable						





Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No

TP04

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 2.00

Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.10			Brown silty CLAY with frequent rootlets. TOPSOIL	
				0.20			Brown gravelly clay. Gravel fm angular to subangular brick. MADE GROUND	
							Light brown and brown mottled CLAY. RIVER TERRACE DEPOSITS	
				0.70			Light brown and brown mottled gravelly CLAY. Gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	1
				1.20			Light brown and greenish yellow sandy CLAY. Sand fine. RIVER TERRACE DEPOSITS	
				1.40			Brown and purplish brown mottled CLAY. RIVER TERRACE DEPOSITS	
				1.50			End of Pit at 1.50m	
								2
								3
								4
								5

Water Strakes
Depth Strake

Rose to (m) (g)

Remarks

Stability Stable





Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP05
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 1.80

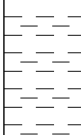
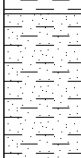
Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
							Light brown and brown CLAY. RIVER TERRACE DEPOSITS	
				0.70			Light brown and blueish grey slightly sandy CLAY. Sand fine. RIVER TERRACE DEPOSITS	1
				1.20			Light brown and blueish grey sandy gravelly CLAY. Sand fine, gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	
				1.50			End of Pit at 1.50m	
								2
								3
								4
								5
Water Struck		Remarks		Groundwater encountered at 1.5m bgl				
Depth Struck	Rose to (m bgl)							
1.50	1.40							
Stability		Stable						







Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No

TP06

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 2.00

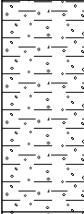
Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
▼				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	1
				0.50			Light brown and brown desiccated slightly gravelly CLAY. Gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	
				1.20			Light brown and greyish brown gravelly CLAY. Gravel fm angular to subangular flint. RIVER TERRACE DEPOSITS	
				1.50			Light brown and blueish gret mottled slightly gravelly CLAY. Gravel fm angular to subangular flint. RIVER TERRACE DEPOSITS	
							End of Pit at 1.50m	
								2
								3
								4
								5
Water Struck		Remarks		Groundwater encountered at 1.5m bgl				
Depth Struck	Rose to (m bgl)							
1.50	0.00							
Stability		Unstable						







Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP07
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 2.00

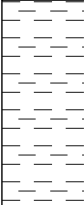
Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
▼				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
				0.50			Light brown and brown desiccated CLAY. RIVER TERRACE DEPOSITS	
				1.20			Light brown and brown CLAY. RIVER TERRACE DEPOSITS	1
				1.40			Light brown and brown gravelly CLAY. Gravel fm angular to rounded flint.	
				1.50			Light brown and blueish grey mottled CLAY. RIVER TERRACE DEPOSITS	
							End of Pit at 1.50m	
								2
								3
								4
								5
Water Struck		Remarks		Groundwater encountered at 1.38m bgl				
Depth Struck	Rose to (m bgl)							
1.38	0.00							
Stability		Stable						







Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP08
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m):
2.00
0.55
Depth 1.40

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with occasional rootlets. TOPSOIL	
				0.50			Light brown and brown CLAY. RIVER TERRACE DEPOSITS	
							Light brown and blueish grey mottled CLAY. RIVER TERRACE DEPOSITS	
				1.20			Light brown and blueish grey clayey fine SAND. RIVER TERRACE DEPOSITS	
				1.40			End of Pit at 1.40m	
								1
								2
								3
								4
								5
Water Strikes								
Depth Strike	Rise to (m bgl)							
1.40	1.33	Remarks Groundwater encountered at 1.4m bgl						
		Stability Stable						





Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP09
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions
(m):

2.50

Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with occasional rootlets. TOPSOIL	
				0.40			Dark brown and brown desiccated CLAY. RIVER TERRACE DEPOSITS	
							Dark brown and brown CLAY. RIVER TERRACE DEPOSITS	
				1.20			Light brown and brown mottled gravelly CLAY. Gravel fm angular to subangular flint. RIVER TERRACE DEPOSITS	1
				1.50			End of Pit at 1.50m	2
								3
								4
								5
Water Strakes								
Depth Strike	Rose to (img)	Remarks						
		Stability Stable						





Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No

TP10

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 2.00

Depth
1.60

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
▼				0.20			Brown silty CLAY with occasional rootlets. TOPSOIL	
				0.50			Brown and light brown desiccated CLAY. RIVER TERRACE DEPOSITS	
				1.20			Light brown and brown mottled slightly gravelly CLAY. Grave fm angular to subangular flint. RIVER TERRACE DEPOSITS	1
				1.60			Light brown and blueish grey sandy CLAY. Sand fmc. RIVER TERRACE DEPOSITS	
							End of Pit at 1.60m	2
								3
								4
								5
Water Strikes								
Depth Strike	Rose to (m bgl)							
1.60	0.00	Remarks Groundwater encountered at 1.6m bgl						
		Stability Unstable						





Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No

TP11

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 2.00

Depth
1.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with occasional rootlets. TOPSOIL	
				0.50			Light brown and brown mottled desiccated CLAY. RIVER TERRACE DEPOSITS	
				1.10			Light brown and brown mottled CLAY. RIVER TERRACE DEPOSITS	1
				1.50			Greenish yellow and yellowish brown clayey SAND. RIVER TERRACE DEPOSITS	
							End of Pit at 1.50m	
								2
								3
								4
								5
Water Strikes								
Depth Strike	Rose to (m bgl)							
1.45	0.00	Remarks Groundwater encountered at 1.45m bgl						
		Stability Stable						





Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP12
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 1.30

Depth
0.60

0.55



Scale
1:25

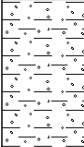
Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty clay with roots and rubbish. MADE GROUND	
				0.60			Light brown and blueish grey slightly gravelly CLAY. Gravel fm angular to subangular flint. RIVER TERRACE DEPOSITS	
							End of Pit at 0.60m	
								1
								2
								3
								4
								5
Water Struck								
Depth Struck								
Remarks								
Stability		Stable						



Trial Pit Log

Project Name: Summer Lane, Pagham			Project No. GE17671		Co-ords: - Level:		Date 14/01/2019	
Location: Bongor Regis, PO21 4NQ					Dimensions (m):		2.00	
Client: Drew Smith Limited					Depth 0.70		0.55	
Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
							Light brown and brown desiccated gravelly CLAY. Gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	
				0.70			End of Pit at 0.70m	
							1	
							2	
							3	
							4	
							5	
Water Strikes		Remarks						
Depth Strike	Raise to (mddg)							
		Stability Stable						



Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP14
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 1.40

Depth
0.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
				0.50			Light brown and brown desiccated CLAY. RIVER TERRACE DEPOSITS	
							End of Pit at 0.50m	
								1
								2
								3
								4
								5
Water Struck								
Depth Struck	Rose to (m)	Remarks						
		Stability Stable						





Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP15
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 1.40

Depth
0.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
				0.50			Light brown and brown slightly gravelly CLAY. Gravel mc angular to subangular flint. RIVER TERRACE DEPOSITS	
							End of Pit at 0.50m	
								1
								2
								3
								4
								5
Water Struck								
Depth Struck	Rose to (m)	Remarks						
		Stability Stable						





Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No
TP16
Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 1.50

Depth
0.70

0.55



Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
				0.70			Light brown and brown desiccated slightly gravelly CLAY. Gravel mc angular to subangular flint. RIVER TERRACE DEPOSITS	
							End of Pit at 0.70m	
								1
								2
								3
								4
								5
Water Struck								
Depth Struck	Rose to (m)	Remarks						
		Stability Stable						



Trial Pit Log

Project Name: Summer Lane, Pagham			Project No. GE17671		Co-ords: - Level:		Date 14/01/2019	
Location: Bongor Regis, PO21 4NQ					Dimensions (m):		Scale 1:25	
Client: Drew Smith Limited					Depth 0.50		Logged RG	
Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
				0.50			Brown and dark brown desiccated CLAY. RIVER TERRACE DEPOSITS	
							----- End of Pit at 0.50m	
							1	
							2	
							3	
							4	
							5	
Water Strikes			Remarks					
Depth Strike		Rose to (mdeg)						
			Stability Stable					



Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No

TP18

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 0.65

Depth
0.70

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.10			Brown silty CLAY with frequent rootlets. TOPSOIL	
				0.30			Light brown and slight gravelly clay. Gravel fm angular to subrounded various lithologies. RIVER TERRACE DEPOSITS	
							Light brown and brown CLAY. RIVER TERRACE DEPOSITS	
				0.70				
							End of Pit at 0.70m	
								1
								2
								3
								4
								5
Water Strike		Remarks						
Depth Strike	Rose to (m)							
		Stability	Stable					







Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Geo-Environmental www.gesl.net

Trial Pit Log

Trial Pit No

TP19

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 1.90

Depth
0.50

0.55

Scale
1:25

Logged
RG

Client: Drew Smith Limited

Water Strike	Samples & In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
	Depth	Type	Results					
				0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
				0.50			Light brown and brown slightly gravelly CLAY. Gravel fm angular to subangular flint. RIVER TERRACE DEPOSITS	
							End of Pit at 0.50m	
								1
								2
								3
								4
								5
Water Struck		Remarks						
Depth Struck	Rose to (m)							
		Stability Stable						



Trial Pit Log

TrialPit No

TP20

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
14/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m):

Scale
1:25

Client: Drew Smith Limited

Depth
0.50

0.55

Logged
RG

[illegible]

Trial Pit Log

TrialPit No

TP21

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords: -
Level:

Date
15/01/2019

Location: Bongor Regis, PO21 4NQ

Dimensions (m): 5 1.40

Scale
1:25

Client: Drew Smith Limited

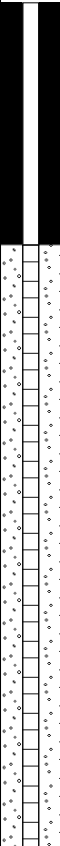
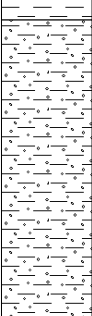
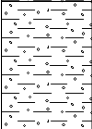
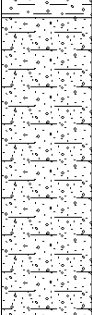
Depth
0.50

0.55

Logged
RG

[illegible]

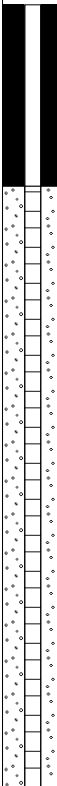
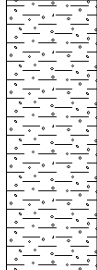
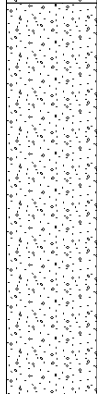
 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log				Borehole No. WS01 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:		Hole Type WLS	
Location: Bongor Regis, PO21 4NQ				Level:		Scale 1:25	
Client: Drew Smith Limited				Dates: 11/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20		 Brown silty CLAY with frequent rootlets. TOPSOIL	1	
					0.50		 Brown silty desiccated CLAY with occasional rootlets. RIVER TERRACE DEPOSITS		
					1.50		 Light brown slightly gravelly CLAY. Gravel fine to medium angular to subangular. RIVER TERRACE DEPOSITS	2	
					2.00		 Light brown gravelly CLAY. Gravel fmc angular to subangular of flint. RIVER TERRACE DEPOSITS		
					3.00		 Light brown and orangish brown gravelly clayey SAND. Sand fine. Gravel fmc angular to subangular of flint. RIVER TERRACE DEPOSITS	3	
End of Borehole at 3.00m								4	
								5	

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.65	0.00			Groundwater encountered at 1.65m bgl. Monitoring standpipe installed



 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log				Borehole No. WS02 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:		Hole Type WLS	
Location: Bongor Regis, PO21 4NQ				Level:		Scale 1:25	
Client: Drew Smith Limited				Dates: 11/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20		 Brown slightly gravelly silty CLAY with frequent rootlets. Gravel fine to medium angular to subangular of flint. TOPSOIL		
					0.50		 Brown silty gravelly desiccated CLAY with occasional rootlets and rare charcoal up to 1mm. Gravel fine to medium angular to subangular of flint. RIVER TERRACE DEPOSITS		
					1.40		 Light brown, pinkish brown, orangish brown and black gravelly CLAY with occasional charcoal and rare rootlets. Gravel fmc of angular to subrounded flint. RIVER TERRACE DEPOSITS		
					2.70		 Yellowish brown gravelly fine SAND. Gravel fmc of angular to subrounded flint and sandstone. RIVER TERRACE DEPOSITS		
					3.00		 Greyish brown and brown mottled CLAY. LONDON CLAY		
							End of Borehole at 3.00m		

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.30	0.00			Groundwater encountered at 1.30m bgl. Monitoring standpipe installed



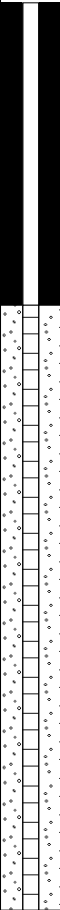
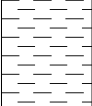
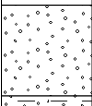
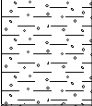
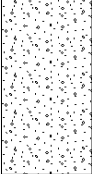
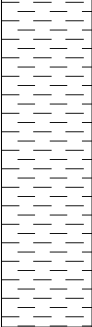
 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log		Borehole No. WS03 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:	
Location: Bongor Regis, PO21 4NQ		Level:		Scale 1:25	
Client: Drew Smith Limited		Dates: 11/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20		 Dark brown silty slightly gravelly CLAY with frequent rootlets. Gravel fine to medium of angular to subangular gravel. TOPSOIL		
					0.40		 Dark brown gravelly desiccated CLAY with occasional rootlets and roots up to 2mm diameter. Gravel fmc of angular to subangular flint. RIVER TERRACE DEPOSITS		
					0.90		 Light brown gravelly CLAY with occasional charcoal up to 2mm. Gravel fine to medium angular to subrounded of flint and sandstone. RIVER TERRACE DEPOSITS		
					1.10		 Light brown and brown gravelly CLAY. Gravel fmc angular to subangular of flint. RIVER TERRACE DEPOSITS		
					1.80		 Light brown, yellowish brown and pinkish brown sandy gravelly CLAY. Sand fine. Gravel fmc of angular to subangular flint. RIVER TERRACE DEPOSITS		
					2.20		 Orangish brown gravelly fine SAND. Gravel fine to medium of angular to subangular flint. RIVER TERRACE DEPOSITS		
				2.20		 Light brown, pinkish brown and greyish brown CLAY. LONDON CLAY			
				3.00		End of Borehole at 3.00m			

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.30	0.00			Groundwater encountered at 1.30m bgl. Monitoring standpipe installed



 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log				Borehole No. WS04 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:		Hole Type WLS	
Location: Bongor Regis, PO21 4NQ				Level:		Scale 1:25	
Client: Drew Smith Limited				Dates: 14/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20		 Brown silty CLAY with frequent rootlets. TOPSOIL		
					0.60		 Light brown and brown desiccated CLAY with occasional charcoal. RIVER TERRACE DEPOSITS		
					0.90		 Brown, black and grey clayey fmc very angular to subangular GRAVEL of flint. RIVER TERRACE DEPOSITS		
					1.30		 Dark brown gravelly CLAY. Gravel fine to medium of angular to subangular flint. RIVER TERRACE DEPOSITS		
					1.90		 Yellowish brown gravelly fine SAND. Gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS		
					3.00		 Light brown and brown CLAY. LONDON CLAY		
End of Borehole at 3.00m									

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.30	0.00			Monitoring standpipe installed





Geo-Environmental
www.gesl.net

Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL

Borehole Log

Borehole No.

WS05

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords:

Hole Type
WLS

Location: Bongor Regis, PO21 4NQ

Level:

Scale
1:25

Client: Drew Smith Limited

Dates: 14/01/2019

Logged By
RG

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	
					0.50			Brown slightly gravelly desiccated CLAY with occasional charcoal. Gravel fine to medium subangular to rounded of flint. RIVER TERRACE DEPOSITS	
								Brown and light brown gravelly CLAY with rare rootlets. Gravel fmc angular to subrounded flint. RIVER TERRACE DEPOSITS	
					1.20			Yellowish brown and greenish brown clayey gravelly fine SAND. Gravel fmc angular to subangular flint. RIVER TERRACE DEPOSITS	
					3.00		End of Borehole at 3.00m		

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.30	0.00			Monitoring standpipe installed





Geo-Environmental

Unit 7, Danworth Farm
Hurstpierpoint
BN6 9GL
www.gesl.net

Borehole Log

Borehole No.

WS06

Sheet 1 of 1

Project Name: Summer Lane, Pagham

Project No.
GE17671

Co-ords:

Hole Type
WLS

Location: Bongor Regis, PO21 4NQ

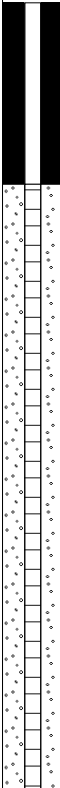
Level:

Scale
1:25

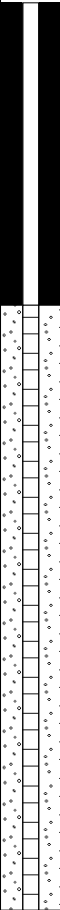
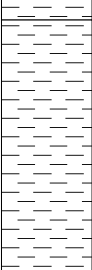
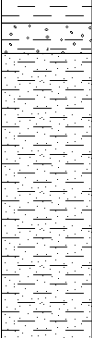
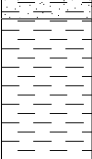
Client: Drew Smith Limited

Dates: 11/01/2019

Logged By
RG

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.30			Brown silty slightly gravelly CLAY with frequent rootlets. Gravel fine to medium angular to subangular of flint. TOPSOIL	1
								Light brown slightly gravelly CLAY with occasional rootlets. Gravel fine angular to subangular of flint. RIVER TERRACE DEPOSITS	
								Light brown and pinkish brown gravelly CLAY with one cobble of rounded flint at 0.9m bgl 80mm diameter. Gravel fine to medium angular to subrounded of flint. RIVER TERRACE DEPOSITS	
								Yellowish brown clayey gravelly fine SAND. Gravel fmc of angular to to subangular flint. RIVER TERRACE DEPOSITS	
								Light brown and pinkish brown mottled slightly sandy CLAY. Sand fine. RIVER TERRACE DEPOSITS	
								Greenish yellow clayey fine SAND. RIVER TERRACE DEPOSITS	
								Light brown, pinkish brown and greyish brown mottled slightly sandy CLAY. Sand fine RIVER TERRACE DEPOSITS	
Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks			
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to				
		1.05	0.00			Groundwater encountered at 1.05m bgl. Monitoring standpipe installed			

 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log				Borehole No. WS07 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:		Hole Type WLS	
Location: Bongor Regis, PO21 4NQ				Level:		Scale 1:25	
Client: Drew Smith Limited				Dates: 14/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20			Brown silty CLAY with occasional rootlets. TOPSOIL	
					0.50			Brown desiccated CLAY with rare rootlets and charcoal. RIVER TERRACE DEPOSITS	
					1.40			Light brown and brown mottled CLAY with rare charcoal. RIVER TERRACE DEPOSITS	
					1.50			Light brown and brown mottled gravelly CLAY. Gravel fine to medium angular to subangular flint. RIVER TERRACE DEPOSITS Yellowish brown and light brown sandy CLAY. Sand fine. RIVER TERRACE DEPOSITS	
					2.50			Dark grey CLAY with rare white shell inclusions up to 30mm. LONDON CLAY	
				3.00		End of Borehole at 3.00m			3
									4
									5

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.30	0.00			Monitoring standpipe installed

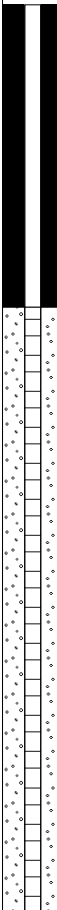


 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log				Borehole No. WS08 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:		Hole Type WLS	
Location: Bongor Regis, PO21 4NQ				Level:		Scale 1:25	
Client: Drew Smith Limited				Dates: 14/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description																			
		Depth (m)	Type	Results																							
					0.20			Brown silty CLAY with frequent rootlets. TOPSOIL	1																		
								Brown desiccated CLAY with occasional rootlets. RIVER TERRACE DEPOSITS																			
					0.60			Brown gravelly CLAY. Gravel fmc angular to subrounded flint. RIVER TERRACE DEPOSITS	2																		
					1.00			Yellowish grey and light brown sandy gravelly CLAY. Sand fine. Gravel fine subangular to rounded flint. RIVER TERRACE DEPOSITS																			
					1.40			Yellowish brown and brown clayey gravelly fine SAND. Gravel fmc angular to subrounded flint. RIVER TERRACE DEPOSITS																			
					2.10			Purplish brown and brown mottled CLAY. LONDON CLAY	3																		
			3.00		End of Borehole at 3.00m																						
<table border="1"> <tr> <th colspan="2">Casing</th> <th colspan="2">Water Strikes (mbgl)</th> <th colspan="2">Chiselling (mbgl)</th> </tr> <tr> <th>Diameter</th> <th>Depth (m)</th> <th>Depth Strike</th> <th>Rose to</th> <th>Depth from</th> <th>Depth to</th> </tr> <tr> <td></td> <td></td> <td>1.30</td> <td>0.00</td> <td></td> <td></td> </tr> </table> Remarks Monitoring standpipe installed										Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to			1.30	0.00		
Casing		Water Strikes (mbgl)		Chiselling (mbgl)																							
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to																						
		1.30	0.00																								



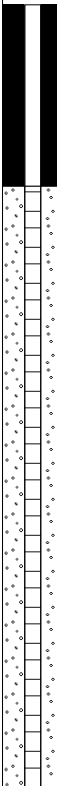
 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log				Borehole No. WS09 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:		Hole Type WLS	
Location: Bongor Regis, PO21 4NQ				Level:		Scale 1:25	
Client: Drew Smith Limited				Dates: 14/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20			Brown silty CLAY with frequent rootlets TOPSOIL	
					0.50			Brown desiccated CLAY with occasional rootlets and charcoal. RIVER TERRACE DEPOSITS	
								Light brown CLAY with occasional charcoal. RIVER TERRACE DEPOSITS	
					1.40			Yellowish brown and yellowish grey fine SAND. RIVER TERRACE DEPOSITS	
					1.60			Yellowish grey sandy CLAY. Sand fmc. RIVER TERRACE DEPOSITS	
					2.00			Brown gravelly CLAY. Gravel fmc of angular to subangular flint. RIVER TERRACE DEPOSITS	
					2.60			Brown and purplish brown mottled CLAY. LONDON CLAY	
			3.00		End of Borehole at 3.00m			3	
								4	
								5	

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.30	0.00			Monitoring standpipe installed



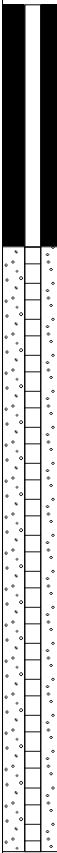
 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log				Borehole No. WS10 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:		Hole Type WLS	
Location: Bongor Regis, PO21 4NQ				Level:		Scale 1:25	
Client: Drew Smith Limited				Dates: 11/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20		 Brown silty CLAY with frequent rootlets. TOPSOIL	1	
							 Light brown and pinkish brown mottled desiccated CLAY with occasional rootlets. RIVER TERRACE DEPOSITS		
					0.70		 Light brown, pinkish brown and brown mottled slightly gravelly sandy CLAY. Sand is fine. Gravel fine to medium angular to subangular of flint. RIVER TERRACE DEPOSITS	1	
					1.10		 Light brown, yellowish brown and greyish brown gravelly CLAY. Gravel fmc of angular to subangular flint. RIVER TERRACE DEPOSITS		
					1.60		 Yellowish brown clayey gravelly fine SAND. Gravel fmc of angular to subrounded flint. RIVER TERRACE DEPOSITS		2
					2.00		 Yellowish brown clayey SAND. Sand fmc. RIVER TERRACE DEPOSITS		
					2.50		 Light brown and pinkish brown CLAY. LONDON CLAY	3	
					3.00		End of Borehole at 3.00m		
								5	

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.05	0.00			Groundwater encountered at 0.80m bgl. Monitoring standpipe installed

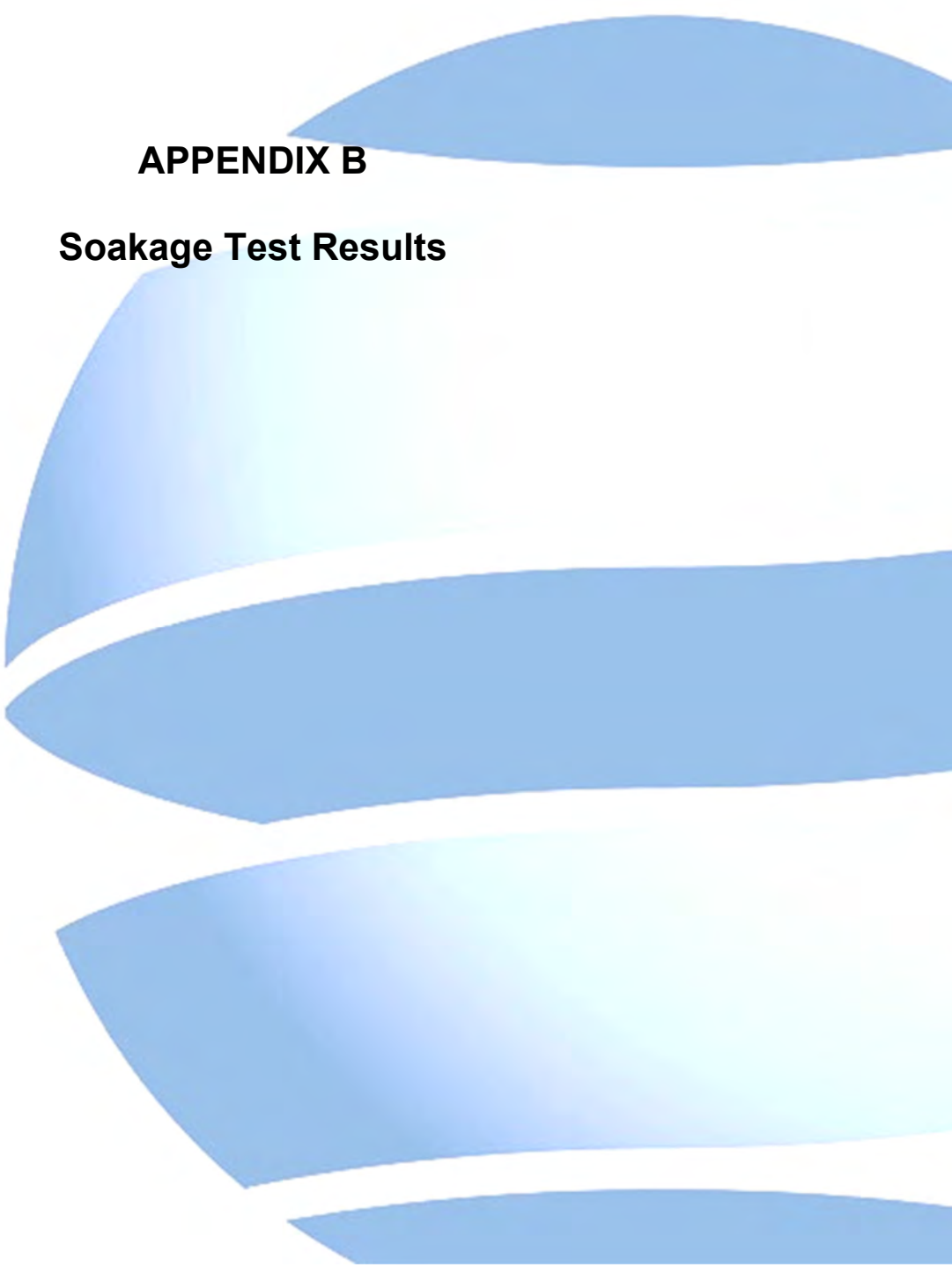


 Unit 7, Danworth Farm Hurstpierpoint BN6 9GL www.gesl.net		Borehole Log				Borehole No. WS11 Sheet 1 of 1	
Project Name: Summer Lane, Pagham		Project No. GE17671		Co-ords:		Hole Type WLS	
Location: Bongor Regis, PO21 4NQ				Level:		Scale 1:25	
Client: Drew Smith Limited				Dates: 11/01/2019		Logged By RG	

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.20		 Brown silty gravelly CLAY with frequent rootlets. Gravel fmc angular to subrounded flint. TOPSOIL		
					0.60		 Brown slightly gravelly desiccated CLAY with frequent rootlets. Gravel fine to medium subangular to subrounded of sandstone and flint. RIVER TERRACE DEPOSITS		
					1.50		 Light brown, pinkish brown and brown mottled CLAY. RIVER TERRACE DEPOSITS		
					1.90		 Light brown pinkish brown and brown sandy gravelly CLAY. Sand fmc. Gravel fmc angular to subangular of flint. RIVER TERRACE DEPOSITS		
					2.80		 Yellowish brown clayey gravelly fine SAND. Gravel fmc angular to subrounded of flint. RIVER TERRACE DEPOSITS		
					3.00		 Light brown and pinkish brown slightly sandy CLAY. Sand fine. LONDON CLAY		
					End of Borehole at 3.00m				

Casing		Water Strikes (mbgl)		Chiselling (mbgl)		Remarks
Diameter	Depth (m)	Depth Strike	Rose to	Depth from	Depth to	
		1.50	0.00			Groundwater encountered at 1.50m bgl. Monitoring standpipe installed



The background of the page features a series of overlapping, wavy blue shapes that create a sense of movement and depth. These shapes are in various shades of blue, ranging from a light, airy blue to a more solid, medium blue. They are positioned primarily on the right side of the page, with some extending towards the center.

APPENDIX B

Soakage Test Results

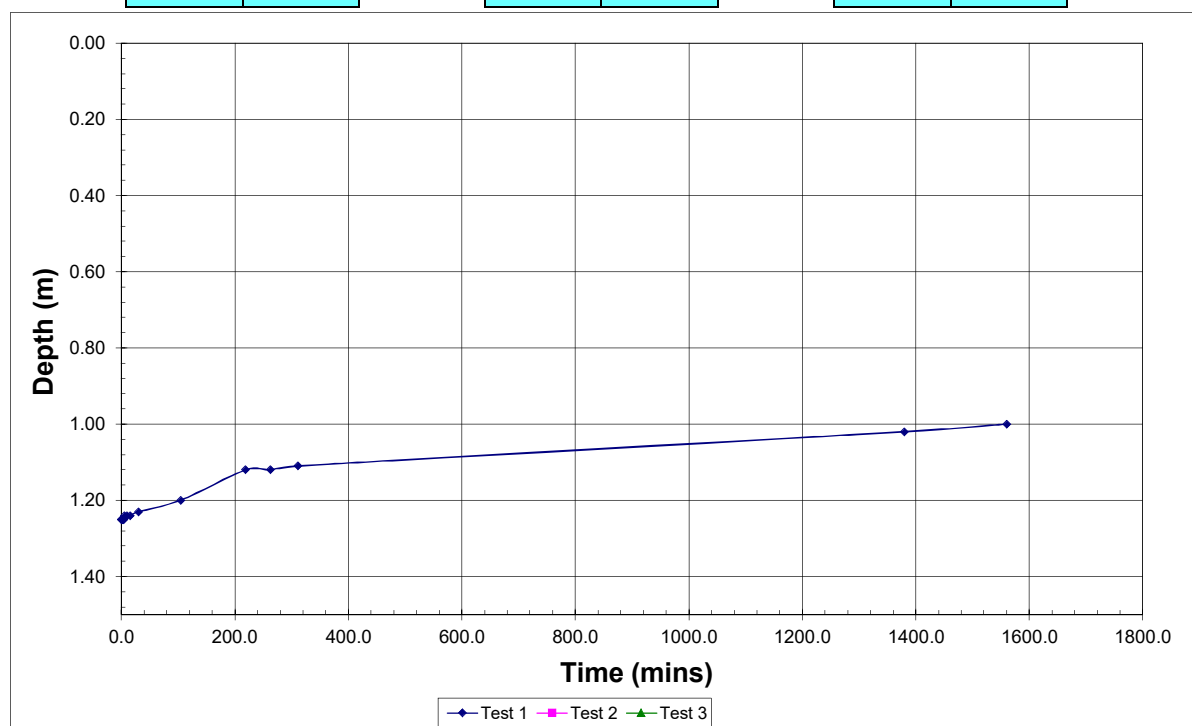
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP01
Pit depth (m)	1.50
Pit width (m)	0.55
Pit length (m)	2.40
Depth to standing water (m)	1.49

Test 1	
Time (min)	Depth (m)
0.0	1.25
1.0	1.25
2.0	1.25
3.0	1.25
4.0	1.25
5.0	1.24
10.0	1.24
15.0	1.24
30.0	1.23
104.0	1.20
219.0	1.12
263.0	1.12
311.0	1.11
1380.0	1.02
1560.0	1.00

Test 2	
Time (min)	Depth (m)

Test 3	
Time (min)	Depth (m)



Max. depth (m)	1.50	1.50	1.50
Effective depth (m)	0.25	1.50	1.50
75% effective depth (m)	1.31	0.38	0.38
50% effective depth (m)	1.38	0.75	0.75
25% effective depth (m)	1.44	1.13	1.13
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.17	0.99	0.99
ap 50	2.0575	5.745	5.745
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test

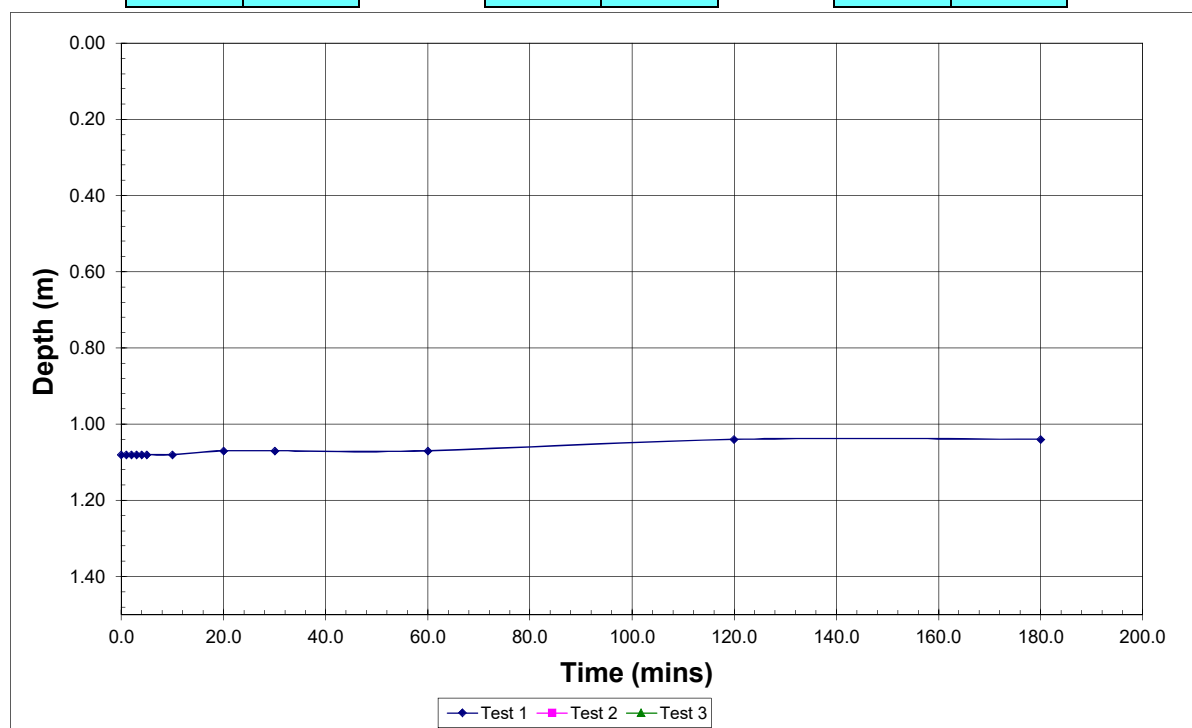
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP02
Pit depth (m)	1.50
Pit width (m)	0.55
Pit length (m)	2.30
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	1.08
1.0	1.08
2.0	1.08
3.0	1.08
4.0	1.08
5.0	1.08
10.0	1.08
20.0	1.07
30.0	1.07
60.0	1.07
120.0	1.04
180.0	1.04

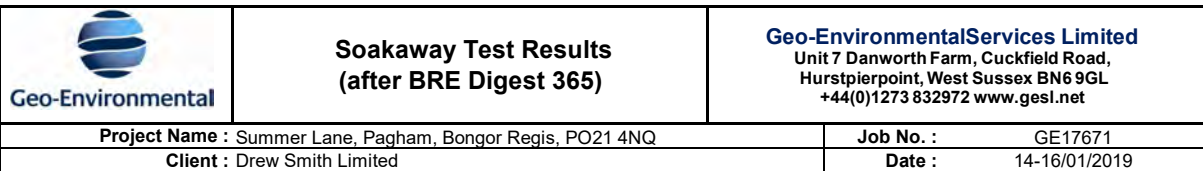
Test 2	
Time (min)	Depth (m)

Test 3	
Time (min)	Depth (m)



Max. depth (m)	1.50	1.50	1.50
Effective depth (m)	0.42	1.50	1.50
75% effective depth (m)	1.19	0.38	0.38
50% effective depth (m)	1.29	0.75	0.75
25% effective depth (m)	1.40	1.13	1.13
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.27	0.95	0.95
ap 50	2.462	5.54	5.54
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test

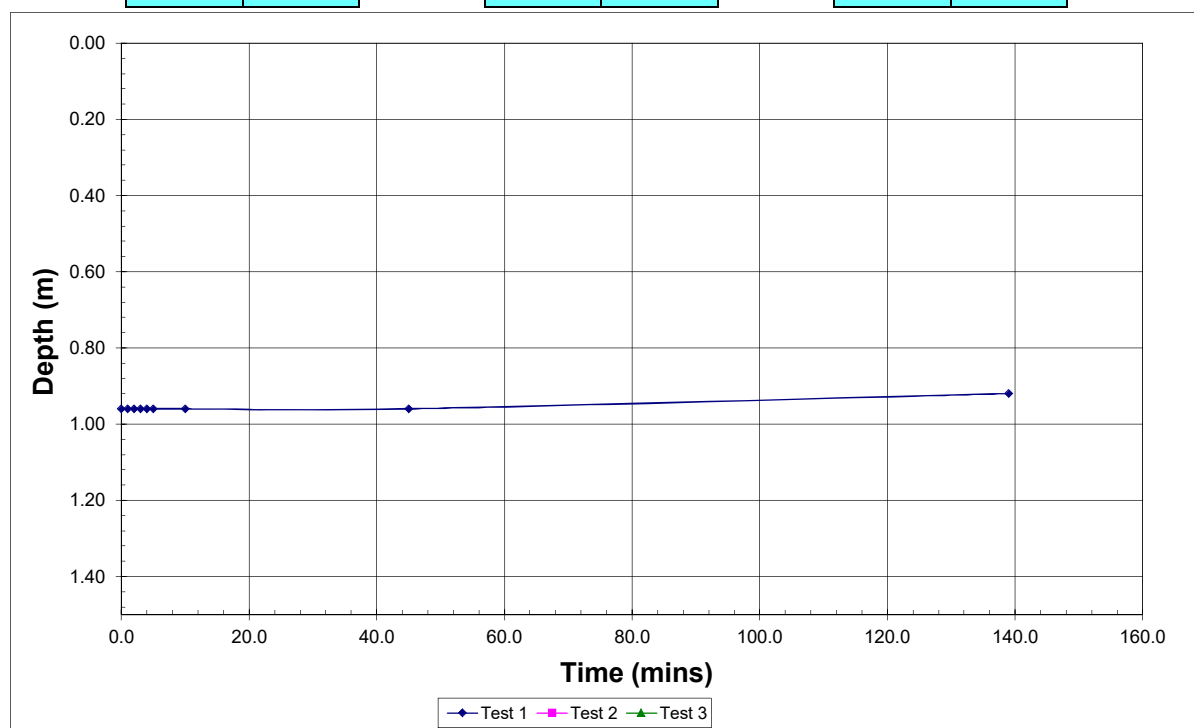


Geo-Environmental Services Limited
Unit 7 Danworth Farm, Cuckfield Road,
Hurstpierpoint, West Sussex BN6 9GL
+44(0)1273 832972 www.gesl.net

Job No. : GE17671

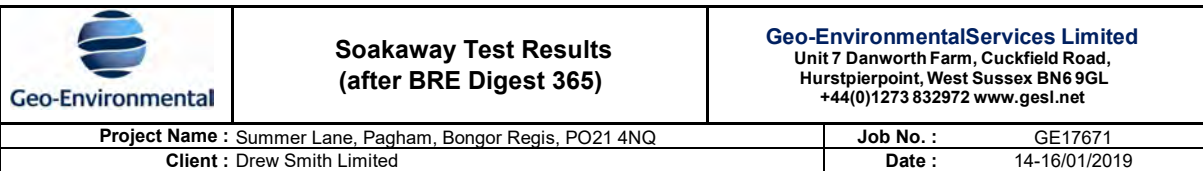
Date : 14-16/01/2019

Pit reference	TP04
Pit depth (m)	1.58
Pit width (m)	0.55
Pit length (m)	2.00
Depth to standing water (m)	

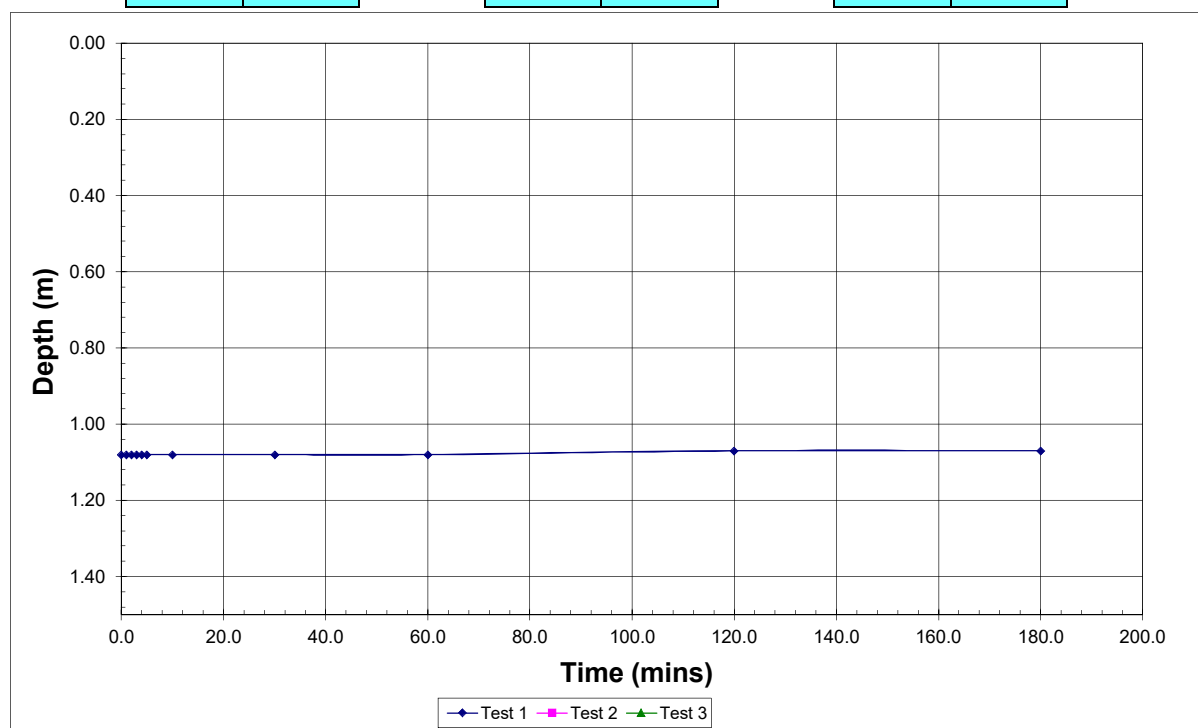
[illegible][illegible][illegible]

Max. depth (m)	1.58	1.58	1.58
Effective depth (m)	0.62	1.58	1.58
75% effective depth (m)	1.12	0.40	0.40
50% effective depth (m)	1.27	0.79	0.79
25% effective depth (m)	1.43	1.19	1.19
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.34	0.87	0.87
ap 50	2.681	5.129	5.129
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test



Pit reference	TP05
Pit depth (m)	1.52
Pit width (m)	0.55
Pit length (m)	1.80
Depth to standing water (m)	1.40

[illegible][illegible][illegible]

Max. depth (m)	1.52	1.52	1.52
Effective depth (m)	0.44	1.52	1.52
75% effective depth (m)	1.19	0.38	0.38
50% effective depth (m)	1.30	0.76	0.76
25% effective depth (m)	1.41	1.14	1.14
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.22	0.75	0.75
ap 50	2.024	4.562	4.562
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test

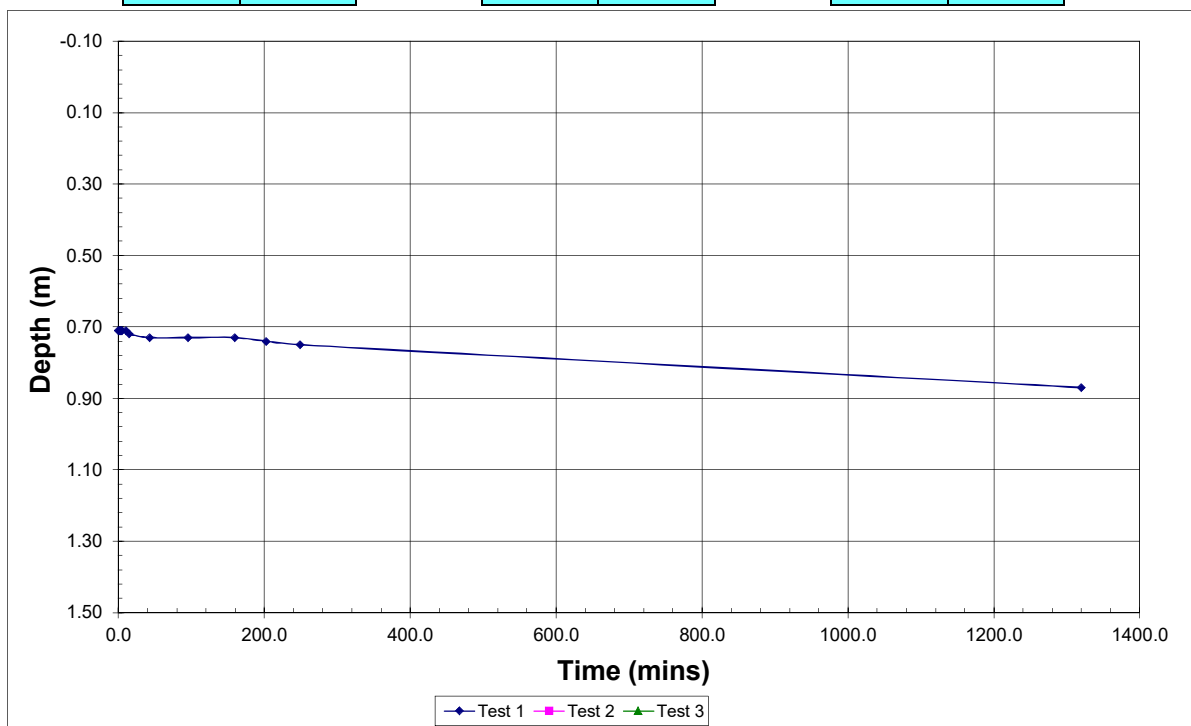
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP07
Pit depth (m)	1.42
Pit width (m)	0.55
Pit length (m)	2.00
Depth to standing water (m)	1.38

Test 1	
Time (min)	Depth (m)
0.0	0.71
1.0	0.71
2.0	0.71
3.0	0.71
4.0	0.71
5.0	0.71
10.0	0.71
15.0	0.72
43.0	0.73
95.0	0.73
159.0	0.73
202.0	0.74
249.0	0.75
1320.0	0.87

Test 2	
Time (min)	Depth (m)

Test 3	
Time (min)	Depth (m)



Max. depth (m)	1.42	1.42	1.42
Effective depth (m)	0.71	1.42	1.42
75% effective depth (m)	0.89	0.36	0.36
50% effective depth (m)	1.07	0.71	0.71
25% effective depth (m)	1.24	1.07	1.07
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.39	0.78	0.78
ap 50	2.9105	4.721	4.721
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test

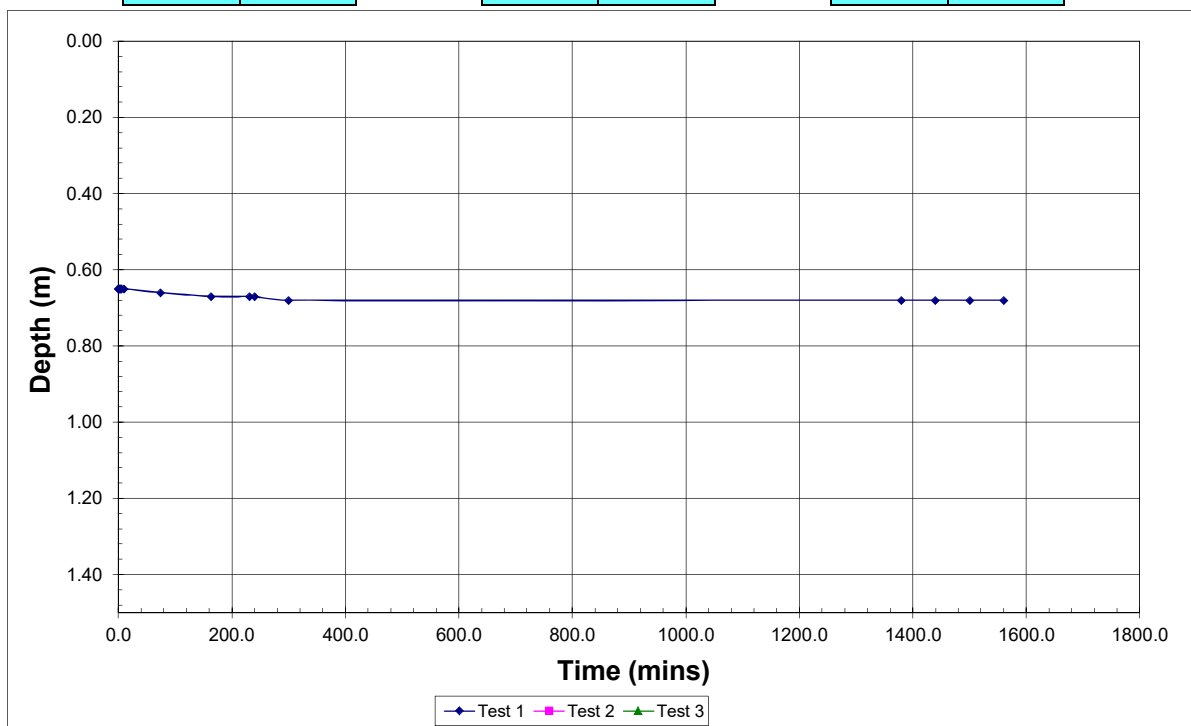
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP08
Pit depth (m)	1.40
Pit width (m)	0.55
Pit length (m)	2.00
Depth to standing water (m)	1.33

Test 1	
Time (min)	Depth (m)
0.0	0.65
1.0	0.65
2.0	0.65
3.0	0.65
4.0	0.65
5.0	0.65
10.0	0.65
74.0	0.66
163.0	0.67
231.0	0.67
240.0	0.67
300.0	0.68
1380.0	0.68
1440.0	0.68
1500.0	0.68
1560.0	0.68

Test 2	
Time (min)	Depth (m)

Test 3	
Time (min)	Depth (m)



Max. depth (m)	1.40	1.40	1.40
Effective depth (m)	0.75	1.40	1.40
75% effective depth (m)	0.84	0.35	0.35
50% effective depth (m)	1.03	0.70	0.70
25% effective depth (m)	1.21	1.05	1.05
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.41	0.77	0.77
ap 50	3.0125	4.67	4.67
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test

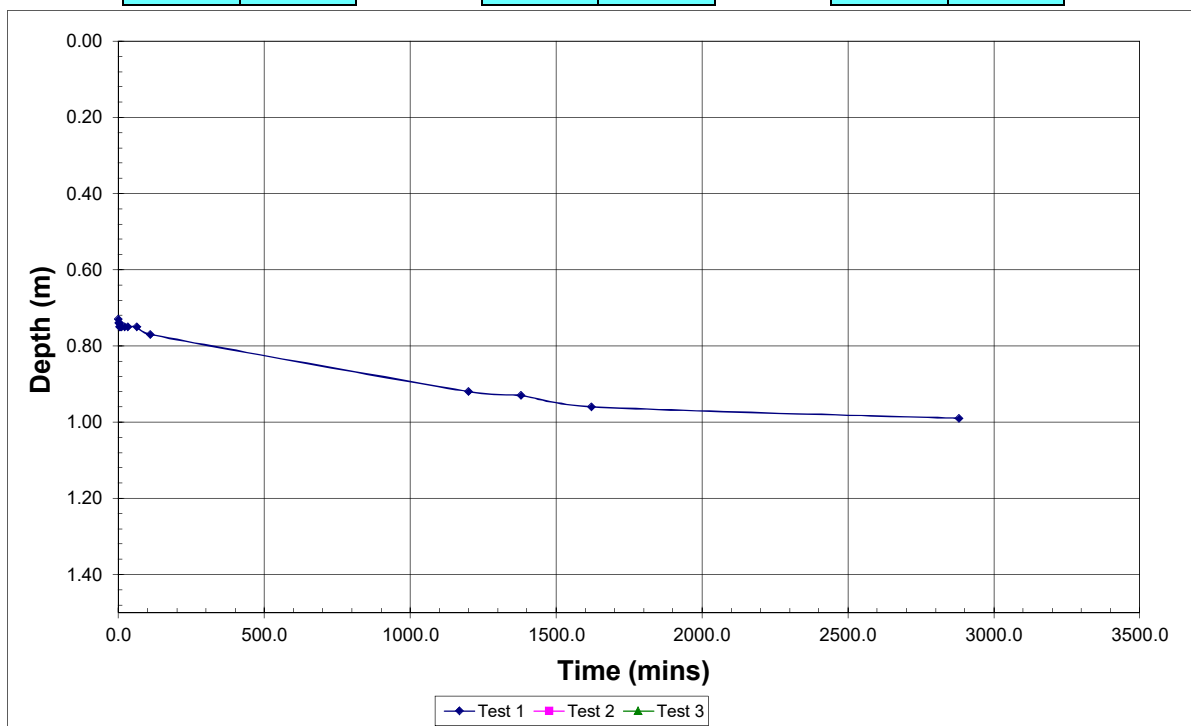
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP11
Pit depth (m)	1.50
Pit width (m)	0.55
Pit length (m)	2.00
Depth to standing water (m)	1.45

Test 1	
Time (min)	Depth (m)
0.0	0.73
1.0	0.74
2.0	0.74
3.0	0.74
4.0	0.75
5.0	0.75
10.0	0.75
20.0	0.75
33.0	0.75
62.0	0.75
108.0	0.77
1200.0	0.92
1380.0	0.93
1620.0	0.96
2880.0	0.99

Test 2	
Time (min)	Depth (m)

Test 3	
Time (min)	Depth (m)



Max. depth (m)	1.50	1.50	1.50
Effective depth (m)	0.77	1.50	1.50
75% effective depth (m)	0.92	0.38	0.38
50% effective depth (m)	1.12	0.75	0.75
25% effective depth (m)	1.31	1.13	1.13
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.42	0.83	0.83
ap 50	3.0635	4.925	4.925
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test

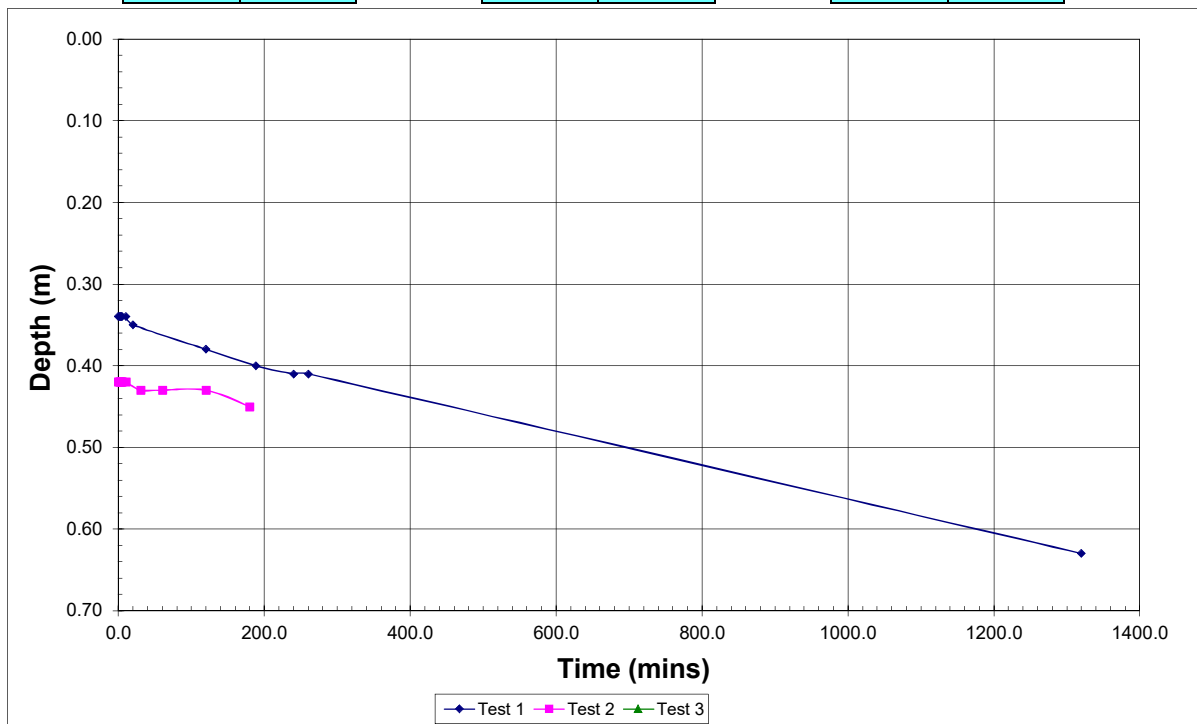
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP12
Pit depth (m)	0.63
Pit width (m)	0.55
Pit length (m)	1.30
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.34
1.0	0.34
2.0	0.34
3.0	0.34
4.0	0.34
5.0	0.34
10.0	0.34
20.0	0.35
120.0	0.38
188.0	0.40
240.0	0.41
260.0	0.41
1320.0	0.63

Test 2	
Time (min)	Depth (m)
0.0	0.42
1.0	0.42
2.0	0.42
3.0	0.42
4.0	0.42
5.0	0.42
10.0	0.42
30.0	0.43
60.0	0.43
120.0	0.43
180.0	0.45

Test 3	
Time (min)	Depth (m)



Max. depth (m)	0.63	0.63	0.63
Effective depth (m)	0.29	0.21	0.63
75% effective depth (m)	0.41	0.47	0.16
50% effective depth (m)	0.49	0.53	0.32
25% effective depth (m)	0.56	0.58	0.47
t75 (min)	260.00		
t50 (min)	640.00		
t25 (min)	980.00		
Vp 75-25	0.10	0.08	0.23
ap 50	1.2515	1.1035	1.8805
tp 75-25	720.00	0.00	0.00

Soil infiltration rate (m/s)	1.9E-06		
Soil infiltration rate (mm/hr)	6.90E+00		

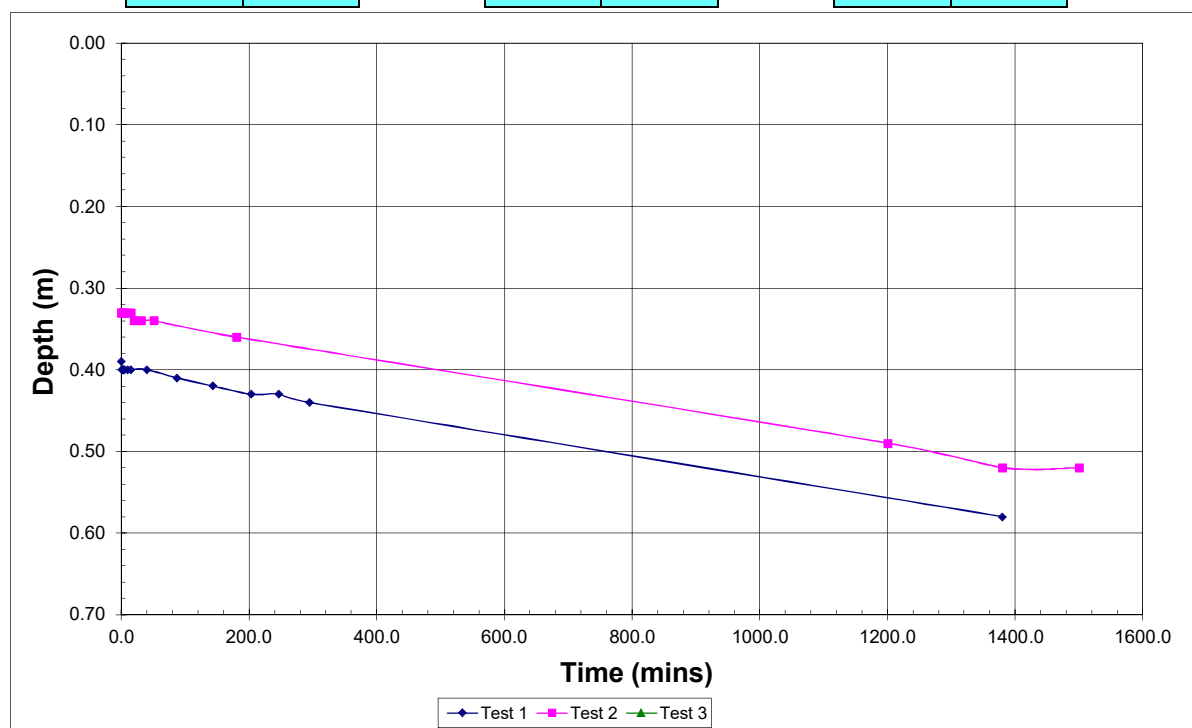
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesi.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP13
Pit depth (m)	0.70
Pit width (m)	0.55
Pit length (m)	2.00
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.39
1.0	0.40
2.0	0.40
3.0	0.40
4.0	0.40
5.0	0.40
10.0	0.40
15.0	0.40
40.0	0.40
87.0	0.41
143.0	0.42
203.0	0.43
246.0	0.43
294.0	0.44
1380.0	0.58

Test 2	
Time (min)	Depth (m)
0.0	0.33
1.0	0.33
2.0	0.33
3.0	0.33
4.0	0.33
5.0	0.33
10.0	0.33
15.0	0.33
20.0	0.34
31.0	0.34
51.0	0.34
180.0	0.36
1200.0	0.49
1380.0	0.52
1500.0	0.52

Test 3	
Time (min)	Depth (m)



Max. depth (m)	0.70	0.70	0.70
Effective depth (m)	0.31	0.37	0.70
75% effective depth (m)	0.47	0.42	0.18
50% effective depth (m)	0.55	0.52	0.35
25% effective depth (m)	0.62	0.61	0.53
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.17	0.20	0.39
ap 50	1.8905	2.0435	2.885
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test

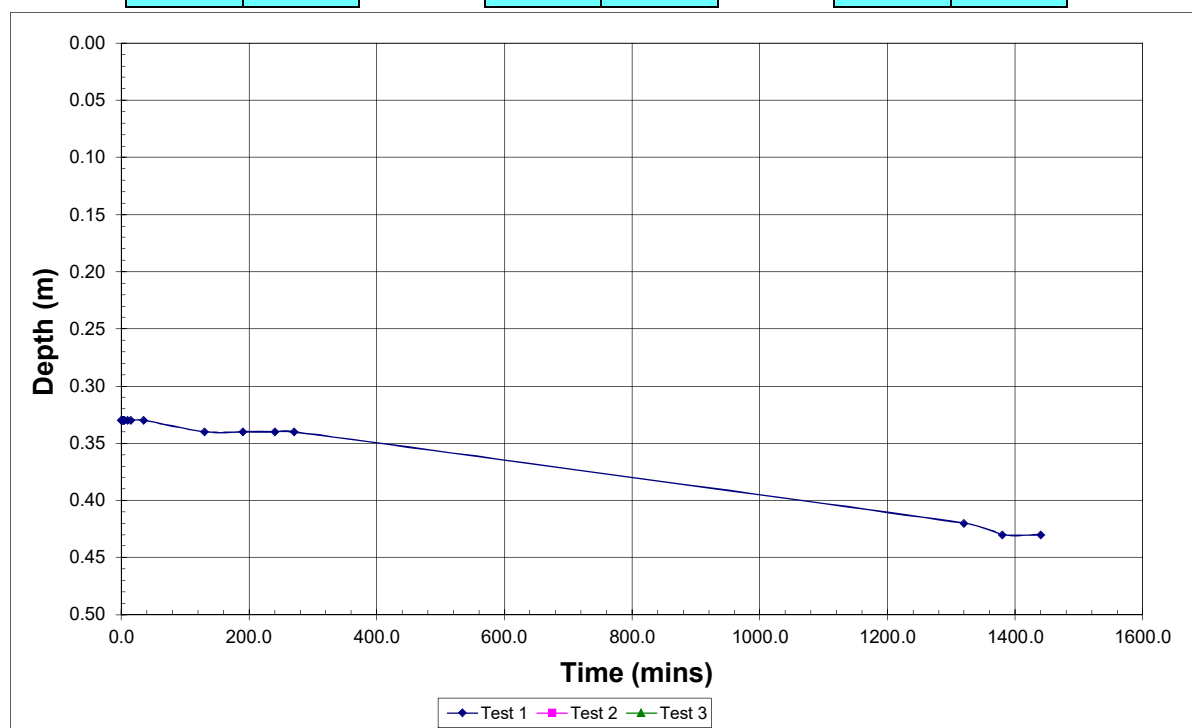
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP14
Pit depth (m)	0.60
Pit width (m)	0.55
Pit length (m)	1.40
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.33
1.0	0.33
2.0	0.33
3.0	0.33
4.0	0.33
5.0	0.33
10.0	0.33
15.0	0.33
35.0	0.33
130.0	0.34
190.0	0.34
240.0	0.34
270.0	0.34
1320.0	0.42
1380.0	0.43
1440.0	0.43

Test 2	
Time (min)	Depth (m)

Test 3	
Time (min)	Depth (m)



Max. depth (m)	0.60	0.60	0.60
Effective depth (m)	0.27	0.60	0.60
75% effective depth (m)	0.40	0.15	0.15
50% effective depth (m)	0.47	0.30	0.30
25% effective depth (m)	0.53	0.45	0.45
t75 (min)			
t50 (min)			
t25 (min)			
Vp 75-25	0.10	0.23	0.23
ap 50	1.2965	1.94	1.94
tp 75-25	0.00	0.00	0.00

Soil infiltration rate (m/s)	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	Insufficient fall in water to complete test

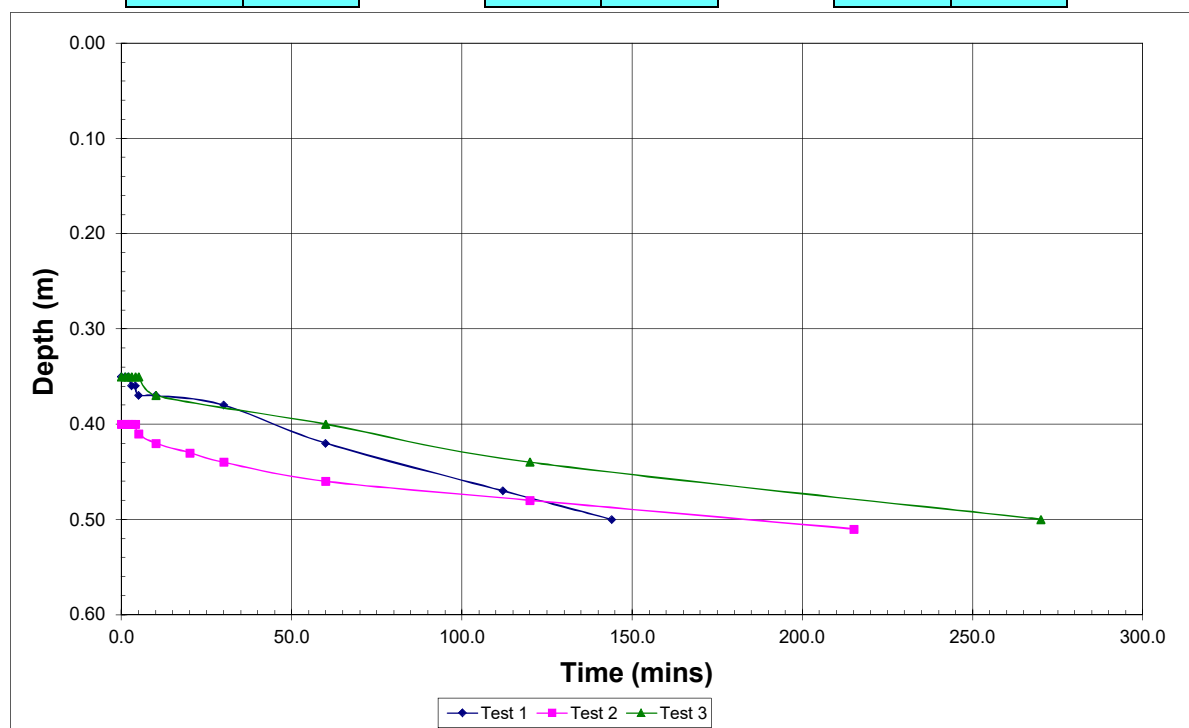
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP15
Pit depth (m)	0.55
Pit width (m)	0.55
Pit length (m)	1.40
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.35
1.0	0.35
2.0	0.35
3.0	0.36
4.0	0.36
5.0	0.37
10.0	0.37
30.0	0.38
60.0	0.42
112.0	0.47
144.0	0.50

Test 2	
Time (min)	Depth (m)
0.0	0.40
1.0	0.40
2.0	0.40
3.0	0.40
4.0	0.40
5.0	0.41
10.0	0.42
20.0	0.43
30.0	0.44
60.0	0.46
120.0	0.48
215.0	0.51

Test 3	
Time (min)	Depth (m)
0.0	0.35
1.0	0.35
2.0	0.35
3.0	0.35
4.0	0.35
5.0	0.35
10.0	0.37
60.0	0.40
120.0	0.44
270.0	0.50



Max. depth (m)	0.55	0.55	0.55
Effective depth (m)	0.20	0.15	0.20
75% effective depth (m)	0.40	0.44	0.40
50% effective depth (m)	0.45	0.48	0.45
25% effective depth (m)	0.50	0.51	0.50
t75 (min)	44.00	30.00	0.60
t50 (min)	90.00	120.00	145.00
t25 (min)	144.00	215.00	270.00
Vp 75-25	0.08	0.06	0.08
ap 50	1.16	1.0625	1.16
tp 75-25	100.00	185.00	269.40

Soil infiltration rate (m/s)	1.1E-05	4.9E-06	4.1E-06
Soil infiltration rate (mm/hr)	3.98E+01	1.76E+01	1.48E+01

Based on extrapolated data in red

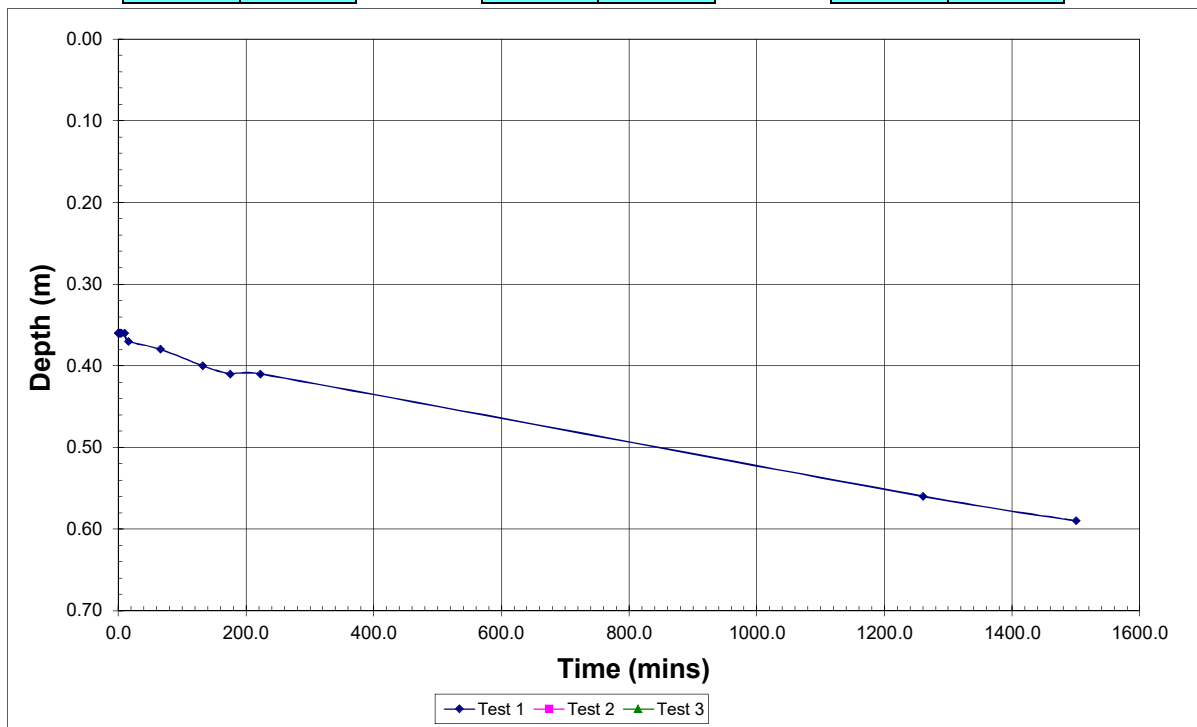
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP16
Pit depth (m)	0.67
Pit width (m)	0.55
Pit length (m)	1.50
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.36
1.0	0.36
2.0	0.36
3.0	0.36
4.0	0.36
5.0	0.36
10.0	0.36
16.0	0.37
66.0	0.38
132.0	0.40
175.0	0.41
222.0	0.41
1260.0	0.56
1500.0	0.59

Test 2	
Time (min)	Depth (m)

Test 3	
Time (min)	Depth (m)



Max. depth (m)	0.67	0.67	0.67
Effective depth (m)	0.31	0.67	0.67
75% effective depth (m)	0.44	0.17	0.17
50% effective depth (m)	0.52	0.34	0.34
25% effective depth (m)	0.59	0.50	0.50
t75 (min)	430.00		
t50 (min)	980.00		
t25 (min)	1500.00		
Vp 75-25	0.13	0.28	0.28
ap 50	1.4605	2.1985	2.1985
tp 75-25	1070.00	0.00	0.00

Soil infiltration rate (m/s)	1.4E-06		
Soil infiltration rate (mm/hr)	4.91E+00		

Based on extrapolated data in red

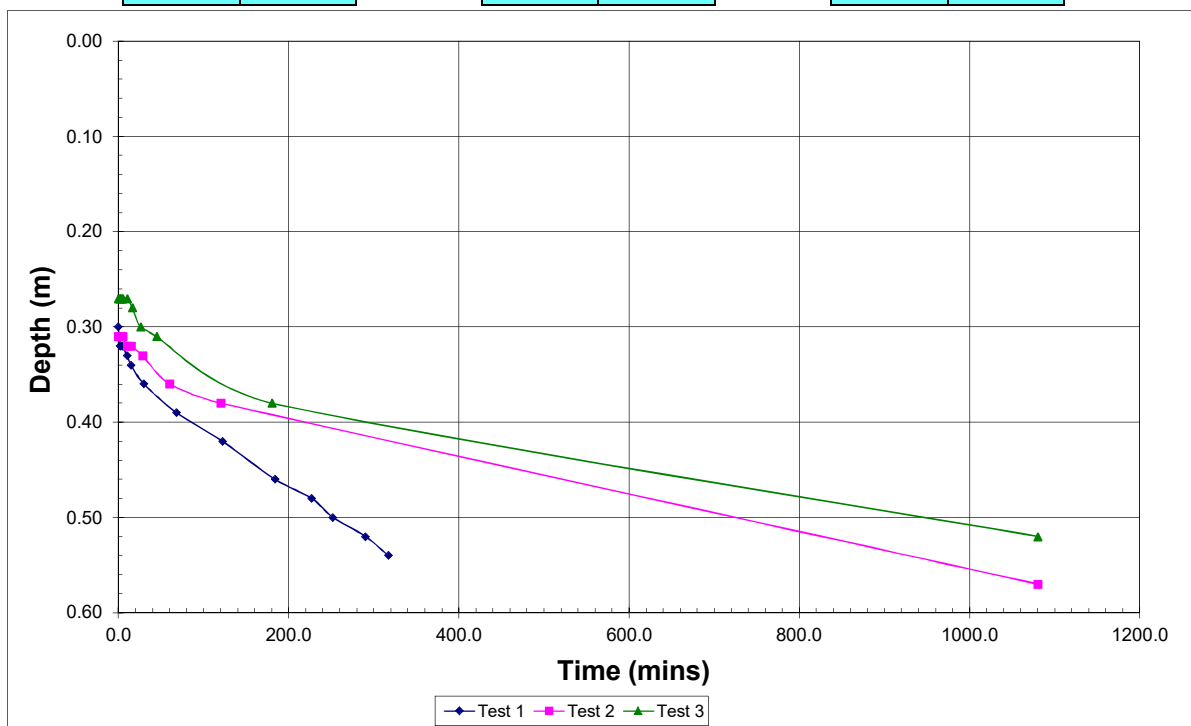
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP17
Pit depth (m)	0.60
Pit width (m)	0.55
Pit length (m)	1.20
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.30
1.0	0.31
2.0	0.32
3.0	0.32
4.0	0.32
5.0	0.32
10.0	0.33
15.0	0.34
30.0	0.36
68.0	0.39
122.0	0.42
184.0	0.46
227.0	0.48
252.0	0.50
290.0	0.52
317.0	0.54

Test 2	
Time (min)	Depth (m)
0.0	0.31
1.0	0.31
2.0	0.31
3.0	0.31
4.0	0.31
5.0	0.31
10.0	0.32
15.0	0.32
28.0	0.33
60.0	0.36
120.0	0.38
1080.0	0.57

Test 3	
Time (min)	Depth (m)
0.0	0.27
1.0	0.27
2.0	0.27
3.0	0.27
4.0	0.27
5.0	0.27
10.0	0.27
16.0	0.28
26.0	0.30
45.0	0.31
180.0	0.38
1080.0	0.52



Max. depth (m)	0.60	0.60	0.60
Effective depth (m)	0.30	0.29	0.33
75% effective depth (m)	0.38	0.38	0.35
50% effective depth (m)	0.45	0.46	0.44
25% effective depth (m)	0.53	0.53	0.52
t75 (min)	50.00	120.00	105.00
t50 (min)	163.00	520.00	540.00
t25 (min)	303.00	860.00	1080.00
Vp 75-25	0.10	0.10	0.11
ap 50	1.185	1.1675	1.2375
tp 75-25	253.00	740.00	975.00

Soil infiltration rate (m/s)	5.5E-06	1.8E-06	1.5E-06
Soil infiltration rate (mm/hr)	1.98E+01	6.65E+00	5.42E+00

Based on extrapolated data in red

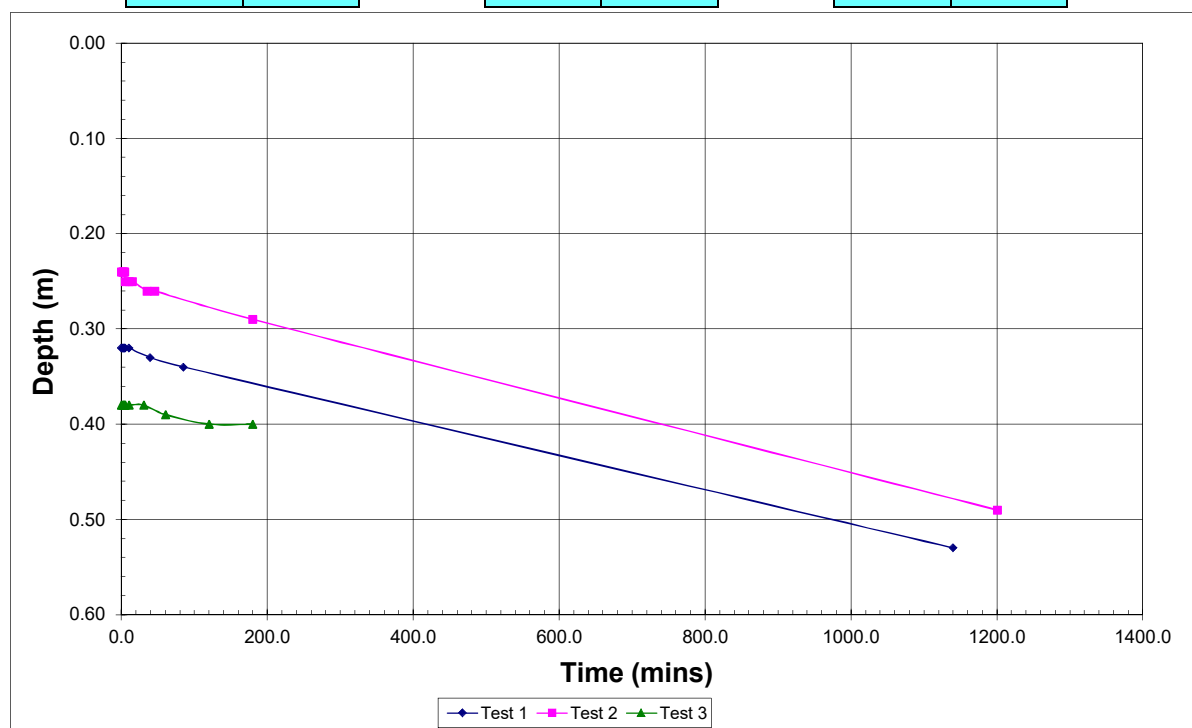
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP19
Pit depth (m)	0.55
Pit width (m)	0.55
Pit length (m)	1.90
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.32
1.0	0.32
2.0	0.32
3.0	0.32
4.0	0.32
5.0	0.32
10.0	0.32
39.0	0.33
85.0	0.34
1140.0	0.53

Test 2	
Time (min)	Depth (m)
0.0	0.24
1.0	0.24
2.0	0.24
3.0	0.24
4.0	0.24
5.0	0.25
10.0	0.25
15.0	0.25
35.0	0.26
45.0	0.26
180.0	0.29
1200.0	0.49

Test 3	
Time (min)	Depth (m)
0.0	0.38
1.0	0.38
2.0	0.38
3.0	0.38
4.0	0.38
5.0	0.38
10.0	0.38
30.0	0.38
60.0	0.39
120.0	0.40
180.0	0.40



Max. depth (m)	0.55	0.55	0.55
Effective depth (m)	0.23	0.31	0.17
75% effective depth (m)	0.38	0.32	0.42
50% effective depth (m)	0.44	0.40	0.47
25% effective depth (m)	0.49	0.47	0.51
t75 (min)	300.00	330.00	
t50 (min)	640.00	740.00	
t25 (min)	930.00	1100.00	
Vp 75-25	0.12	0.16	0.09
ap 50	1.6085	1.8045	1.4615
tp 75-25	630.00	770.00	0.00

Soil infiltration rate (m/s)	2.0E-06	1.9E-06	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	7.12E+00	6.99E+00	Insufficient fall in water to complete test

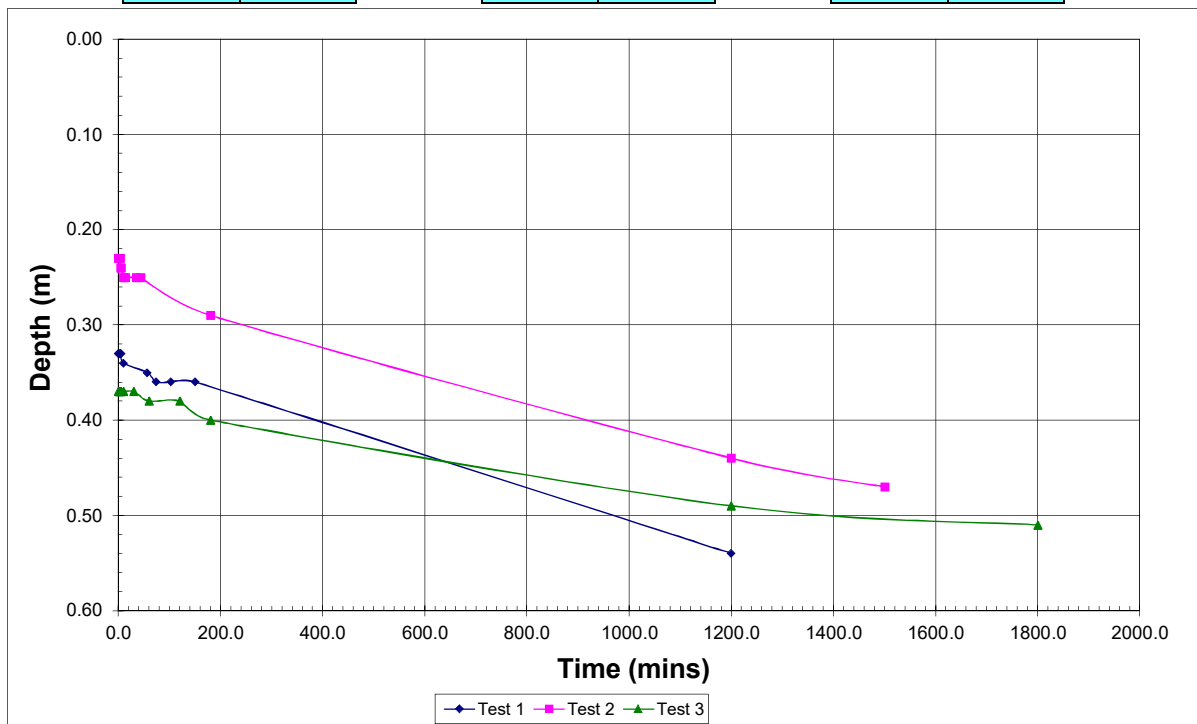
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP20
Pit depth (m)	0.55
Pit width (m)	0.55
Pit length (m)	1.60
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.33
1.0	0.33
2.0	0.33
3.0	0.33
4.0	0.33
5.0	0.33
10.0	0.34
56.0	0.35
74.0	0.36
102.0	0.36
150.0	0.36
1200.0	0.54

Test 2	
Time (min)	Depth (m)
0.0	0.23
1.0	0.23
2.0	0.23
3.0	0.23
4.0	0.24
5.0	0.24
10.0	0.25
13.0	0.25
35.0	0.25
43.0	0.25
180.0	0.29
1200.0	0.44
1500.0	0.47

Test 3	
Time (min)	Depth (m)
0.0	0.37
1.0	0.37
2.0	0.37
3.0	0.37
4.0	0.37
5.0	0.37
10.0	0.37
30.0	0.37
60.0	0.38
120.0	0.38
180.0	0.40
1200.0	0.49
1800.0	0.51



Max. depth (m)	0.55	0.55	0.55
Effective depth (m)	0.22	0.32	0.18
75% effective depth (m)	0.39	0.31	0.42
50% effective depth (m)	0.44	0.39	0.46
25% effective depth (m)	0.50	0.47	0.51
t75 (min)	270.00	380.00	400.00
t50 (min)	620.00	790.00	800.00
t25 (min)	970.00	1500.00	1500.00
Vp 75-25	0.10	0.14	0.08
ap 50	1.353	1.568	1.267
tp 75-25	700.00	1120.00	1100.00

Soil infiltration rate (m/s)	1.7E-06	1.3E-06	9.5E-07
Soil infiltration rate (mm/hr)	6.13E+00	4.81E+00	3.41E+00

Based on extrapolated data in red

Based on extrapolated data in red

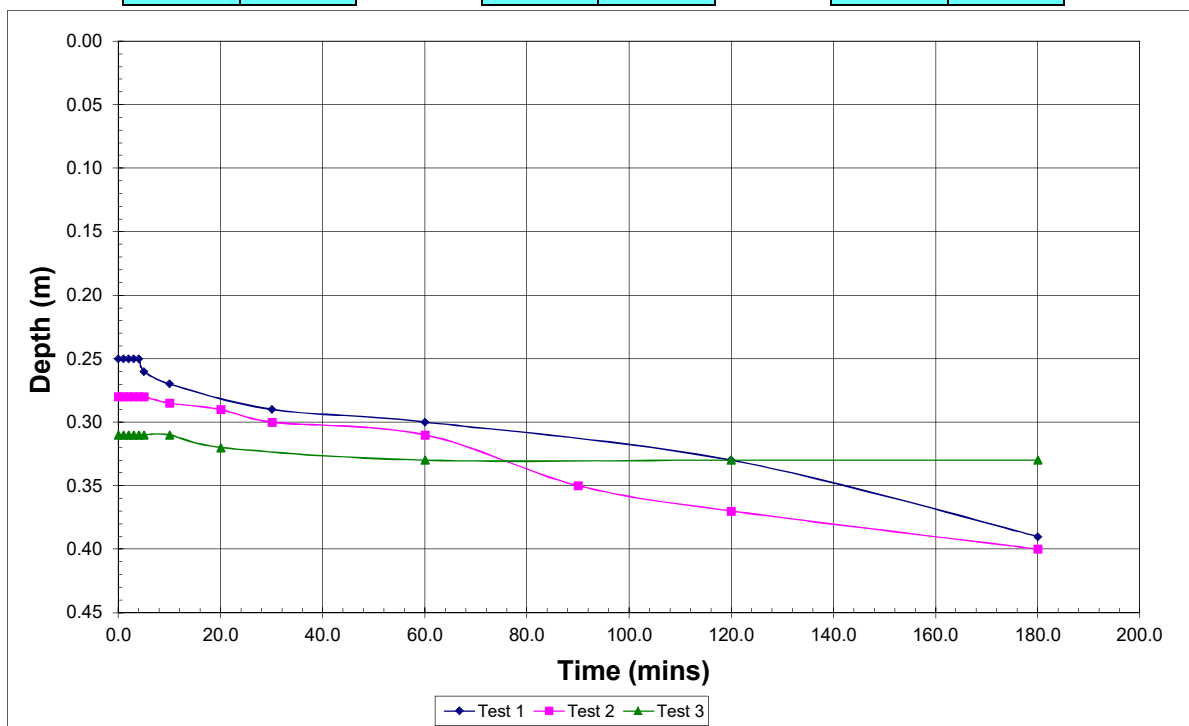
 Geo-Environmental	Soakaway Test Results (after BRE Digest 365)	Geo-Environmental Services Limited Unit 7 Danworth Farm, Cuckfield Road, Hurstpierpoint, West Sussex BN6 9GL +44(0)1273 832972 www.gesl.net
Project Name : Summer Lane, Pagham, Bongor Regis, PO21 4NQ		Job No. : GE17671
Client : Drew Smith Limited		Date : 14-16/01/2019

Pit reference	TP21
Pit depth (m)	0.44
Pit width (m)	0.55
Pit length (m)	1.40
Depth to standing water (m)	

Test 1	
Time (min)	Depth (m)
0.0	0.25
1.0	0.25
2.0	0.25
3.0	0.25
4.0	0.25
5.0	0.26
10.0	0.27
30.0	0.29
60.0	0.30
120.0	0.33
180.0	0.39

Test 2	
Time (min)	Depth (m)
0.0	0.28
1.0	0.28
2.0	0.28
3.0	0.28
4.0	0.28
5.0	0.28
10.0	0.29
20.0	0.29
30.0	0.30
60.0	0.31
90.0	0.35
120.0	0.37
180.0	0.40

Test 3	
Time (min)	Depth (m)
0.0	0.31
1.0	0.31
2.0	0.31
3.0	0.31
4.0	0.31
5.0	0.31
10.0	0.31
20.0	0.32
60.0	0.33
120.0	0.33
180.0	0.33



Max. depth (m)	0.44	0.44	0.44
Effective depth (m)	0.19	0.16	0.13
75% effective depth (m)	0.30	0.32	0.34
50% effective depth (m)	0.35	0.36	0.38
25% effective depth (m)	0.39	0.40	0.41
t75 (min)	60.00	76.00	
t50 (min)	142.00	100.00	
t25 (min)	180.00	180.00	
Vp 75-25	0.07	0.06	0.05
ap 50	1.1405	1.082	1.0235
tp 75-25	120.00	104.00	0.00

Soil infiltration rate (m/s)	8.9E-06	9.1E-06	Insufficient fall in water to complete test
Soil infiltration rate (mm/hr)	3.21E+01	3.28E+01	Insufficient fall in water to complete test

Appendix (C)
Proposed Site Layout

GENERAL NOTES:
1. This drawing is the copyright of Kenn Scaddan Associates Ltd and may not be copied, altered or reproduced in any form or passed on to a third party without written consent. If in doubt ASK.
2. The drawing reflects current standards and legislation agreed for this project at the time of original issue.

Schedule of Accommodation

WESTERN PARCEL - (44 units)

- 8no. 3 Bed Houses (TYPE A) 93m² - 97m²
- 2no. 4 Bed Houses (TYPE B) 122m²
- 4no. 2 Bed Houses (TYPE C) 79m²
- 7no. 3 Bed Houses (TYPE D) 102m² - 104m²
- 10no. 3 Bed Bungalows (TYPE F) 92m²
- 3no. 3 Bed Houses (TYPE G) 98m²

Sub Total - 34 Units

AR - Affordable Rent

- 2no. 3 Bed Houses (TYPE A) 93m² - 95m²
- 8no. 2 Bed Houses (TYPE C) 79m²

Sub Total - 10 Units

EASTERN PARCEL - (46 units)

- 4no. 3 Bed Houses (TYPE A) 93m² - 97m²
- 6no. 4 Bed Houses (TYPE B) 122m²
- 15no. 2 Bed Houses (TYPE C) 79m²
- 3no. 3 Bed Bungalows (TYPE E) 105m²
- 1no. 3 Bed Bungalows (TYPE F) 92m²

Sub Total - 29 Units

AR - Affordable Rent

- 17no. 2 Bed Houses (TYPE C) 79m²

Sub Total - 17 Units

P2	17.07.19	Boundary amended	CG	-
P1	10.07.19	Planning Issue	CG	-
REV	DATE	DESCRIPTION	REV BY	CKD BY

CLIENT

DREW SMITH GROUP



PROJECT
Land off Summer Lane
PAGHAM
West Sussex

DRAWING TITLE
Proposed Site Plan
90 Unit Scheme

DRAWING STATUS	SCALE
PLANNING	1:500 @ A1
PROJECT NO. DRAWING NO.	REVISION
1177 PD100	P2
	DRAWN BY
	CG



Appendix (D)

Existing Drainage Regime

Appendix (E)

Proposed Surface Water Strategy



NOTES

1. All dimensions are in metres unless stated otherwise.
2. Do not scale from this drawing. Only written dimensions are to be used.
3. Site layout based on Kenn Scaddan Associates Ltd site plan issued to RCP in DWG format on 17.07.2019.
4. Topographic Survey as per Siteline Level Survey, drawing number 657PG01 dated July 2012.
5. Additional topographic Survey as per ADA Solutions Ltd Topographical Survey, drawing number 0614-HP2-T1 dated June 2014.
6. Ditch survey based on Siteline Ditch Level Survey drawing number 657PG05 dated 30.01.19
7. The current surface water drainage proposals only show primary SW drainage runs. An allowance must be made for secondary drainage which is all subject to design development

KEY

- Red Line Boundary as per Outline Application
- Permeable Paving
- Proposed Surface Water Network
- Proposed outfall headwall

SCALE BAR 1:500 at A1

© Crown copyright. All rights reserved. Licence number 100042156

Rev.	Date	Details	By	Chkd	Appd
E	17.07.19	Update to latest site layout	TRS	TRS	TRS
D	11.07.19	Update to latest site layout	TRS	TRS	TRS
C	10.07.19	Update to latest site layout	TRS	TRS	TRS
B	03.07.19	Update to latest site layout	TRS	TRS	TRS
A	02.07.19	Update to latest site layout	TRS	TRS	TRS

Client:-

DREW SMITH LIMITED

Site:-
SUMMER LANE
PAGHAM

Drawing Title:-
DRAINAGE
STRATEGY
LAYOUT

Date: February 2019
Drawn: KK
Checked: SRV
Scales: 1:500 at A1
Approved: TRS

Drawing No. DSM/E4761/001E

FOR INFORMATION ONLY



Rogers Cory Partnership
Architectural and Civil Consultants
The Old School Old School Road
Hook Hampshire RG27 9NJ

T: 01256 769269 E: mail@rcpconsultants.co.uk W: rcpconsultants.co.uk

Appendix (F)

Micro Drainage Calculations

Rogers Cory Partnership		Page 0
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		

STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for SW-1.SWS

Pipe Sizes SW-1 Manhole Sizes SW-1

FSR Rainfall Model - England and Wales

Return Period (years)	2	PIMP (%)	100
M5-60 (mm)	19.000	Add Flow / Climate Change (%)	10
Ratio R	0.350	Minimum Backdrop Height (m)	0.200
Maximum Rainfall (mm/hr)	50	Maximum Backdrop Height (m)	0.000
Maximum Time of Concentration (mins)	30	Min Design Depth for Optimisation (m)	1.200
Foul Sewage (l/s/ha)	0.000	Min Vel for Auto Design only (m/s)	0.75
Volumetric Runoff Coeff.	0.750	Min Slope for Optimisation (1:X)	500

Designed with Level Soffits

Network Design Table for SW-1.SWS

« - Indicates pipe capacity < flow

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	n	HYD SECT	DIA (mm)	Section Type	Auto Design
S1.000	30.250	0.178	169.9	0.141	5.00	0.0	0.600		o	300	Pipe/Conduit	
S2.000	19.464	0.380	51.2	0.078	5.00	0.0	0.600		o	225	Pipe/Conduit	
S1.001	35.964	0.147	244.7	0.054	0.00	0.0	0.600		o	375	Pipe/Conduit	
S1.002	19.565	0.080	244.6	0.104	0.00	0.0	0.600		o	375	Pipe/Conduit	
S3.000	24.269	0.143	169.7	0.066	5.00	0.0	0.600		o	225	Pipe/Conduit	
S4.000	25.210	0.148	170.3	0.057	5.00	0.0	0.600		o	225	Pipe/Conduit	

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
S1.000	50.00	5.42	4.412	0.141	0.0	0.0	1.9	1.20	85.0	21.0
S2.000	50.00	5.18	4.614	0.078	0.0	0.0	1.1	1.83	72.8	11.6
S1.001	50.00	5.94	4.309	0.273	0.0	0.0	3.7	1.15	127.4	40.7
S1.002	50.00	6.22	4.162	0.377	0.0	0.0	5.1	1.15	127.5	56.2
S3.000	50.00	5.40	4.445	0.066	0.0	0.0	0.9	1.00	39.8	9.8
S4.000	50.00	5.42	4.300	0.057	0.0	0.0	0.8	1.00	39.7	8.5

©1982-2017 XP Solutions

Rogers Cory Partnership											Page 1	
The Old School Old School Road Hook Hampshire RG27 9NJ						Summer Lane Pagham						
Date 25/06/2019 15:38						Designed by Terry Seymour						
File SW1-with Crayfern site.MDX						Checked by Terry Seymour						
Innovyze						Network 2017.1.2						
<u>Network Design Table for SW-1.SWS</u>												
PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	n	HYD SECT	DIA (mm)	Section Type	Auto Design
S1.003	36.592	0.113	323.8	0.079	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.004	12.233	0.030	407.8	0.095	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.005	8.977	0.022	408.0	0.007	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.006	18.565	0.046	403.6	0.007	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.007	31.963	0.079	404.6	0.041	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.008	13.143	0.032	410.7	0.080	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.009	6.866	0.017	403.9	0.000	0.00	0.0	0.600		o	450	Pipe/Conduit	
S5.000	10.000	0.040	250.0	0.260	5.00	0.0	0.600		o	300	Pipe/Conduit	
S5.001	5.000	0.020	250.0	0.000	0.00	0.0	0.600		o	300	Pipe/Conduit	
S1.010	43.627	0.087	501.5	0.000	0.00	0.0	0.600		1 _ /	525	1:1 Ditch	
S6.000	10.000	0.040	250.0	0.150	5.00	0.0	0.600		1 _ /	300	1:1 Ditch	
S6.001	5.000	0.020	250.0	0.000	0.00	0.0	0.600		1 _ /	300	1:1 Ditch	
S1.011	5.353	0.011	486.6	0.000	0.00	0.0	0.600		1 _ /	525	1:1 Ditch	
S1.012	17.096	0.034	502.8	0.000	0.00	0.0	0.600		1 _ /	525	1:1 Ditch	
S1.013	13.810	0.028	493.2	0.000	0.00	0.0		0.045	o	525	Pipe/Conduit	
S1.014	6.683	0.013	514.1	0.000	0.00	0.0		0.045	1 _ /	525	1:1 Ditch	
S1.015	4.615	0.009	512.8	0.000	0.00	0.0	0.600		o	525	Pipe/Conduit	
S1.016	27.468	0.055	499.4	0.000	0.00	0.0	0.600		1 _ /	525	1:1 Ditch	
<u>Network Results Table</u>												
PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)		
S1.003	50.00	6.76	3.932	0.579		0.0	0.0	7.8	1.12	178.8	86.2	
S1.004	50.00	6.97	3.744	0.674		0.0	0.0	9.1	1.00	159.1	100.4	
S1.005	50.00	7.12	3.714	0.681		0.0	0.0	9.2	1.00	159.1	101.4	
S1.006	50.00	7.42	3.692	0.688		0.0	0.0	9.3	1.01	160.0	102.5	
S1.007	50.00	7.95	3.646	0.729		0.0	0.0	9.9	1.00	159.8	108.6	
S1.008	50.00	8.17	3.567	0.809		0.0	0.0	11.0	1.00	158.5	120.5	
S1.009	49.71	8.29	3.535	0.809		0.0	0.0	11.0	1.01	159.9	120.5	
S5.000	50.00	5.17	4.000	0.260		0.0	0.0	3.5	0.99	70.0	38.7	
S5.001	50.00	5.25	3.960	0.260		0.0	0.0	3.5	0.99	70.0	38.7	
S1.010	48.39	8.75	3.443	1.069		0.0	0.0	14.0	1.57	867.7	154.1	
S6.000	50.00	5.11	4.000	0.150		0.0	0.0	2.0	1.58	284.1	22.3	
S6.001	50.00	5.16	3.960	0.150		0.0	0.0	2.0	1.58	284.1	22.3	
S1.011	48.24	8.81	3.356	1.219		0.0	0.0	15.9	1.60	881.0	175.2	
S1.012	47.75	8.99	3.345	1.219		0.0	0.0	15.9	1.57	866.6	175.2	
S1.013	45.51	9.88	3.311	1.219		0.0	0.0	15.9	0.26	55.9	175.2	
S1.014	44.88	10.15	3.283	1.219		0.0	0.0	15.9	0.41	228.1	175.2	
S1.015	44.70	10.23	3.270	1.219		0.0	0.0	15.9	0.98	212.6	175.2	
S1.016	44.05	10.52	3.261	1.219		0.0	0.0	15.9	1.58	869.5	175.2	
©1982-2017 XP Solutions												

Rogers Cory Partnership											Page 2	
The Old School Old School Road Hook Hampshire RG27 9NJ					Summer Lane Pagham							
Date 25/06/2019 15:38					Designed by Terry Seymour							
File SW1-with Crayfern site.MDX					Checked by Terry Seymour							
Innovyze					Network 2017.1.2							
<u>Network Design Table for SW-1.SWS</u>												
PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	n	HYD SECT	DIA (mm)	Section Type	Auto Design
S1.017	70.410	0.141	499.4	0.087	0.00	0.0	0.600	1	_/_	525	1:1 Ditch	
S7.000	37.874	0.223	169.8	0.067	5.00	0.0	0.600		o	225	Pipe/Conduit	
S7.001	13.335	0.078	171.0	0.039	0.00	0.0	0.600		o	225	Pipe/Conduit	
S7.002	15.006	0.088	170.5	0.000	0.00	0.0	0.600		o	225	Pipe/Conduit	
S7.003	47.205	0.193	244.6	0.085	0.00	0.0	0.600		o	300	Pipe/Conduit	
S8.000	46.917	0.456	102.9	0.137	5.00	0.0	0.600		o	300	Pipe/Conduit	
S7.004	37.876	0.117	323.7	0.114	0.00	0.0	0.600		o	375	Pipe/Conduit	
S7.005	18.226	0.045	405.0	0.183	0.00	0.0	0.600		o	450	Pipe/Conduit	
S7.006	10.518	0.027	389.6	0.000	0.00	0.0	0.600		o	450	Pipe/Conduit	
S9.000	13.486	0.079	170.7	0.020	5.00	0.0	0.600		o	225	Pipe/Conduit	
S9.001	18.636	0.110	169.4	0.062	0.00	0.0	0.600		o	225	Pipe/Conduit	
S9.002	13.429	0.143	93.9	0.026	0.00	0.0	0.600		o	225	Pipe/Conduit	
S7.007	15.587	0.031	502.8	0.000	0.00	0.0	0.600	1	_/_	525	1:1 Ditch	
S7.008	13.290	0.027	492.2	0.000	0.00	0.0	0.600		o	525	Pipe/Conduit	
S7.009	5.199	0.013	399.9	0.000	0.00	0.0	0.600		o	525	Pipe/Conduit	
S7.010	6.968	0.017	409.9	0.000	0.00	0.0	0.600		o	525	Pipe/Conduit	
<u>Network Results Table</u>												
PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)		
S1.017	42.49	11.26	3.206	1.306		0.0	0.0	15.9	1.58	869.6	175.2	
S7.000	50.00	5.63	4.167	0.067		0.0	0.0	0.9	1.00	39.8	10.0	
S7.001	50.00	5.85	3.944	0.106		0.0	0.0	1.4	1.00	39.6	15.8	
S7.002	50.00	6.10	3.866	0.106		0.0	0.0	1.4	1.00	39.7	15.8	
S7.003	50.00	6.89	3.703	0.191		0.0	0.0	2.6	1.00	70.7	28.5	
S8.000	50.00	5.50	4.000	0.137		0.0	0.0	1.9	1.55	109.6	20.4	
S7.004	50.00	7.52	3.435	0.442		0.0	0.0	6.0	1.00	110.6	65.8	
S7.005	50.00	7.82	3.243	0.625		0.0	0.0	8.5	1.00	159.7	93.1	
S7.006	50.00	7.99	3.198	0.625		0.0	0.0	8.5	1.02	162.9	93.1	
S9.000	50.00	5.23	3.728	0.020		0.0	0.0	0.3	1.00	39.7	3.0	
S9.001	50.00	5.54	3.649	0.082		0.0	0.0	1.1	1.00	39.8	12.2	
S9.002	50.00	5.70	3.539	0.108		0.0	0.0	1.5	1.35	53.7	16.1	
S7.007	50.00	8.16	3.096	0.733		0.0	0.0	9.9	1.57	866.6	109.2	
S7.008	49.44	8.38	3.065	0.733		0.0	0.0	9.9	1.00	217.1	109.2	
S7.009	49.21	8.46	3.038	0.733		0.0	0.0	9.9	1.11	241.1	109.2	
S7.010	48.91	8.56	3.025	0.733		0.0	0.0	9.9	1.10	238.1	109.2	
©1982-2017 XP Solutions												

Rogers Cory Partnership										Page 3	
The Old School Old School Road Hook Hampshire RG27 9NJ						Summer Lane Pagham					
Date 25/06/2019 15:38						Designed by Terry Seymour					
File SW1-with Crayfern site.MDX						Checked by Terry Seymour					
Innovyze						Network 2017.1.2					
<u>Network Design Table for SW-1.SWS</u>											
PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	n	HYD SECT	DIA (mm)	Section Type
S1.018	38.980	0.078	499.7	0.000	0.00	0.0	0.600		1 _/_	525	1:1 Ditch
S1.019	48.609	0.111	437.9	0.000	0.00	0.0	0.600		1 _/_	525	1:1 Ditch
S10.000	15.057	0.089	169.2	0.046	5.00	0.0	0.600		o	225	Pipe/Conduit
S10.001	12.781	0.093	137.4	0.031	0.00	0.0	0.600		o	225	Pipe/Conduit
S1.020	14.254	0.036	396.0	0.000	0.00	0.0	0.600		1 _/_	525	1:1 Ditch
S11.000	19.401	0.048	404.2	0.120	5.00	0.0		0.045	o	450	Pipe/Conduit
S1.021	2.098	0.029	72.4	0.000	0.00	0.0		0.045	1 _/_	525	1:1 Ditch
S1.022	27.502	0.006	4583.7	0.000	0.00	0.0		0.045	o	600	Pipe/Conduit
<u>Network Results Table</u>											
PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)	
S1.018	41.69	11.67	3.065	2.039	0.0	0.0	23.0	1.58	869.2	253.3	
S1.019	40.81	12.15	2.987	2.039	0.0	0.0	23.0	1.69	929.0	253.3	
S10.000	50.00	5.25	3.318	0.046	0.0	0.0	0.6	1.00	39.9	6.9	
S10.001	50.00	5.44	3.229	0.077	0.0	0.0	1.0	1.11	44.3	11.5	
S1.020	40.57	12.29	2.876	2.116	0.0	0.0	23.2	1.77	977.4	255.7	
S11.000	50.00	6.26	3.467	0.120	0.0	0.0	1.6	0.26	41.0	17.9	
S1.021	40.51	12.32	2.840	2.236	0.0	0.0	24.5	1.10	607.9	269.9	
S1.022	33.57	17.26	2.803	2.236	0.0	0.0	24.5	0.09	26.2«	269.9	
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Outfall Pipe Number	Outfall Name	C. Level (m)	I. Level (m)	Min I. Level (m)	D,L (mm)	W (mm)					
S1.022	SW-1	3.450	2.797	2.851	0	0					
Datum (m) 0.000 Offset (mins) 0											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
1	4.080	5	4.080	9	4.080	13	4.080	17	4.080	21	4.080
2	4.080	6	4.080	10	4.080	14	4.080	18	4.080	22	4.080
3	4.080	7	4.080	11	4.080	15	4.080	19	4.080	23	4.080
4	4.080	8	4.080	12	4.080	16	4.080	20	4.080	24	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership								Page 4	
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
25	4.080	75	4.080	125	4.080	175	4.080	225	4.080
26	4.080	76	4.080	126	4.080	176	4.080	226	4.080
27	4.080	77	4.080	127	4.080	177	4.080	227	4.080
28	4.080	78	4.080	128	4.080	178	4.080	228	4.080
29	4.080	79	4.080	129	4.080	179	4.080	229	4.080
30	4.080	80	4.080	130	4.080	180	4.080	230	4.080
31	4.080	81	4.080	131	4.080	181	4.080	231	4.080
32	4.080	82	4.080	132	4.080	182	4.080	232	4.080
33	4.080	83	4.080	133	4.080	183	4.080	233	4.080
34	4.080	84	4.080	134	4.080	184	4.080	234	4.080
35	4.080	85	4.080	135	4.080	185	4.080	235	4.080
36	4.080	86	4.080	136	4.080	186	4.080	236	4.080
37	4.080	87	4.080	137	4.080	187	4.080	237	4.080
38	4.080	88	4.080	138	4.080	188	4.080	238	4.080
39	4.080	89	4.080	139	4.080	189	4.080	239	4.080
40	4.080	90	4.080	140	4.080	190	4.080	240	4.080
41	4.080	91	4.080	141	4.080	191	4.080	241	4.080
42	4.080	92	4.080	142	4.080	192	4.080	242	4.080
43	4.080	93	4.080	143	4.080	193	4.080	243	4.080
44	4.080	94	4.080	144	4.080	194	4.080	244	4.080
45	4.080	95	4.080	145	4.080	195	4.080	245	4.080
46	4.080	96	4.080	146	4.080	196	4.080	246	4.080
47	4.080	97	4.080	147	4.080	197	4.080	247	4.080
48	4.080	98	4.080	148	4.080	198	4.080	248	4.080
49	4.080	99	4.080	149	4.080	199	4.080	249	4.080
50	4.080	100	4.080	150	4.080	200	4.080	250	4.080
51	4.080	101	4.080	151	4.080	201	4.080	251	4.080
52	4.080	102	4.080	152	4.080	202	4.080	252	4.080
53	4.080	103	4.080	153	4.080	203	4.080	253	4.080
54	4.080	104	4.080	154	4.080	204	4.080	254	4.080
55	4.080	105	4.080	155	4.080	205	4.080	255	4.080
56	4.080	106	4.080	156	4.080	206	4.080	256	4.080
57	4.080	107	4.080	157	4.080	207	4.080	257	4.080
58	4.080	108	4.080	158	4.080	208	4.080	258	4.080
59	4.080	109	4.080	159	4.080	209	4.080	259	4.080
60	4.080	110	4.080	160	4.080	210	4.080	260	4.080
61	4.080	111	4.080	161	4.080	211	4.080	261	4.080
62	4.080	112	4.080	162	4.080	212	4.080	262	4.080
63	4.080	113	4.080	163	4.080	213	4.080	263	4.080
64	4.080	114	4.080	164	4.080	214	4.080	264	4.080
65	4.080	115	4.080	165	4.080	215	4.080	265	4.080
66	4.080	116	4.080	166	4.080	216	4.080	266	4.080
67	4.080	117	4.080	167	4.080	217	4.080	267	4.080
68	4.080	118	4.080	168	4.080	218	4.080	268	4.080
69	4.080	119	4.080	169	4.080	219	4.080	269	4.080
70	4.080	120	4.080	170	4.080	220	4.080	270	4.080
71	4.080	121	4.080	171	4.080	221	4.080	271	4.080
72	4.080	122	4.080	172	4.080	222	4.080	272	4.080
73	4.080	123	4.080	173	4.080	223	4.080	273	4.080
74	4.080	124	4.080	174	4.080	224	4.080	274	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 5	
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
325	4.080	375	4.080	425	4.080	475	4.080	525	4.080
326	4.080	376	4.080	426	4.080	476	4.080	526	4.080
327	4.080	377	4.080	427	4.080	477	4.080	527	4.080
328	4.080	378	4.080	428	4.080	478	4.080	528	4.080
329	4.080	379	4.080	429	4.080	479	4.080	529	4.080
330	4.080	380	4.080	430	4.080	480	4.080	530	4.080
331	4.080	381	4.080	431	4.080	481	4.080	531	4.080
332	4.080	382	4.080	432	4.080	482	4.080	532	4.080
333	4.080	383	4.080	433	4.080	483	4.080	533	4.080
334	4.080	384	4.080	434	4.080	484	4.080	534	4.080
335	4.080	385	4.080	435	4.080	485	4.080	535	4.080
336	4.080	386	4.080	436	4.080	486	4.080	536	4.080
337	4.080	387	4.080	437	4.080	487	4.080	537	4.080
338	4.080	388	4.080	438	4.080	488	4.080	538	4.080
339	4.080	389	4.080	439	4.080	489	4.080	539	4.080
340	4.080	390	4.080	440	4.080	490	4.080	540	4.080
341	4.080	391	4.080	441	4.080	491	4.080	541	4.080
342	4.080	392	4.080	442	4.080	492	4.080	542	4.080
343	4.080	393	4.080	443	4.080	493	4.080	543	4.080
344	4.080	394	4.080	444	4.080	494	4.080	544	4.080
345	4.080	395	4.080	445	4.080	495	4.080	545	4.080
346	4.080	396	4.080	446	4.080	496	4.080	546	4.080
347	4.080	397	4.080	447	4.080	497	4.080	547	4.080
348	4.080	398	4.080	448	4.080	498	4.080	548	4.080
349	4.080	399	4.080	449	4.080	499	4.080	549	4.080
350	4.080	400	4.080	450	4.080	500	4.080	550	4.080
351	4.080	401	4.080	451	4.080	501	4.080	551	4.080
352	4.080	402	4.080	452	4.080	502	4.080	552	4.080
353	4.080	403	4.080	453	4.080	503	4.080	553	4.080
354	4.080	404	4.080	454	4.080	504	4.080	554	4.080
355	4.080	405	4.080	455	4.080	505	4.080	555	4.080
356	4.080	406	4.080	456	4.080	506	4.080	556	4.080
357	4.080	407	4.080	457	4.080	507	4.080	557	4.080
358	4.080	408	4.080	458	4.080	508	4.080	558	4.080
359	4.080	409	4.080	459	4.080	509	4.080	559	4.080
360	4.080	410	4.080	460	4.080	510	4.080	560	4.080
361	4.080	411	4.080	461	4.080	511	4.080	561	4.080
362	4.080	412	4.080	462	4.080	512	4.080	562	4.080
363	4.080	413	4.080	463	4.080	513	4.080	563	4.080
364	4.080	414	4.080	464	4.080	514	4.080	564	4.080
365	4.080	415	4.080	465	4.080	515	4.080	565	4.080
366	4.080	416	4.080	466	4.080	516	4.080	566	4.080
367	4.080	417	4.080	467	4.080	517	4.080	567	4.080
368	4.080	418	4.080	468	4.080	518	4.080	568	4.080
369	4.080	419	4.080	469	4.080	519	4.080	569	4.080
370	4.080	420	4.080	470	4.080	520	4.080	570	4.080
371	4.080	421	4.080	471	4.080	521	4.080	571	4.080
372	4.080	422	4.080	472	4.080	522	4.080	572	4.080
373	4.080	423	4.080	473	4.080	523	4.080	573	4.080
374	4.080	424	4.080	474	4.080	524	4.080	574	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership										Page 6	
The Old School Old School Road Hook Hampshire RG27 9NJ					Summer Lane Pagham						
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX					Designed by Terry Seymour Checked by Terry Seymour						
Innovyze					Network 2017.1.2						
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
625	4.080	675	4.080	725	4.080	775	4.080	825	4.080	875	4.080
626	4.080	676	4.080	726	4.080	776	4.080	826	4.080	876	4.080
627	4.080	677	4.080	727	4.080	777	4.080	827	4.080	877	4.080
628	4.080	678	4.080	728	4.080	778	4.080	828	4.080	878	4.080
629	4.080	679	4.080	729	4.080	779	4.080	829	4.080	879	4.080
630	4.080	680	4.080	730	4.080	780	4.080	830	4.080	880	4.080
631	4.080	681	4.080	731	4.080	781	4.080	831	4.080	881	4.080
632	4.080	682	4.080	732	4.080	782	4.080	832	4.080	882	4.080
633	4.080	683	4.080	733	4.080	783	4.080	833	4.080	883	4.080
634	4.080	684	4.080	734	4.080	784	4.080	834	4.080	884	4.080
635	4.080	685	4.080	735	4.080	785	4.080	835	4.080	885	4.080
636	4.080	686	4.080	736	4.080	786	4.080	836	4.080	886	4.080
637	4.080	687	4.080	737	4.080	787	4.080	837	4.080	887	4.080
638	4.080	688	4.080	738	4.080	788	4.080	838	4.080	888	4.080
639	4.080	689	4.080	739	4.080	789	4.080	839	4.080	889	4.080
640	4.080	690	4.080	740	4.080	790	4.080	840	4.080	890	4.080
641	4.080	691	4.080	741	4.080	791	4.080	841	4.080	891	4.080
642	4.080	692	4.080	742	4.080	792	4.080	842	4.080	892	4.080
643	4.080	693	4.080	743	4.080	793	4.080	843	4.080	893	4.080
644	4.080	694	4.080	744	4.080	794	4.080	844	4.080	894	4.080
645	4.080	695	4.080	745	4.080	795	4.080	845	4.080	895	4.080
646	4.080	696	4.080	746	4.080	796	4.080	846	4.080	896	4.080
647	4.080	697	4.080	747	4.080	797	4.080	847	4.080	897	4.080
648	4.080	698	4.080	748	4.080	798	4.080	848	4.080	898	4.080
649	4.080	699	4.080	749	4.080	799	4.080	849	4.080	899	4.080
650	4.080	700	4.080	750	4.080	800	4.080	850	4.080	900	4.080
651	4.080	701	4.080	751	4.080	801	4.080	851	4.080	901	4.080
652	4.080	702	4.080	752	4.080	802	4.080	852	4.080	902	4.080
653	4.080	703	4.080	753	4.080	803	4.080	853	4.080	903	4.080
654	4.080	704	4.080	754	4.080	804	4.080	854	4.080	904	4.080
655	4.080	705	4.080	755	4.080	805	4.080	855	4.080	905	4.080
656	4.080	706	4.080	756	4.080	806	4.080	856	4.080	906	4.080
657	4.080	707	4.080	757	4.080	807	4.080	857	4.080	907	4.080
658	4.080	708	4.080	758	4.080	808	4.080	858	4.080	908	4.080
659	4.080	709	4.080	759	4.080	809	4.080	859	4.080	909	4.080
660	4.080	710	4.080	760	4.080	810	4.080	860	4.080	910	4.080
661	4.080	711	4.080	761	4.080	811	4.080	861	4.080	911	4.080
662	4.080	712	4.080	762	4.080	812	4.080	862	4.080	912	4.080
663	4.080	713	4.080	763	4.080	813	4.080	863	4.080	913	4.080
664	4.080	714	4.080	764	4.080	814	4.080	864	4.080	914	4.080
665	4.080	715	4.080	765	4.080	815	4.080	865	4.080	915	4.080
666	4.080	716	4.080	766	4.080	816	4.080	866	4.080	916	4.080
667	4.080	717	4.080	767	4.080	817	4.080	867	4.080	917	4.080
668	4.080	718	4.080	768	4.080	818	4.080	868	4.080	918	4.080
669	4.080	719	4.080	769	4.080	819	4.080	869	4.080	919	4.080
670	4.080	720	4.080	770	4.080	820	4.080	870	4.080	920	4.080
671	4.080	721	4.080	771	4.080	821	4.080	871	4.080	921	4.080
672	4.080	722	4.080	772	4.080	822	4.080	872	4.080	922	4.080
673	4.080	723	4.080	773	4.080	823	4.080	873	4.080	923	4.080
674	4.080	724	4.080	774	4.080	824	4.080	874	4.080	924	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership						Page 7			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
925	4.080	975	4.080	1025	4.080	1075	4.080	1125	4.080
926	4.080	976	4.080	1026	4.080	1076	4.080	1126	4.080
927	4.080	977	4.080	1027	4.080	1077	4.080	1127	4.080
928	4.080	978	4.080	1028	4.080	1078	4.080	1128	4.080
929	4.080	979	4.080	1029	4.080	1079	4.080	1129	4.080
930	4.080	980	4.080	1030	4.080	1080	4.080	1130	4.080
931	4.080	981	4.080	1031	4.080	1081	4.080	1131	4.080
932	4.080	982	4.080	1032	4.080	1082	4.080	1132	4.080
933	4.080	983	4.080	1033	4.080	1083	4.080	1133	4.080
934	4.080	984	4.080	1034	4.080	1084	4.080	1134	4.080
935	4.080	985	4.080	1035	4.080	1085	4.080	1135	4.080
936	4.080	986	4.080	1036	4.080	1086	4.080	1136	4.080
937	4.080	987	4.080	1037	4.080	1087	4.080	1137	4.080
938	4.080	988	4.080	1038	4.080	1088	4.080	1138	4.080
939	4.080	989	4.080	1039	4.080	1089	4.080	1139	4.080
940	4.080	990	4.080	1040	4.080	1090	4.080	1140	4.080
941	4.080	991	4.080	1041	4.080	1091	4.080	1141	4.080
942	4.080	992	4.080	1042	4.080	1092	4.080	1142	4.080
943	4.080	993	4.080	1043	4.080	1093	4.080	1143	4.080
944	4.080	994	4.080	1044	4.080	1094	4.080	1144	4.080
945	4.080	995	4.080	1045	4.080	1095	4.080	1145	4.080
946	4.080	996	4.080	1046	4.080	1096	4.080	1146	4.080
947	4.080	997	4.080	1047	4.080	1097	4.080	1147	4.080
948	4.080	998	4.080	1048	4.080	1098	4.080	1148	4.080
949	4.080	999	4.080	1049	4.080	1099	4.080	1149	4.080
950	4.080	1000	4.080	1050	4.080	1100	4.080	1150	4.080
951	4.080	1001	4.080	1051	4.080	1101	4.080	1151	4.080
952	4.080	1002	4.080	1052	4.080	1102	4.080	1152	4.080
953	4.080	1003	4.080	1053	4.080	1103	4.080	1153	4.080
954	4.080	1004	4.080	1054	4.080	1104	4.080	1154	4.080
955	4.080	1005	4.080	1055	4.080	1105	4.080	1155	4.080
956	4.080	1006	4.080	1056	4.080	1106	4.080	1156	4.080
957	4.080	1007	4.080	1057	4.080	1107	4.080	1157	4.080
958	4.080	1008	4.080	1058	4.080	1108	4.080	1158	4.080
959	4.080	1009	4.080	1059	4.080	1109	4.080	1159	4.080
960	4.080	1010	4.080	1060	4.080	1110	4.080	1160	4.080
961	4.080	1011	4.080	1061	4.080	1111	4.080	1161	4.080
962	4.080	1012	4.080	1062	4.080	1112	4.080	1162	4.080
963	4.080	1013	4.080	1063	4.080	1113	4.080	1163	4.080
964	4.080	1014	4.080	1064	4.080	1114	4.080	1164	4.080
965	4.080	1015	4.080	1065	4.080	1115	4.080	1165	4.080
966	4.080	1016	4.080	1066	4.080	1116	4.080	1166	4.080
967	4.080	1017	4.080	1067	4.080	1117	4.080	1167	4.080
968	4.080	1018	4.080	1068	4.080	1118	4.080	1168	4.080
969	4.080	1019	4.080	1069	4.080	1119	4.080	1169	4.080
970	4.080	1020	4.080	1070	4.080	1120	4.080	1170	4.080
971	4.080	1021	4.080	1071	4.080	1121	4.080	1171	4.080
972	4.080	1022	4.080	1072	4.080	1122	4.080	1172	4.080
973	4.080	1023	4.080	1073	4.080	1123	4.080	1173	4.080
974	4.080	1024	4.080	1074	4.080	1124	4.080	1174	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 8			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
1225	4.080	1275	4.080	1325	4.080	1375	4.080	1425	4.080
1226	4.080	1276	4.080	1326	4.080	1376	4.080	1426	4.080
1227	4.080	1277	4.080	1327	4.080	1377	4.080	1427	4.080
1228	4.080	1278	4.080	1328	4.080	1378	4.080	1428	4.080
1229	4.080	1279	4.080	1329	4.080	1379	4.080	1429	4.080
1230	4.080	1280	4.080	1330	4.080	1380	4.080	1430	4.080
1231	4.080	1281	4.080	1331	4.080	1381	4.080	1431	4.080
1232	4.080	1282	4.080	1332	4.080	1382	4.080	1432	4.080
1233	4.080	1283	4.080	1333	4.080	1383	4.080	1433	4.080
1234	4.080	1284	4.080	1334	4.080	1384	4.080	1434	4.080
1235	4.080	1285	4.080	1335	4.080	1385	4.080	1435	4.080
1236	4.080	1286	4.080	1336	4.080	1386	4.080	1436	4.080
1237	4.080	1287	4.080	1337	4.080	1387	4.080	1437	4.080
1238	4.080	1288	4.080	1338	4.080	1388	4.080	1438	4.080
1239	4.080	1289	4.080	1339	4.080	1389	4.080	1439	4.080
1240	4.080	1290	4.080	1340	4.080	1390	4.080	1440	4.080
1241	4.080	1291	4.080	1341	4.080	1391	4.080	1441	4.080
1242	4.080	1292	4.080	1342	4.080	1392	4.080	1442	4.080
1243	4.080	1293	4.080	1343	4.080	1393	4.080	1443	4.080
1244	4.080	1294	4.080	1344	4.080	1394	4.080	1444	4.080
1245	4.080	1295	4.080	1345	4.080	1395	4.080	1445	4.080
1246	4.080	1296	4.080	1346	4.080	1396	4.080	1446	4.080
1247	4.080	1297	4.080	1347	4.080	1397	4.080	1447	4.080
1248	4.080	1298	4.080	1348	4.080	1398	4.080	1448	4.080
1249	4.080	1299	4.080	1349	4.080	1399	4.080	1449	4.080
1250	4.080	1300	4.080	1350	4.080	1400	4.080	1450	4.080
1251	4.080	1301	4.080	1351	4.080	1401	4.080	1451	4.080
1252	4.080	1302	4.080	1352	4.080	1402	4.080	1452	4.080
1253	4.080	1303	4.080	1353	4.080	1403	4.080	1453	4.080
1254	4.080	1304	4.080	1354	4.080	1404	4.080	1454	4.080
1255	4.080	1305	4.080	1355	4.080	1405	4.080	1455	4.080
1256	4.080	1306	4.080	1356	4.080	1406	4.080	1456	4.080
1257	4.080	1307	4.080	1357	4.080	1407	4.080	1457	4.080
1258	4.080	1308	4.080	1358	4.080	1408	4.080	1458	4.080
1259	4.080	1309	4.080	1359	4.080	1409	4.080	1459	4.080
1260	4.080	1310	4.080	1360	4.080	1410	4.080	1460	4.080
1261	4.080	1311	4.080	1361	4.080	1411	4.080	1461	4.080
1262	4.080	1312	4.080	1362	4.080	1412	4.080	1462	4.080
1263	4.080	1313	4.080	1363	4.080	1413	4.080	1463	4.080
1264	4.080	1314	4.080	1364	4.080	1414	4.080	1464	4.080
1265	4.080	1315	4.080	1365	4.080	1415	4.080	1465	4.080
1266	4.080	1316	4.080	1366	4.080	1416	4.080	1466	4.080
1267	4.080	1317	4.080	1367	4.080	1417	4.080	1467	4.080
1268	4.080	1318	4.080	1368	4.080	1418	4.080	1468	4.080
1269	4.080	1319	4.080	1369	4.080	1419	4.080	1469	4.080
1270	4.080	1320	4.080	1370	4.080	1420	4.080	1470	4.080
1271	4.080	1321	4.080	1371	4.080	1421	4.080	1471	4.080
1272	4.080	1322	4.080	1372	4.080	1422	4.080	1472	4.080
1273	4.080	1323	4.080	1373	4.080	1423	4.080	1473	4.080
1274	4.080	1324	4.080	1374	4.080	1424	4.080	1474	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 9	
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
1525	4.080	1575	4.080	1625	4.080	1675	4.080	1725	4.080
1526	4.080	1576	4.080	1626	4.080	1676	4.080	1726	4.080
1527	4.080	1577	4.080	1627	4.080	1677	4.080	1727	4.080
1528	4.080	1578	4.080	1628	4.080	1678	4.080	1728	4.080
1529	4.080	1579	4.080	1629	4.080	1679	4.080	1729	4.080
1530	4.080	1580	4.080	1630	4.080	1680	4.080	1730	4.080
1531	4.080	1581	4.080	1631	4.080	1681	4.080	1731	4.080
1532	4.080	1582	4.080	1632	4.080	1682	4.080	1732	4.080
1533	4.080	1583	4.080	1633	4.080	1683	4.080	1733	4.080
1534	4.080	1584	4.080	1634	4.080	1684	4.080	1734	4.080
1535	4.080	1585	4.080	1635	4.080	1685	4.080	1735	4.080
1536	4.080	1586	4.080	1636	4.080	1686	4.080	1736	4.080
1537	4.080	1587	4.080	1637	4.080	1687	4.080	1737	4.080
1538	4.080	1588	4.080	1638	4.080	1688	4.080	1738	4.080
1539	4.080	1589	4.080	1639	4.080	1689	4.080	1739	4.080
1540	4.080	1590	4.080	1640	4.080	1690	4.080	1740	4.080
1541	4.080	1591	4.080	1641	4.080	1691	4.080	1741	4.080
1542	4.080	1592	4.080	1642	4.080	1692	4.080	1742	4.080
1543	4.080	1593	4.080	1643	4.080	1693	4.080	1743	4.080
1544	4.080	1594	4.080	1644	4.080	1694	4.080	1744	4.080
1545	4.080	1595	4.080	1645	4.080	1695	4.080	1745	4.080
1546	4.080	1596	4.080	1646	4.080	1696	4.080	1746	4.080
1547	4.080	1597	4.080	1647	4.080	1697	4.080	1747	4.080
1548	4.080	1598	4.080	1648	4.080	1698	4.080	1748	4.080
1549	4.080	1599	4.080	1649	4.080	1699	4.080	1749	4.080
1550	4.080	1600	4.080	1650	4.080	1700	4.080	1750	4.080
1551	4.080	1601	4.080	1651	4.080	1701	4.080	1751	4.080
1552	4.080	1602	4.080	1652	4.080	1702	4.080	1752	4.080
1553	4.080	1603	4.080	1653	4.080	1703	4.080	1753	4.080
1554	4.080	1604	4.080	1654	4.080	1704	4.080	1754	4.080
1555	4.080	1605	4.080	1655	4.080	1705	4.080	1755	4.080
1556	4.080	1606	4.080	1656	4.080	1706	4.080	1756	4.080
1557	4.080	1607	4.080	1657	4.080	1707	4.080	1757	4.080
1558	4.080	1608	4.080	1658	4.080	1708	4.080	1758	4.080
1559	4.080	1609	4.080	1659	4.080	1709	4.080	1759	4.080
1560	4.080	1610	4.080	1660	4.080	1710	4.080	1760	4.080
1561	4.080	1611	4.080	1661	4.080	1711	4.080	1761	4.080
1562	4.080	1612	4.080	1662	4.080	1712	4.080	1762	4.080
1563	4.080	1613	4.080	1663	4.080	1713	4.080	1763	4.080
1564	4.080	1614	4.080	1664	4.080	1714	4.080	1764	4.080
1565	4.080	1615	4.080	1665	4.080	1715	4.080	1765	4.080
1566	4.080	1616	4.080	1666	4.080	1716	4.080	1766	4.080
1567	4.080	1617	4.080	1667	4.080	1717	4.080	1767	4.080
1568	4.080	1618	4.080	1668	4.080	1718	4.080	1768	4.080
1569	4.080	1619	4.080	1669	4.080	1719	4.080	1769	4.080
1570	4.080	1620	4.080	1670	4.080	1720	4.080	1770	4.080
1571	4.080	1621	4.080	1671	4.080	1721	4.080	1771	4.080
1572	4.080	1622	4.080	1672	4.080	1722	4.080	1772	4.080
1573	4.080	1623	4.080	1673	4.080	1723	4.080	1773	4.080
1574	4.080	1624	4.080	1674	4.080	1724	4.080	1774	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 10			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
1825	4.080	1875	4.080	1925	4.080	1975	4.080	2025	4.080
1826	4.080	1876	4.080	1926	4.080	1976	4.080	2026	4.080
1827	4.080	1877	4.080	1927	4.080	1977	4.080	2027	4.080
1828	4.080	1878	4.080	1928	4.080	1978	4.080	2028	4.080
1829	4.080	1879	4.080	1929	4.080	1979	4.080	2029	4.080
1830	4.080	1880	4.080	1930	4.080	1980	4.080	2030	4.080
1831	4.080	1881	4.080	1931	4.080	1981	4.080	2031	4.080
1832	4.080	1882	4.080	1932	4.080	1982	4.080	2032	4.080
1833	4.080	1883	4.080	1933	4.080	1983	4.080	2033	4.080
1834	4.080	1884	4.080	1934	4.080	1984	4.080	2034	4.080
1835	4.080	1885	4.080	1935	4.080	1985	4.080	2035	4.080
1836	4.080	1886	4.080	1936	4.080	1986	4.080	2036	4.080
1837	4.080	1887	4.080	1937	4.080	1987	4.080	2037	4.080
1838	4.080	1888	4.080	1938	4.080	1988	4.080	2038	4.080
1839	4.080	1889	4.080	1939	4.080	1989	4.080	2039	4.080
1840	4.080	1890	4.080	1940	4.080	1990	4.080	2040	4.080
1841	4.080	1891	4.080	1941	4.080	1991	4.080	2041	4.080
1842	4.080	1892	4.080	1942	4.080	1992	4.080	2042	4.080
1843	4.080	1893	4.080	1943	4.080	1993	4.080	2043	4.080
1844	4.080	1894	4.080	1944	4.080	1994	4.080	2044	4.080
1845	4.080	1895	4.080	1945	4.080	1995	4.080	2045	4.080
1846	4.080	1896	4.080	1946	4.080	1996	4.080	2046	4.080
1847	4.080	1897	4.080	1947	4.080	1997	4.080	2047	4.080
1848	4.080	1898	4.080	1948	4.080	1998	4.080	2048	4.080
1849	4.080	1899	4.080	1949	4.080	1999	4.080	2049	4.080
1850	4.080	1900	4.080	1950	4.080	2000	4.080	2050	4.080
1851	4.080	1901	4.080	1951	4.080	2001	4.080	2051	4.080
1852	4.080	1902	4.080	1952	4.080	2002	4.080	2052	4.080
1853	4.080	1903	4.080	1953	4.080	2003	4.080	2053	4.080
1854	4.080	1904	4.080	1954	4.080	2004	4.080	2054	4.080
1855	4.080	1905	4.080	1955	4.080	2005	4.080	2055	4.080
1856	4.080	1906	4.080	1956	4.080	2006	4.080	2056	4.080
1857	4.080	1907	4.080	1957	4.080	2007	4.080	2057	4.080
1858	4.080	1908	4.080	1958	4.080	2008	4.080	2058	4.080
1859	4.080	1909	4.080	1959	4.080	2009	4.080	2059	4.080
1860	4.080	1910	4.080	1960	4.080	2010	4.080	2060	4.080
1861	4.080	1911	4.080	1961	4.080	2011	4.080	2061	4.080
1862	4.080	1912	4.080	1962	4.080	2012	4.080	2062	4.080
1863	4.080	1913	4.080	1963	4.080	2013	4.080	2063	4.080
1864	4.080	1914	4.080	1964	4.080	2014	4.080	2064	4.080
1865	4.080	1915	4.080	1965	4.080	2015	4.080	2065	4.080
1866	4.080	1916	4.080	1966	4.080	2016	4.080	2066	4.080
1867	4.080	1917	4.080	1967	4.080	2017	4.080	2067	4.080
1868	4.080	1918	4.080	1968	4.080	2018	4.080	2068	4.080
1869	4.080	1919	4.080	1969	4.080	2019	4.080	2069	4.080
1870	4.080	1920	4.080	1970	4.080	2020	4.080	2070	4.080
1871	4.080	1921	4.080	1971	4.080	2021	4.080	2071	4.080
1872	4.080	1922	4.080	1972	4.080	2022	4.080	2072	4.080
1873	4.080	1923	4.080	1973	4.080	2023	4.080	2073	4.080
1874	4.080	1924	4.080	1974	4.080	2024	4.080	2074	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 11			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
2125	4.080	2175	4.080	2225	4.080	2275	4.080	2325	4.080
2126	4.080	2176	4.080	2226	4.080	2276	4.080	2326	4.080
2127	4.080	2177	4.080	2227	4.080	2277	4.080	2327	4.080
2128	4.080	2178	4.080	2228	4.080	2278	4.080	2328	4.080
2129	4.080	2179	4.080	2229	4.080	2279	4.080	2329	4.080
2130	4.080	2180	4.080	2230	4.080	2280	4.080	2330	4.080
2131	4.080	2181	4.080	2231	4.080	2281	4.080	2331	4.080
2132	4.080	2182	4.080	2232	4.080	2282	4.080	2332	4.080
2133	4.080	2183	4.080	2233	4.080	2283	4.080	2333	4.080
2134	4.080	2184	4.080	2234	4.080	2284	4.080	2334	4.080
2135	4.080	2185	4.080	2235	4.080	2285	4.080	2335	4.080
2136	4.080	2186	4.080	2236	4.080	2286	4.080	2336	4.080
2137	4.080	2187	4.080	2237	4.080	2287	4.080	2337	4.080
2138	4.080	2188	4.080	2238	4.080	2288	4.080	2338	4.080
2139	4.080	2189	4.080	2239	4.080	2289	4.080	2339	4.080
2140	4.080	2190	4.080	2240	4.080	2290	4.080	2340	4.080
2141	4.080	2191	4.080	2241	4.080	2291	4.080	2341	4.080
2142	4.080	2192	4.080	2242	4.080	2292	4.080	2342	4.080
2143	4.080	2193	4.080	2243	4.080	2293	4.080	2343	4.080
2144	4.080	2194	4.080	2244	4.080	2294	4.080	2344	4.080
2145	4.080	2195	4.080	2245	4.080	2295	4.080	2345	4.080
2146	4.080	2196	4.080	2246	4.080	2296	4.080	2346	4.080
2147	4.080	2197	4.080	2247	4.080	2297	4.080	2347	4.080
2148	4.080	2198	4.080	2248	4.080	2298	4.080	2348	4.080
2149	4.080	2199	4.080	2249	4.080	2299	4.080	2349	4.080
2150	4.080	2200	4.080	2250	4.080	2300	4.080	2350	4.080
2151	4.080	2201	4.080	2251	4.080	2301	4.080	2351	4.080
2152	4.080	2202	4.080	2252	4.080	2302	4.080	2352	4.080
2153	4.080	2203	4.080	2253	4.080	2303	4.080	2353	4.080
2154	4.080	2204	4.080	2254	4.080	2304	4.080	2354	4.080
2155	4.080	2205	4.080	2255	4.080	2305	4.080	2355	4.080
2156	4.080	2206	4.080	2256	4.080	2306	4.080	2356	4.080
2157	4.080	2207	4.080	2257	4.080	2307	4.080	2357	4.080
2158	4.080	2208	4.080	2258	4.080	2308	4.080	2358	4.080
2159	4.080	2209	4.080	2259	4.080	2309	4.080	2359	4.080
2160	4.080	2210	4.080	2260	4.080	2310	4.080	2360	4.080
2161	4.080	2211	4.080	2261	4.080	2311	4.080	2361	4.080
2162	4.080	2212	4.080	2262	4.080	2312	4.080	2362	4.080
2163	4.080	2213	4.080	2263	4.080	2313	4.080	2363	4.080
2164	4.080	2214	4.080	2264	4.080	2314	4.080	2364	4.080
2165	4.080	2215	4.080	2265	4.080	2315	4.080	2365	4.080
2166	4.080	2216	4.080	2266	4.080	2316	4.080	2366	4.080
2167	4.080	2217	4.080	2267	4.080	2317	4.080	2367	4.080
2168	4.080	2218	4.080	2268	4.080	2318	4.080	2368	4.080
2169	4.080	2219	4.080	2269	4.080	2319	4.080	2369	4.080
2170	4.080	2220	4.080	2270	4.080	2320	4.080	2370	4.080
2171	4.080	2221	4.080	2271	4.080	2321	4.080	2371	4.080
2172	4.080	2222	4.080	2272	4.080	2322	4.080	2372	4.080
2173	4.080	2223	4.080	2273	4.080	2323	4.080	2373	4.080
2174	4.080	2224	4.080	2274	4.080	2324	4.080	2374	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 12			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
2425	4.080	2475	4.080	2525	4.080	2575	4.080	2625	4.080	2675	4.080
2426	4.080	2476	4.080	2526	4.080	2576	4.080	2626	4.080	2676	4.080
2427	4.080	2477	4.080	2527	4.080	2577	4.080	2627	4.080	2677	4.080
2428	4.080	2478	4.080	2528	4.080	2578	4.080	2628	4.080	2678	4.080
2429	4.080	2479	4.080	2529	4.080	2579	4.080	2629	4.080	2679	4.080
2430	4.080	2480	4.080	2530	4.080	2580	4.080	2630	4.080	2680	4.080
2431	4.080	2481	4.080	2531	4.080	2581	4.080	2631	4.080	2681	4.080
2432	4.080	2482	4.080	2532	4.080	2582	4.080	2632	4.080	2682	4.080
2433	4.080	2483	4.080	2533	4.080	2583	4.080	2633	4.080	2683	4.080
2434	4.080	2484	4.080	2534	4.080	2584	4.080	2634	4.080	2684	4.080
2435	4.080	2485	4.080	2535	4.080	2585	4.080	2635	4.080	2685	4.080
2436	4.080	2486	4.080	2536	4.080	2586	4.080	2636	4.080	2686	4.080
2437	4.080	2487	4.080	2537	4.080	2587	4.080	2637	4.080	2687	4.080
2438	4.080	2488	4.080	2538	4.080	2588	4.080	2638	4.080	2688	4.080
2439	4.080	2489	4.080	2539	4.080	2589	4.080	2639	4.080	2689	4.080
2440	4.080	2490	4.080	2540	4.080	2590	4.080	2640	4.080	2690	4.080
2441	4.080	2491	4.080	2541	4.080	2591	4.080	2641	4.080	2691	4.080
2442	4.080	2492	4.080	2542	4.080	2592	4.080	2642	4.080	2692	4.080
2443	4.080	2493	4.080	2543	4.080	2593	4.080	2643	4.080	2693	4.080
2444	4.080	2494	4.080	2544	4.080	2594	4.080	2644	4.080	2694	4.080
2445	4.080	2495	4.080	2545	4.080	2595	4.080	2645	4.080	2695	4.080
2446	4.080	2496	4.080	2546	4.080	2596	4.080	2646	4.080	2696	4.080
2447	4.080	2497	4.080	2547	4.080	2597	4.080	2647	4.080	2697	4.080
2448	4.080	2498	4.080	2548	4.080	2598	4.080	2648	4.080	2698	4.080
2449	4.080	2499	4.080	2549	4.080	2599	4.080	2649	4.080	2699	4.080
2450	4.080	2500	4.080	2550	4.080	2600	4.080	2650	4.080	2700	4.080
2451	4.080	2501	4.080	2551	4.080	2601	4.080	2651	4.080	2701	4.080
2452	4.080	2502	4.080	2552	4.080	2602	4.080	2652	4.080	2702	4.080
2453	4.080	2503	4.080	2553	4.080	2603	4.080	2653	4.080	2703	4.080
2454	4.080	2504	4.080	2554	4.080	2604	4.080	2654	4.080	2704	4.080
2455	4.080	2505	4.080	2555	4.080	2605	4.080	2655	4.080	2705	4.080
2456	4.080	2506	4.080	2556	4.080	2606	4.080	2656	4.080	2706	4.080
2457	4.080	2507	4.080	2557	4.080	2607	4.080	2657	4.080	2707	4.080
2458	4.080	2508	4.080	2558	4.080	2608	4.080	2658	4.080	2708	4.080
2459	4.080	2509	4.080	2559	4.080	2609	4.080	2659	4.080	2709	4.080
2460	4.080	2510	4.080	2560	4.080	2610	4.080	2660	4.080	2710	4.080
2461	4.080	2511	4.080	2561	4.080	2611	4.080	2661	4.080	2711	4.080
2462	4.080	2512	4.080	2562	4.080	2612	4.080	2662	4.080	2712	4.080
2463	4.080	2513	4.080	2563	4.080	2613	4.080	2663	4.080	2713	4.080
2464	4.080	2514	4.080	2564	4.080	2614	4.080	2664	4.080	2714	4.080
2465	4.080	2515	4.080	2565	4.080	2615	4.080	2665	4.080	2715	4.080
2466	4.080	2516	4.080	2566	4.080	2616	4.080	2666	4.080	2716	4.080
2467	4.080	2517	4.080	2567	4.080	2617	4.080	2667	4.080	2717	4.080
2468	4.080	2518	4.080	2568	4.080	2618	4.080	2668	4.080	2718	4.080
2469	4.080	2519	4.080	2569	4.080	2619	4.080	2669	4.080	2719	4.080
2470	4.080	2520	4.080	2570	4.080	2620	4.080	2670	4.080	2720	4.080
2471	4.080	2521	4.080	2571	4.080	2621	4.080	2671	4.080	2721	4.080
2472	4.080	2522	4.080	2572	4.080	2622	4.080	2672	4.080	2722	4.080
2473	4.080	2523	4.080	2573	4.080	2623	4.080	2673	4.080	2723	4.080
2474	4.080	2524	4.080	2574	4.080	2624	4.080	2674	4.080	2724	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership						Page 13			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
2725	4.080	2775	4.080	2825	4.080	2875	4.080	2925	4.080
2726	4.080	2776	4.080	2826	4.080	2876	4.080	2926	4.080
2727	4.080	2777	4.080	2827	4.080	2877	4.080	2927	4.080
2728	4.080	2778	4.080	2828	4.080	2878	4.080	2928	4.080
2729	4.080	2779	4.080	2829	4.080	2879	4.080	2929	4.080
2730	4.080	2780	4.080	2830	4.080	2880	4.080	2930	4.080
2731	4.080	2781	4.080	2831	4.080	2881	4.080	2931	4.080
2732	4.080	2782	4.080	2832	4.080	2882	4.080	2932	4.080
2733	4.080	2783	4.080	2833	4.080	2883	4.080	2933	4.080
2734	4.080	2784	4.080	2834	4.080	2884	4.080	2934	4.080
2735	4.080	2785	4.080	2835	4.080	2885	4.080	2935	4.080
2736	4.080	2786	4.080	2836	4.080	2886	4.080	2936	4.080
2737	4.080	2787	4.080	2837	4.080	2887	4.080	2937	4.080
2738	4.080	2788	4.080	2838	4.080	2888	4.080	2938	4.080
2739	4.080	2789	4.080	2839	4.080	2889	4.080	2939	4.080
2740	4.080	2790	4.080	2840	4.080	2890	4.080	2940	4.080
2741	4.080	2791	4.080	2841	4.080	2891	4.080	2941	4.080
2742	4.080	2792	4.080	2842	4.080	2892	4.080	2942	4.080
2743	4.080	2793	4.080	2843	4.080	2893	4.080	2943	4.080
2744	4.080	2794	4.080	2844	4.080	2894	4.080	2944	4.080
2745	4.080	2795	4.080	2845	4.080	2895	4.080	2945	4.080
2746	4.080	2796	4.080	2846	4.080	2896	4.080	2946	4.080
2747	4.080	2797	4.080	2847	4.080	2897	4.080	2947	4.080
2748	4.080	2798	4.080	2848	4.080	2898	4.080	2948	4.080
2749	4.080	2799	4.080	2849	4.080	2899	4.080	2949	4.080
2750	4.080	2800	4.080	2850	4.080	2900	4.080	2950	4.080
2751	4.080	2801	4.080	2851	4.080	2901	4.080	2951	4.080
2752	4.080	2802	4.080	2852	4.080	2902	4.080	2952	4.080
2753	4.080	2803	4.080	2853	4.080	2903	4.080	2953	4.080
2754	4.080	2804	4.080	2854	4.080	2904	4.080	2954	4.080
2755	4.080	2805	4.080	2855	4.080	2905	4.080	2955	4.080
2756	4.080	2806	4.080	2856	4.080	2906	4.080	2956	4.080
2757	4.080	2807	4.080	2857	4.080	2907	4.080	2957	4.080
2758	4.080	2808	4.080	2858	4.080	2908	4.080	2958	4.080
2759	4.080	2809	4.080	2859	4.080	2909	4.080	2959	4.080
2760	4.080	2810	4.080	2860	4.080	2910	4.080	2960	4.080
2761	4.080	2811	4.080	2861	4.080	2911	4.080	2961	4.080
2762	4.080	2812	4.080	2862	4.080	2912	4.080	2962	4.080
2763	4.080	2813	4.080	2863	4.080	2913	4.080	2963	4.080
2764	4.080	2814	4.080	2864	4.080	2914	4.080	2964	4.080
2765	4.080	2815	4.080	2865	4.080	2915	4.080	2965	4.080
2766	4.080	2816	4.080	2866	4.080	2916	4.080	2966	4.080
2767	4.080	2817	4.080	2867	4.080	2917	4.080	2967	4.080
2768	4.080	2818	4.080	2868	4.080	2918	4.080	2968	4.080
2769	4.080	2819	4.080	2869	4.080	2919	4.080	2969	4.080
2770	4.080	2820	4.080	2870	4.080	2920	4.080	2970	4.080
2771	4.080	2821	4.080	2871	4.080	2921	4.080	2971	4.080
2772	4.080	2822	4.080	2872	4.080	2922	4.080	2972	4.080
2773	4.080	2823	4.080	2873	4.080	2923	4.080	2973	4.080
2774	4.080	2824	4.080	2874	4.080	2924	4.080	2974	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 15			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
3325	4.080	3375	4.080	3425	4.080	3475	4.080	3525	4.080
3326	4.080	3376	4.080	3426	4.080	3476	4.080	3526	4.080
3327	4.080	3377	4.080	3427	4.080	3477	4.080	3527	4.080
3328	4.080	3378	4.080	3428	4.080	3478	4.080	3528	4.080
3329	4.080	3379	4.080	3429	4.080	3479	4.080	3529	4.080
3330	4.080	3380	4.080	3430	4.080	3480	4.080	3530	4.080
3331	4.080	3381	4.080	3431	4.080	3481	4.080	3531	4.080
3332	4.080	3382	4.080	3432	4.080	3482	4.080	3532	4.080
3333	4.080	3383	4.080	3433	4.080	3483	4.080	3533	4.080
3334	4.080	3384	4.080	3434	4.080	3484	4.080	3534	4.080
3335	4.080	3385	4.080	3435	4.080	3485	4.080	3535	4.080
3336	4.080	3386	4.080	3436	4.080	3486	4.080	3536	4.080
3337	4.080	3387	4.080	3437	4.080	3487	4.080	3537	4.080
3338	4.080	3388	4.080	3438	4.080	3488	4.080	3538	4.080
3339	4.080	3389	4.080	3439	4.080	3489	4.080	3539	4.080
3340	4.080	3390	4.080	3440	4.080	3490	4.080	3540	4.080
3341	4.080	3391	4.080	3441	4.080	3491	4.080	3541	4.080
3342	4.080	3392	4.080	3442	4.080	3492	4.080	3542	4.080
3343	4.080	3393	4.080	3443	4.080	3493	4.080	3543	4.080
3344	4.080	3394	4.080	3444	4.080	3494	4.080	3544	4.080
3345	4.080	3395	4.080	3445	4.080	3495	4.080	3545	4.080
3346	4.080	3396	4.080	3446	4.080	3496	4.080	3546	4.080
3347	4.080	3397	4.080	3447	4.080	3497	4.080	3547	4.080
3348	4.080	3398	4.080	3448	4.080	3498	4.080	3548	4.080
3349	4.080	3399	4.080	3449	4.080	3499	4.080	3549	4.080
3350	4.080	3400	4.080	3450	4.080	3500	4.080	3550	4.080
3351	4.080	3401	4.080	3451	4.080	3501	4.080	3551	4.080
3352	4.080	3402	4.080	3452	4.080	3502	4.080	3552	4.080
3353	4.080	3403	4.080	3453	4.080	3503	4.080	3553	4.080
3354	4.080	3404	4.080	3454	4.080	3504	4.080	3554	4.080
3355	4.080	3405	4.080	3455	4.080	3505	4.080	3555	4.080
3356	4.080	3406	4.080	3456	4.080	3506	4.080	3556	4.080
3357	4.080	3407	4.080	3457	4.080	3507	4.080	3557	4.080
3358	4.080	3408	4.080	3458	4.080	3508	4.080	3558	4.080
3359	4.080	3409	4.080	3459	4.080	3509	4.080	3559	4.080
3360	4.080	3410	4.080	3460	4.080	3510	4.080	3560	4.080
3361	4.080	3411	4.080	3461	4.080	3511	4.080	3561	4.080
3362	4.080	3412	4.080	3462	4.080	3512	4.080	3562	4.080
3363	4.080	3413	4.080	3463	4.080	3513	4.080	3563	4.080
3364	4.080	3414	4.080	3464	4.080	3514	4.080	3564	4.080
3365	4.080	3415	4.080	3465	4.080	3515	4.080	3565	4.080
3366	4.080	3416	4.080	3466	4.080	3516	4.080	3566	4.080
3367	4.080	3417	4.080	3467	4.080	3517	4.080	3567	4.080
3368	4.080	3418	4.080	3468	4.080	3518	4.080	3568	4.080
3369	4.080	3419	4.080	3469	4.080	3519	4.080	3569	4.080
3370	4.080	3420	4.080	3470	4.080	3520	4.080	3570	4.080
3371	4.080	3421	4.080	3471	4.080	3521	4.080	3571	4.080
3372	4.080	3422	4.080	3472	4.080	3522	4.080	3572	4.080
3373	4.080	3423	4.080	3473	4.080	3523	4.080	3573	4.080
3374	4.080	3424	4.080	3474	4.080	3524	4.080	3574	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 16			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
Surcharged Outfall Details for SW-1.SWS									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
3625	4.080	3675	4.080	3725	4.080	3775	4.080	3825	4.080
3626	4.080	3676	4.080	3726	4.080	3776	4.080	3826	4.080
3627	4.080	3677	4.080	3727	4.080	3777	4.080	3827	4.080
3628	4.080	3678	4.080	3728	4.080	3778	4.080	3828	4.080
3629	4.080	3679	4.080	3729	4.080	3779	4.080	3829	4.080
3630	4.080	3680	4.080	3730	4.080	3780	4.080	3830	4.080
3631	4.080	3681	4.080	3731	4.080	3781	4.080	3831	4.080
3632	4.080	3682	4.080	3732	4.080	3782	4.080	3832	4.080
3633	4.080	3683	4.080	3733	4.080	3783	4.080	3833	4.080
3634	4.080	3684	4.080	3734	4.080	3784	4.080	3834	4.080
3635	4.080	3685	4.080	3735	4.080	3785	4.080	3835	4.080
3636	4.080	3686	4.080	3736	4.080	3786	4.080	3836	4.080
3637	4.080	3687	4.080	3737	4.080	3787	4.080	3837	4.080
3638	4.080	3688	4.080	3738	4.080	3788	4.080	3838	4.080
3639	4.080	3689	4.080	3739	4.080	3789	4.080	3839	4.080
3640	4.080	3690	4.080	3740	4.080	3790	4.080	3840	4.080
3641	4.080	3691	4.080	3741	4.080	3791	4.080	3841	4.080
3642	4.080	3692	4.080	3742	4.080	3792	4.080	3842	4.080
3643	4.080	3693	4.080	3743	4.080	3793	4.080	3843	4.080
3644	4.080	3694	4.080	3744	4.080	3794	4.080	3844	4.080
3645	4.080	3695	4.080	3745	4.080	3795	4.080	3845	4.080
3646	4.080	3696	4.080	3746	4.080	3796	4.080	3846	4.080
3647	4.080	3697	4.080	3747	4.080	3797	4.080	3847	4.080
3648	4.080	3698	4.080	3748	4.080	3798	4.080	3848	4.080
3649	4.080	3699	4.080	3749	4.080	3799	4.080	3849	4.080
3650	4.080	3700	4.080	3750	4.080	3800	4.080	3850	4.080
3651	4.080	3701	4.080	3751	4.080	3801	4.080	3851	4.080
3652	4.080	3702	4.080	3752	4.080	3802	4.080	3852	4.080
3653	4.080	3703	4.080	3753	4.080	3803	4.080	3853	4.080
3654	4.080	3704	4.080	3754	4.080	3804	4.080	3854	4.080
3655	4.080	3705	4.080	3755	4.080	3805	4.080	3855	4.080
3656	4.080	3706	4.080	3756	4.080	3806	4.080	3856	4.080
3657	4.080	3707	4.080	3757	4.080	3807	4.080	3857	4.080
3658	4.080	3708	4.080	3758	4.080	3808	4.080	3858	4.080
3659	4.080	3709	4.080	3759	4.080	3809	4.080	3859	4.080
3660	4.080	3710	4.080	3760	4.080	3810	4.080	3860	4.080
3661	4.080	3711	4.080	3761	4.080	3811	4.080	3861	4.080
3662	4.080	3712	4.080	3762	4.080	3812	4.080	3862	4.080
3663	4.080	3713	4.080	3763	4.080	3813	4.080	3863	4.080
3664	4.080	3714	4.080	3764	4.080	3814	4.080	3864	4.080
3665	4.080	3715	4.080	3765	4.080	3815	4.080	3865	4.080
3666	4.080	3716	4.080	3766	4.080	3816	4.080	3866	4.080
3667	4.080	3717	4.080	3767	4.080	3817	4.080	3867	4.080
3668	4.080	3718	4.080	3768	4.080	3818	4.080	3868	4.080
3669	4.080	3719	4.080	3769	4.080	3819	4.080	3869	4.080
3670	4.080	3720	4.080	3770	4.080	3820	4.080	3870	4.080
3671	4.080	3721	4.080	3771	4.080	3821	4.080	3871	4.080
3672	4.080	3722	4.080	3772	4.080	3822	4.080	3872	4.080
3673	4.080	3723	4.080	3773	4.080	3823	4.080	3873	4.080
3674	4.080	3724	4.080	3774	4.080	3824	4.080	3874	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 17			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
3925	4.080	3975	4.080	4025	4.080	4075	4.080	4125	4.080	4175	4.080
3926	4.080	3976	4.080	4026	4.080	4076	4.080	4126	4.080	4176	4.080
3927	4.080	3977	4.080	4027	4.080	4077	4.080	4127	4.080	4177	4.080
3928	4.080	3978	4.080	4028	4.080	4078	4.080	4128	4.080	4178	4.080
3929	4.080	3979	4.080	4029	4.080	4079	4.080	4129	4.080	4179	4.080
3930	4.080	3980	4.080	4030	4.080	4080	4.080	4130	4.080	4180	4.080
3931	4.080	3981	4.080	4031	4.080	4081	4.080	4131	4.080	4181	4.080
3932	4.080	3982	4.080	4032	4.080	4082	4.080	4132	4.080	4182	4.080
3933	4.080	3983	4.080	4033	4.080	4083	4.080	4133	4.080	4183	4.080
3934	4.080	3984	4.080	4034	4.080	4084	4.080	4134	4.080	4184	4.080
3935	4.080	3985	4.080	4035	4.080	4085	4.080	4135	4.080	4185	4.080
3936	4.080	3986	4.080	4036	4.080	4086	4.080	4136	4.080	4186	4.080
3937	4.080	3987	4.080	4037	4.080	4087	4.080	4137	4.080	4187	4.080
3938	4.080	3988	4.080	4038	4.080	4088	4.080	4138	4.080	4188	4.080
3939	4.080	3989	4.080	4039	4.080	4089	4.080	4139	4.080	4189	4.080
3940	4.080	3990	4.080	4040	4.080	4090	4.080	4140	4.080	4190	4.080
3941	4.080	3991	4.080	4041	4.080	4091	4.080	4141	4.080	4191	4.080
3942	4.080	3992	4.080	4042	4.080	4092	4.080	4142	4.080	4192	4.080
3943	4.080	3993	4.080	4043	4.080	4093	4.080	4143	4.080	4193	4.080
3944	4.080	3994	4.080	4044	4.080	4094	4.080	4144	4.080	4194	4.080
3945	4.080	3995	4.080	4045	4.080	4095	4.080	4145	4.080	4195	4.080
3946	4.080	3996	4.080	4046	4.080	4096	4.080	4146	4.080	4196	4.080
3947	4.080	3997	4.080	4047	4.080	4097	4.080	4147	4.080	4197	4.080
3948	4.080	3998	4.080	4048	4.080	4098	4.080	4148	4.080	4198	4.080
3949	4.080	3999	4.080	4049	4.080	4099	4.080	4149	4.080	4199	4.080
3950	4.080	4000	4.080	4050	4.080	4100	4.080	4150	4.080	4200	4.080
3951	4.080	4001	4.080	4051	4.080	4101	4.080	4151	4.080	4201	4.080
3952	4.080	4002	4.080	4052	4.080	4102	4.080	4152	4.080	4202	4.080
3953	4.080	4003	4.080	4053	4.080	4103	4.080	4153	4.080	4203	4.080
3954	4.080	4004	4.080	4054	4.080	4104	4.080	4154	4.080	4204	4.080
3955	4.080	4005	4.080	4055	4.080	4105	4.080	4155	4.080	4205	4.080
3956	4.080	4006	4.080	4056	4.080	4106	4.080	4156	4.080	4206	4.080
3957	4.080	4007	4.080	4057	4.080	4107	4.080	4157	4.080	4207	4.080
3958	4.080	4008	4.080	4058	4.080	4108	4.080	4158	4.080	4208	4.080
3959	4.080	4009	4.080	4059	4.080	4109	4.080	4159	4.080	4209	4.080
3960	4.080	4010	4.080	4060	4.080	4110	4.080	4160	4.080	4210	4.080
3961	4.080	4011	4.080	4061	4.080	4111	4.080	4161	4.080	4211	4.080
3962	4.080	4012	4.080	4062	4.080	4112	4.080	4162	4.080	4212	4.080
3963	4.080	4013	4.080	4063	4.080	4113	4.080	4163	4.080	4213	4.080
3964	4.080	4014	4.080	4064	4.080	4114	4.080	4164	4.080	4214	4.080
3965	4.080	4015	4.080	4065	4.080	4115	4.080	4165	4.080	4215	4.080
3966	4.080	4016	4.080	4066	4.080	4116	4.080	4166	4.080	4216	4.080
3967	4.080	4017	4.080	4067	4.080	4117	4.080	4167	4.080	4217	4.080
3968	4.080	4018	4.080	4068	4.080	4118	4.080	4168	4.080	4218	4.080
3969	4.080	4019	4.080	4069	4.080	4119	4.080	4169	4.080	4219	4.080
3970	4.080	4020	4.080	4070	4.080	4120	4.080	4170	4.080	4220	4.080
3971	4.080	4021	4.080	4071	4.080	4121	4.080	4171	4.080	4221	4.080
3972	4.080	4022	4.080	4072	4.080	4122	4.080	4172	4.080	4222	4.080
3973	4.080	4023	4.080	4073	4.080	4123	4.080	4173	4.080	4223	4.080
3974	4.080	4024	4.080	4074	4.080	4124	4.080	4174	4.080	4224	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership								Page 18			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
4225	4.080	4275	4.080	4325	4.080	4375	4.080	4425	4.080	4475	4.080
4226	4.080	4276	4.080	4326	4.080	4376	4.080	4426	4.080	4476	4.080
4227	4.080	4277	4.080	4327	4.080	4377	4.080	4427	4.080	4477	4.080
4228	4.080	4278	4.080	4328	4.080	4378	4.080	4428	4.080	4478	4.080
4229	4.080	4279	4.080	4329	4.080	4379	4.080	4429	4.080	4479	4.080
4230	4.080	4280	4.080	4330	4.080	4380	4.080	4430	4.080	4480	4.080
4231	4.080	4281	4.080	4331	4.080	4381	4.080	4431	4.080	4481	4.080
4232	4.080	4282	4.080	4332	4.080	4382	4.080	4432	4.080	4482	4.080
4233	4.080	4283	4.080	4333	4.080	4383	4.080	4433	4.080	4483	4.080
4234	4.080	4284	4.080	4334	4.080	4384	4.080	4434	4.080	4484	4.080
4235	4.080	4285	4.080	4335	4.080	4385	4.080	4435	4.080	4485	4.080
4236	4.080	4286	4.080	4336	4.080	4386	4.080	4436	4.080	4486	4.080
4237	4.080	4287	4.080	4337	4.080	4387	4.080	4437	4.080	4487	4.080
4238	4.080	4288	4.080	4338	4.080	4388	4.080	4438	4.080	4488	4.080
4239	4.080	4289	4.080	4339	4.080	4389	4.080	4439	4.080	4489	4.080
4240	4.080	4290	4.080	4340	4.080	4390	4.080	4440	4.080	4490	4.080
4241	4.080	4291	4.080	4341	4.080	4391	4.080	4441	4.080	4491	4.080
4242	4.080	4292	4.080	4342	4.080	4392	4.080	4442	4.080	4492	4.080
4243	4.080	4293	4.080	4343	4.080	4393	4.080	4443	4.080	4493	4.080
4244	4.080	4294	4.080	4344	4.080	4394	4.080	4444	4.080	4494	4.080
4245	4.080	4295	4.080	4345	4.080	4395	4.080	4445	4.080	4495	4.080
4246	4.080	4296	4.080	4346	4.080	4396	4.080	4446	4.080	4496	4.080
4247	4.080	4297	4.080	4347	4.080	4397	4.080	4447	4.080	4497	4.080
4248	4.080	4298	4.080	4348	4.080	4398	4.080	4448	4.080	4498	4.080
4249	4.080	4299	4.080	4349	4.080	4399	4.080	4449	4.080	4499	4.080
4250	4.080	4300	4.080	4350	4.080	4400	4.080	4450	4.080	4500	4.080
4251	4.080	4301	4.080	4351	4.080	4401	4.080	4451	4.080	4501	4.080
4252	4.080	4302	4.080	4352	4.080	4402	4.080	4452	4.080	4502	4.080
4253	4.080	4303	4.080	4353	4.080	4403	4.080	4453	4.080	4503	4.080
4254	4.080	4304	4.080	4354	4.080	4404	4.080	4454	4.080	4504	4.080
4255	4.080	4305	4.080	4355	4.080	4405	4.080	4455	4.080	4505	4.080
4256	4.080	4306	4.080	4356	4.080	4406	4.080	4456	4.080	4506	4.080
4257	4.080	4307	4.080	4357	4.080	4407	4.080	4457	4.080	4507	4.080
4258	4.080	4308	4.080	4358	4.080	4408	4.080	4458	4.080	4508	4.080
4259	4.080	4309	4.080	4359	4.080	4409	4.080	4459	4.080	4509	4.080
4260	4.080	4310	4.080	4360	4.080	4410	4.080	4460	4.080	4510	4.080
4261	4.080	4311	4.080	4361	4.080	4411	4.080	4461	4.080	4511	4.080
4262	4.080	4312	4.080	4362	4.080	4412	4.080	4462	4.080	4512	4.080
4263	4.080	4313	4.080	4363	4.080	4413	4.080	4463	4.080	4513	4.080
4264	4.080	4314	4.080	4364	4.080	4414	4.080	4464	4.080	4514	4.080
4265	4.080	4315	4.080	4365	4.080	4415	4.080	4465	4.080	4515	4.080
4266	4.080	4316	4.080	4366	4.080	4416	4.080	4466	4.080	4516	4.080
4267	4.080	4317	4.080	4367	4.080	4417	4.080	4467	4.080	4517	4.080
4268	4.080	4318	4.080	4368	4.080	4418	4.080	4468	4.080	4518	4.080
4269	4.080	4319	4.080	4369	4.080	4419	4.080	4469	4.080	4519	4.080
4270	4.080	4320	4.080	4370	4.080	4420	4.080	4470	4.080	4520	4.080
4271	4.080	4321	4.080	4371	4.080	4421	4.080	4471	4.080	4521	4.080
4272	4.080	4322	4.080	4372	4.080	4422	4.080	4472	4.080	4522	4.080
4273	4.080	4323	4.080	4373	4.080	4423	4.080	4473	4.080	4523	4.080
4274	4.080	4324	4.080	4374	4.080	4424	4.080	4474	4.080	4524	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership								Page 19			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
4525	4.080	4575	4.080	4625	4.080	4675	4.080	4725	4.080	4775	4.080
4526	4.080	4576	4.080	4626	4.080	4676	4.080	4726	4.080	4776	4.080
4527	4.080	4577	4.080	4627	4.080	4677	4.080	4727	4.080	4777	4.080
4528	4.080	4578	4.080	4628	4.080	4678	4.080	4728	4.080	4778	4.080
4529	4.080	4579	4.080	4629	4.080	4679	4.080	4729	4.080	4779	4.080
4530	4.080	4580	4.080	4630	4.080	4680	4.080	4730	4.080	4780	4.080
4531	4.080	4581	4.080	4631	4.080	4681	4.080	4731	4.080	4781	4.080
4532	4.080	4582	4.080	4632	4.080	4682	4.080	4732	4.080	4782	4.080
4533	4.080	4583	4.080	4633	4.080	4683	4.080	4733	4.080	4783	4.080
4534	4.080	4584	4.080	4634	4.080	4684	4.080	4734	4.080	4784	4.080
4535	4.080	4585	4.080	4635	4.080	4685	4.080	4735	4.080	4785	4.080
4536	4.080	4586	4.080	4636	4.080	4686	4.080	4736	4.080	4786	4.080
4537	4.080	4587	4.080	4637	4.080	4687	4.080	4737	4.080	4787	4.080
4538	4.080	4588	4.080	4638	4.080	4688	4.080	4738	4.080	4788	4.080
4539	4.080	4589	4.080	4639	4.080	4689	4.080	4739	4.080	4789	4.080
4540	4.080	4590	4.080	4640	4.080	4690	4.080	4740	4.080	4790	4.080
4541	4.080	4591	4.080	4641	4.080	4691	4.080	4741	4.080	4791	4.080
4542	4.080	4592	4.080	4642	4.080	4692	4.080	4742	4.080	4792	4.080
4543	4.080	4593	4.080	4643	4.080	4693	4.080	4743	4.080	4793	4.080
4544	4.080	4594	4.080	4644	4.080	4694	4.080	4744	4.080	4794	4.080
4545	4.080	4595	4.080	4645	4.080	4695	4.080	4745	4.080	4795	4.080
4546	4.080	4596	4.080	4646	4.080	4696	4.080	4746	4.080	4796	4.080
4547	4.080	4597	4.080	4647	4.080	4697	4.080	4747	4.080	4797	4.080
4548	4.080	4598	4.080	4648	4.080	4698	4.080	4748	4.080	4798	4.080
4549	4.080	4599	4.080	4649	4.080	4699	4.080	4749	4.080	4799	4.080
4550	4.080	4600	4.080	4650	4.080	4700	4.080	4750	4.080	4800	4.080
4551	4.080	4601	4.080	4651	4.080	4701	4.080	4751	4.080	4801	4.080
4552	4.080	4602	4.080	4652	4.080	4702	4.080	4752	4.080	4802	4.080
4553	4.080	4603	4.080	4653	4.080	4703	4.080	4753	4.080	4803	4.080
4554	4.080	4604	4.080	4654	4.080	4704	4.080	4754	4.080	4804	4.080
4555	4.080	4605	4.080	4655	4.080	4705	4.080	4755	4.080	4805	4.080
4556	4.080	4606	4.080	4656	4.080	4706	4.080	4756	4.080	4806	4.080
4557	4.080	4607	4.080	4657	4.080	4707	4.080	4757	4.080	4807	4.080
4558	4.080	4608	4.080	4658	4.080	4708	4.080	4758	4.080	4808	4.080
4559	4.080	4609	4.080	4659	4.080	4709	4.080	4759	4.080	4809	4.080
4560	4.080	4610	4.080	4660	4.080	4710	4.080	4760	4.080	4810	4.080
4561	4.080	4611	4.080	4661	4.080	4711	4.080	4761	4.080	4811	4.080
4562	4.080	4612	4.080	4662	4.080	4712	4.080	4762	4.080	4812	4.080
4563	4.080	4613	4.080	4663	4.080	4713	4.080	4763	4.080	4813	4.080
4564	4.080	4614	4.080	4664	4.080	4714	4.080	4764	4.080	4814	4.080
4565	4.080	4615	4.080	4665	4.080	4715	4.080	4765	4.080	4815	4.080
4566	4.080	4616	4.080	4666	4.080	4716	4.080	4766	4.080	4816	4.080
4567	4.080	4617	4.080	4667	4.080	4717	4.080	4767	4.080	4817	4.080
4568	4.080	4618	4.080	4668	4.080	4718	4.080	4768	4.080	4818	4.080
4569	4.080	4619	4.080	4669	4.080	4719	4.080	4769	4.080	4819	4.080
4570	4.080	4620	4.080	4670	4.080	4720	4.080	4770	4.080	4820	4.080
4571	4.080	4621	4.080	4671	4.080	4721	4.080	4771	4.080	4821	4.080
4572	4.080	4622	4.080	4672	4.080	4722	4.080	4772	4.080	4822	4.080
4573	4.080	4623	4.080	4673	4.080	4723	4.080	4773	4.080	4823	4.080
4574	4.080	4624	4.080	4674	4.080	4724	4.080	4774	4.080	4824	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership								Page 20			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
4825	4.080	4875	4.080	4925	4.080	4975	4.080	5025	4.080	5075	4.080
4826	4.080	4876	4.080	4926	4.080	4976	4.080	5026	4.080	5076	4.080
4827	4.080	4877	4.080	4927	4.080	4977	4.080	5027	4.080	5077	4.080
4828	4.080	4878	4.080	4928	4.080	4978	4.080	5028	4.080	5078	4.080
4829	4.080	4879	4.080	4929	4.080	4979	4.080	5029	4.080	5079	4.080
4830	4.080	4880	4.080	4930	4.080	4980	4.080	5030	4.080	5080	4.080
4831	4.080	4881	4.080	4931	4.080	4981	4.080	5031	4.080	5081	4.080
4832	4.080	4882	4.080	4932	4.080	4982	4.080	5032	4.080	5082	4.080
4833	4.080	4883	4.080	4933	4.080	4983	4.080	5033	4.080	5083	4.080
4834	4.080	4884	4.080	4934	4.080	4984	4.080	5034	4.080	5084	4.080
4835	4.080	4885	4.080	4935	4.080	4985	4.080	5035	4.080	5085	4.080
4836	4.080	4886	4.080	4936	4.080	4986	4.080	5036	4.080	5086	4.080
4837	4.080	4887	4.080	4937	4.080	4987	4.080	5037	4.080	5087	4.080
4838	4.080	4888	4.080	4938	4.080	4988	4.080	5038	4.080	5088	4.080
4839	4.080	4889	4.080	4939	4.080	4989	4.080	5039	4.080	5089	4.080
4840	4.080	4890	4.080	4940	4.080	4990	4.080	5040	4.080	5090	4.080
4841	4.080	4891	4.080	4941	4.080	4991	4.080	5041	4.080	5091	4.080
4842	4.080	4892	4.080	4942	4.080	4992	4.080	5042	4.080	5092	4.080
4843	4.080	4893	4.080	4943	4.080	4993	4.080	5043	4.080	5093	4.080
4844	4.080	4894	4.080	4944	4.080	4994	4.080	5044	4.080	5094	4.080
4845	4.080	4895	4.080	4945	4.080	4995	4.080	5045	4.080	5095	4.080
4846	4.080	4896	4.080	4946	4.080	4996	4.080	5046	4.080	5096	4.080
4847	4.080	4897	4.080	4947	4.080	4997	4.080	5047	4.080	5097	4.080
4848	4.080	4898	4.080	4948	4.080	4998	4.080	5048	4.080	5098	4.080
4849	4.080	4899	4.080	4949	4.080	4999	4.080	5049	4.080	5099	4.080
4850	4.080	4900	4.080	4950	4.080	5000	4.080	5050	4.080	5100	4.080
4851	4.080	4901	4.080	4951	4.080	5001	4.080	5051	4.080	5101	4.080
4852	4.080	4902	4.080	4952	4.080	5002	4.080	5052	4.080	5102	4.080
4853	4.080	4903	4.080	4953	4.080	5003	4.080	5053	4.080	5103	4.080
4854	4.080	4904	4.080	4954	4.080	5004	4.080	5054	4.080	5104	4.080
4855	4.080	4905	4.080	4955	4.080	5005	4.080	5055	4.080	5105	4.080
4856	4.080	4906	4.080	4956	4.080	5006	4.080	5056	4.080	5106	4.080
4857	4.080	4907	4.080	4957	4.080	5007	4.080	5057	4.080	5107	4.080
4858	4.080	4908	4.080	4958	4.080	5008	4.080	5058	4.080	5108	4.080
4859	4.080	4909	4.080	4959	4.080	5009	4.080	5059	4.080	5109	4.080
4860	4.080	4910	4.080	4960	4.080	5010	4.080	5060	4.080	5110	4.080
4861	4.080	4911	4.080	4961	4.080	5011	4.080	5061	4.080	5111	4.080
4862	4.080	4912	4.080	4962	4.080	5012	4.080	5062	4.080	5112	4.080
4863	4.080	4913	4.080	4963	4.080	5013	4.080	5063	4.080	5113	4.080
4864	4.080	4914	4.080	4964	4.080	5014	4.080	5064	4.080	5114	4.080
4865	4.080	4915	4.080	4965	4.080	5015	4.080	5065	4.080	5115	4.080
4866	4.080	4916	4.080	4966	4.080	5016	4.080	5066	4.080	5116	4.080
4867	4.080	4917	4.080	4967	4.080	5017	4.080	5067	4.080	5117	4.080
4868	4.080	4918	4.080	4968	4.080	5018	4.080	5068	4.080	5118	4.080
4869	4.080	4919	4.080	4969	4.080	5019	4.080	5069	4.080	5119	4.080
4870	4.080	4920	4.080	4970	4.080	5020	4.080	5070	4.080	5120	4.080
4871	4.080	4921	4.080	4971	4.080	5021	4.080	5071	4.080	5121	4.080
4872	4.080	4922	4.080	4972	4.080	5022	4.080	5072	4.080	5122	4.080
4873	4.080	4923	4.080	4973	4.080	5023	4.080	5073	4.080	5123	4.080
4874	4.080	4924	4.080	4974	4.080	5024	4.080	5074	4.080	5124	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership						Page 21			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
5125	4.080	5175	4.080	5225	4.080	5275	4.080	5325	4.080
5126	4.080	5176	4.080	5226	4.080	5276	4.080	5326	4.080
5127	4.080	5177	4.080	5227	4.080	5277	4.080	5327	4.080
5128	4.080	5178	4.080	5228	4.080	5278	4.080	5328	4.080
5129	4.080	5179	4.080	5229	4.080	5279	4.080	5329	4.080
5130	4.080	5180	4.080	5230	4.080	5280	4.080	5330	4.080
5131	4.080	5181	4.080	5231	4.080	5281	4.080	5331	4.080
5132	4.080	5182	4.080	5232	4.080	5282	4.080	5332	4.080
5133	4.080	5183	4.080	5233	4.080	5283	4.080	5333	4.080
5134	4.080	5184	4.080	5234	4.080	5284	4.080	5334	4.080
5135	4.080	5185	4.080	5235	4.080	5285	4.080	5335	4.080
5136	4.080	5186	4.080	5236	4.080	5286	4.080	5336	4.080
5137	4.080	5187	4.080	5237	4.080	5287	4.080	5337	4.080
5138	4.080	5188	4.080	5238	4.080	5288	4.080	5338	4.080
5139	4.080	5189	4.080	5239	4.080	5289	4.080	5339	4.080
5140	4.080	5190	4.080	5240	4.080	5290	4.080	5340	4.080
5141	4.080	5191	4.080	5241	4.080	5291	4.080	5341	4.080
5142	4.080	5192	4.080	5242	4.080	5292	4.080	5342	4.080
5143	4.080	5193	4.080	5243	4.080	5293	4.080	5343	4.080
5144	4.080	5194	4.080	5244	4.080	5294	4.080	5344	4.080
5145	4.080	5195	4.080	5245	4.080	5295	4.080	5345	4.080
5146	4.080	5196	4.080	5246	4.080	5296	4.080	5346	4.080
5147	4.080	5197	4.080	5247	4.080	5297	4.080	5347	4.080
5148	4.080	5198	4.080	5248	4.080	5298	4.080	5348	4.080
5149	4.080	5199	4.080	5249	4.080	5299	4.080	5349	4.080
5150	4.080	5200	4.080	5250	4.080	5300	4.080	5350	4.080
5151	4.080	5201	4.080	5251	4.080	5301	4.080	5351	4.080
5152	4.080	5202	4.080	5252	4.080	5302	4.080	5352	4.080
5153	4.080	5203	4.080	5253	4.080	5303	4.080	5353	4.080
5154	4.080	5204	4.080	5254	4.080	5304	4.080	5354	4.080
5155	4.080	5205	4.080	5255	4.080	5305	4.080	5355	4.080
5156	4.080	5206	4.080	5256	4.080	5306	4.080	5356	4.080
5157	4.080	5207	4.080	5257	4.080	5307	4.080	5357	4.080
5158	4.080	5208	4.080	5258	4.080	5308	4.080	5358	4.080
5159	4.080	5209	4.080	5259	4.080	5309	4.080	5359	4.080
5160	4.080	5210	4.080	5260	4.080	5310	4.080	5360	4.080
5161	4.080	5211	4.080	5261	4.080	5311	4.080	5361	4.080
5162	4.080	5212	4.080	5262	4.080	5312	4.080	5362	4.080
5163	4.080	5213	4.080	5263	4.080	5313	4.080	5363	4.080
5164	4.080	5214	4.080	5264	4.080	5314	4.080	5364	4.080
5165	4.080	5215	4.080	5265	4.080	5315	4.080	5365	4.080
5166	4.080	5216	4.080	5266	4.080	5316	4.080	5366	4.080
5167	4.080	5217	4.080	5267	4.080	5317	4.080	5367	4.080
5168	4.080	5218	4.080	5268	4.080	5318	4.080	5368	4.080
5169	4.080	5219	4.080	5269	4.080	5319	4.080	5369	4.080
5170	4.080	5220	4.080	5270	4.080	5320	4.080	5370	4.080
5171	4.080	5221	4.080	5271	4.080	5321	4.080	5371	4.080
5172	4.080	5222	4.080	5272	4.080	5322	4.080	5372	4.080
5173	4.080	5223	4.080	5273	4.080	5323	4.080	5373	4.080
5174	4.080	5224	4.080	5274	4.080	5324	4.080	5374	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 22			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
5425	4.080	5475	4.080	5525	4.080	5575	4.080	5625	4.080	5675	4.080
5426	4.080	5476	4.080	5526	4.080	5576	4.080	5626	4.080	5676	4.080
5427	4.080	5477	4.080	5527	4.080	5577	4.080	5627	4.080	5677	4.080
5428	4.080	5478	4.080	5528	4.080	5578	4.080	5628	4.080	5678	4.080
5429	4.080	5479	4.080	5529	4.080	5579	4.080	5629	4.080	5679	4.080
5430	4.080	5480	4.080	5530	4.080	5580	4.080	5630	4.080	5680	4.080
5431	4.080	5481	4.080	5531	4.080	5581	4.080	5631	4.080	5681	4.080
5432	4.080	5482	4.080	5532	4.080	5582	4.080	5632	4.080	5682	4.080
5433	4.080	5483	4.080	5533	4.080	5583	4.080	5633	4.080	5683	4.080
5434	4.080	5484	4.080	5534	4.080	5584	4.080	5634	4.080	5684	4.080
5435	4.080	5485	4.080	5535	4.080	5585	4.080	5635	4.080	5685	4.080
5436	4.080	5486	4.080	5536	4.080	5586	4.080	5636	4.080	5686	4.080
5437	4.080	5487	4.080	5537	4.080	5587	4.080	5637	4.080	5687	4.080
5438	4.080	5488	4.080	5538	4.080	5588	4.080	5638	4.080	5688	4.080
5439	4.080	5489	4.080	5539	4.080	5589	4.080	5639	4.080	5689	4.080
5440	4.080	5490	4.080	5540	4.080	5590	4.080	5640	4.080	5690	4.080
5441	4.080	5491	4.080	5541	4.080	5591	4.080	5641	4.080	5691	4.080
5442	4.080	5492	4.080	5542	4.080	5592	4.080	5642	4.080	5692	4.080
5443	4.080	5493	4.080	5543	4.080	5593	4.080	5643	4.080	5693	4.080
5444	4.080	5494	4.080	5544	4.080	5594	4.080	5644	4.080	5694	4.080
5445	4.080	5495	4.080	5545	4.080	5595	4.080	5645	4.080	5695	4.080
5446	4.080	5496	4.080	5546	4.080	5596	4.080	5646	4.080	5696	4.080
5447	4.080	5497	4.080	5547	4.080	5597	4.080	5647	4.080	5697	4.080
5448	4.080	5498	4.080	5548	4.080	5598	4.080	5648	4.080	5698	4.080
5449	4.080	5499	4.080	5549	4.080	5599	4.080	5649	4.080	5699	4.080
5450	4.080	5500	4.080	5550	4.080	5600	4.080	5650	4.080	5700	4.080
5451	4.080	5501	4.080	5551	4.080	5601	4.080	5651	4.080	5701	4.080
5452	4.080	5502	4.080	5552	4.080	5602	4.080	5652	4.080	5702	4.080
5453	4.080	5503	4.080	5553	4.080	5603	4.080	5653	4.080	5703	4.080
5454	4.080	5504	4.080	5554	4.080	5604	4.080	5654	4.080	5704	4.080
5455	4.080	5505	4.080	5555	4.080	5605	4.080	5655	4.080	5705	4.080
5456	4.080	5506	4.080	5556	4.080	5606	4.080	5656	4.080	5706	4.080
5457	4.080	5507	4.080	5557	4.080	5607	4.080	5657	4.080	5707	4.080
5458	4.080	5508	4.080	5558	4.080	5608	4.080	5658	4.080	5708	4.080
5459	4.080	5509	4.080	5559	4.080	5609	4.080	5659	4.080	5709	4.080
5460	4.080	5510	4.080	5560	4.080	5610	4.080	5660	4.080	5710	4.080
5461	4.080	5511	4.080	5561	4.080	5611	4.080	5661	4.080	5711	4.080
5462	4.080	5512	4.080	5562	4.080	5612	4.080	5662	4.080	5712	4.080
5463	4.080	5513	4.080	5563	4.080	5613	4.080	5663	4.080	5713	4.080
5464	4.080	5514	4.080	5564	4.080	5614	4.080	5664	4.080	5714	4.080
5465	4.080	5515	4.080	5565	4.080	5615	4.080	5665	4.080	5715	4.080
5466	4.080	5516	4.080	5566	4.080	5616	4.080	5666	4.080	5716	4.080
5467	4.080	5517	4.080	5567	4.080	5617	4.080	5667	4.080	5717	4.080
5468	4.080	5518	4.080	5568	4.080	5618	4.080	5668	4.080	5718	4.080
5469	4.080	5519	4.080	5569	4.080	5619	4.080	5669	4.080	5719	4.080
5470	4.080	5520	4.080	5570	4.080	5620	4.080	5670	4.080	5720	4.080
5471	4.080	5521	4.080	5571	4.080	5621	4.080	5671	4.080	5721	4.080
5472	4.080	5522	4.080	5572	4.080	5622	4.080	5672	4.080	5722	4.080
5473	4.080	5523	4.080	5573	4.080	5623	4.080	5673	4.080	5723	4.080
5474	4.080	5524	4.080	5574	4.080	5624	4.080	5674	4.080	5724	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership						Page 23			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
5725	4.080	5775	4.080	5825	4.080	5875	4.080	5925	4.080
5726	4.080	5776	4.080	5826	4.080	5876	4.080	5926	4.080
5727	4.080	5777	4.080	5827	4.080	5877	4.080	5927	4.080
5728	4.080	5778	4.080	5828	4.080	5878	4.080	5928	4.080
5729	4.080	5779	4.080	5829	4.080	5879	4.080	5929	4.080
5730	4.080	5780	4.080	5830	4.080	5880	4.080	5930	4.080
5731	4.080	5781	4.080	5831	4.080	5881	4.080	5931	4.080
5732	4.080	5782	4.080	5832	4.080	5882	4.080	5932	4.080
5733	4.080	5783	4.080	5833	4.080	5883	4.080	5933	4.080
5734	4.080	5784	4.080	5834	4.080	5884	4.080	5934	4.080
5735	4.080	5785	4.080	5835	4.080	5885	4.080	5935	4.080
5736	4.080	5786	4.080	5836	4.080	5886	4.080	5936	4.080
5737	4.080	5787	4.080	5837	4.080	5887	4.080	5937	4.080
5738	4.080	5788	4.080	5838	4.080	5888	4.080	5938	4.080
5739	4.080	5789	4.080	5839	4.080	5889	4.080	5939	4.080
5740	4.080	5790	4.080	5840	4.080	5890	4.080	5940	4.080
5741	4.080	5791	4.080	5841	4.080	5891	4.080	5941	4.080
5742	4.080	5792	4.080	5842	4.080	5892	4.080	5942	4.080
5743	4.080	5793	4.080	5843	4.080	5893	4.080	5943	4.080
5744	4.080	5794	4.080	5844	4.080	5894	4.080	5944	4.080
5745	4.080	5795	4.080	5845	4.080	5895	4.080	5945	4.080
5746	4.080	5796	4.080	5846	4.080	5896	4.080	5946	4.080
5747	4.080	5797	4.080	5847	4.080	5897	4.080	5947	4.080
5748	4.080	5798	4.080	5848	4.080	5898	4.080	5948	4.080
5749	4.080	5799	4.080	5849	4.080	5899	4.080	5949	4.080
5750	4.080	5800	4.080	5850	4.080	5900	4.080	5950	4.080
5751	4.080	5801	4.080	5851	4.080	5901	4.080	5951	4.080
5752	4.080	5802	4.080	5852	4.080	5902	4.080	5952	4.080
5753	4.080	5803	4.080	5853	4.080	5903	4.080	5953	4.080
5754	4.080	5804	4.080	5854	4.080	5904	4.080	5954	4.080
5755	4.080	5805	4.080	5855	4.080	5905	4.080	5955	4.080
5756	4.080	5806	4.080	5856	4.080	5906	4.080	5956	4.080
5757	4.080	5807	4.080	5857	4.080	5907	4.080	5957	4.080
5758	4.080	5808	4.080	5858	4.080	5908	4.080	5958	4.080
5759	4.080	5809	4.080	5859	4.080	5909	4.080	5959	4.080
5760	4.080	5810	4.080	5860	4.080	5910	4.080	5960	4.080
5761	4.080	5811	4.080	5861	4.080	5911	4.080	5961	4.080
5762	4.080	5812	4.080	5862	4.080	5912	4.080	5962	4.080
5763	4.080	5813	4.080	5863	4.080	5913	4.080	5963	4.080
5764	4.080	5814	4.080	5864	4.080	5914	4.080	5964	4.080
5765	4.080	5815	4.080	5865	4.080	5915	4.080	5965	4.080
5766	4.080	5816	4.080	5866	4.080	5916	4.080	5966	4.080
5767	4.080	5817	4.080	5867	4.080	5917	4.080	5967	4.080
5768	4.080	5818	4.080	5868	4.080	5918	4.080	5968	4.080
5769	4.080	5819	4.080	5869	4.080	5919	4.080	5969	4.080
5770	4.080	5820	4.080	5870	4.080	5920	4.080	5970	4.080
5771	4.080	5821	4.080	5871	4.080	5921	4.080	5971	4.080
5772	4.080	5822	4.080	5872	4.080	5922	4.080	5972	4.080
5773	4.080	5823	4.080	5873	4.080	5923	4.080	5973	4.080
5774	4.080	5824	4.080	5874	4.080	5924	4.080	5974	4.080
5975	4.080	6025	4.080	5975	4.080	6025	4.080	5975	4.080
5976	4.080	6026	4.080	5976	4.080	6026	4.080	5976	4.080
5977	4.080	6027	4.080	5977	4.080	6027	4.080	5977	4.080
5978	4.080	6028	4.080	5978	4.080	6028	4.080	5978	4.080
5979	4.080	6029	4.080	5979	4.080	6029	4.080	5979	4.080
5980	4.080	6030	4.080	5980	4.080	6030	4.080	5980	4.080
5981	4.080	6031	4.080	5981	4.080	6031	4.080	5981	4.080
5982	4.080	6032	4.080	5982	4.080	6032	4.080	5982	4.080
5983	4.080	6033	4.080	5983	4.080	6033	4.080	5983	4.080
5984	4.080	6034	4.080	5984	4.080	6034	4.080	5984	4.080
5985	4.080	6035	4.080	5985	4.080	6035	4.080	5985	4.080
5986	4.080	6036	4.080	5986	4.080	6036	4.080	5986	4.080
5987	4.080	6037	4.080	5987	4.080	6037	4.080	5987	4.080
5988	4.080	6038	4.080	5988	4.080	6038	4.080	5988	4.080
5989	4.080	6039	4.080	5989	4.080	6039	4.080	5989	4.080
5990	4.080	6040	4.080	5990	4.080	6040	4.080	5990	4.080
5991	4.080	6041	4.080	5991	4.080	6041	4.080	5991	4.080
5992	4.080	6042	4.080	5992	4.080	6042	4.080	5992	4.080
5993	4.080	6043	4.080	5993	4.080	6043	4.080	5993	4.080
5994	4.080	6044	4.080	5994	4.080	6044	4.080	5994	4.080
5995	4.080	6045	4.080	5995	4.080	6045	4.080	5995	4.080
5996	4.080	6046	4.080	5996	4.080	6046	4.080	5996	4.080
5997	4.080	6047	4.080	5997	4.080	6047	4.080	5997	4.080
5998	4.080	6048	4.080	5998	4.080	6048	4.080	5998	4.080
5999	4.080	6049	4.080	5999	4.080	6049	4.080	5999	4.080
6000	4.080	6050	4.080	6000	4.080	6050	4.080	6000	4.080
6001	4.080	6051	4.080	6001	4.080	6051	4.080	6001	4.080
6002	4.080	6052	4.080	6002	4.080	6052	4.080	6002	4.080
6003	4.080	6053	4.080	6003	4.080	6053	4.080	6003	4.080
6004	4.080	6054	4.080	6004	4.080	6054	4.080	6004	4.080
6005	4.080	6055	4.080	6005	4.080	6055	4.080	6005	4.080
6006	4.080	6056	4.080	6006	4.080	6056	4.080	6006	4.080
6007	4.080	6057	4.080	6007	4.080	6057	4.080	6007	4.080
6008	4.080	6058	4.080	6008	4.080	6058	4.080	6008	4.080
6009	4.080	6059	4.080	6009	4.080	6059	4.080	6009	4.080
6010	4.080	6060	4.080	6010	4.080	6060	4.080	6010	4.080
6011	4.080	6061	4.080	6011	4.080	6061	4.080	6011	4.080
6012	4.080	6062	4.080	6012	4.080	6062	4.080	6012	4.080
6013	4.080	6063	4.080	6013	4.080	6063	4.080	6013	4.080
6014	4.080	6064	4.080	6014	4.080	6064	4.080	6014	4.080
6015	4.080	6065	4.080	6015	4.080	6065	4.080	6015	4.080
6016	4.080	6066	4.080	6016	4.080	6066	4.080	6016	4.080
6017	4.080	6067	4.080	6017	4.080	6067	4.080	6017	4.080
6018	4.080	6068	4.080	6018	4.080	6068	4.080	6018	4.080
6019	4.080	6069	4.080	6019	4.080	6069	4.080	6019	4.080
6020	4.080	6070	4.080	6020	4.080	6070	4.080	6020	4.080
6021	4.080	6071	4.080	6021	4.080	6071	4.080	6021	4.080
6022	4.080	6072	4.080	6022	4.080	6072	4.080	6022	4.080
6023	4.080	6073	4.080	6023	4.080	6073	4.080	6023	4.080
6024	4.080	6074	4.080	6024	4.080	6074	4.080	6024	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 24			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
6025	4.080	6075	4.080	6125	4.080	6175	4.080	6225	4.080
6026	4.080	6076	4.080	6126	4.080	6176	4.080	6226	4.080
6027	4.080	6077	4.080	6127	4.080	6177	4.080	6227	4.080
6028	4.080	6078	4.080	6128	4.080	6178	4.080	6228	4.080
6029	4.080	6079	4.080	6129	4.080	6179	4.080	6229	4.080
6030	4.080	6080	4.080	6130	4.080	6180	4.080	6230	4.080
6031	4.080	6081	4.080	6131	4.080	6181	4.080	6231	4.080
6032	4.080	6082	4.080	6132	4.080	6182	4.080	6232	4.080
6033	4.080	6083	4.080	6133	4.080	6183	4.080	6233	4.080
6034	4.080	6084	4.080	6134	4.080	6184	4.080	6234	4.080
6035	4.080	6085	4.080	6135	4.080	6185	4.080	6235	4.080
6036	4.080	6086	4.080	6136	4.080	6186	4.080	6236	4.080
6037	4.080	6087	4.080	6137	4.080	6187	4.080	6237	4.080
6038	4.080	6088	4.080	6138	4.080	6188	4.080	6238	4.080
6039	4.080	6089	4.080	6139	4.080	6189	4.080	6239	4.080
6040	4.080	6090	4.080	6140	4.080	6190	4.080	6240	4.080
6041	4.080	6091	4.080	6141	4.080	6191	4.080	6241	4.080
6042	4.080	6092	4.080	6142	4.080	6192	4.080	6242	4.080
6043	4.080	6093	4.080	6143	4.080	6193	4.080	6243	4.080
6044	4.080	6094	4.080	6144	4.080	6194	4.080	6244	4.080
6045	4.080	6095	4.080	6145	4.080	6195	4.080	6245	4.080
6046	4.080	6096	4.080	6146	4.080	6196	4.080	6246	4.080
6047	4.080	6097	4.080	6147	4.080	6197	4.080	6247	4.080
6048	4.080	6098	4.080	6148	4.080	6198	4.080	6248	4.080
6049	4.080	6099	4.080	6149	4.080	6199	4.080	6249	4.080
6050	4.080	6100	4.080	6150	4.080	6200	4.080	6250	4.080
6051	4.080	6101	4.080	6151	4.080	6201	4.080	6251	4.080
6052	4.080	6102	4.080	6152	4.080	6202	4.080	6252	4.080
6053	4.080	6103	4.080	6153	4.080	6203	4.080	6253	4.080
6054	4.080	6104	4.080	6154	4.080	6204	4.080	6254	4.080
6055	4.080	6105	4.080	6155	4.080	6205	4.080	6255	4.080
6056	4.080	6106	4.080	6156	4.080	6206	4.080	6256	4.080
6057	4.080	6107	4.080	6157	4.080	6207	4.080	6257	4.080
6058	4.080	6108	4.080	6158	4.080	6208	4.080	6258	4.080
6059	4.080	6109	4.080	6159	4.080	6209	4.080	6259	4.080
6060	4.080	6110	4.080	6160	4.080	6210	4.080	6260	4.080
6061	4.080	6111	4.080	6161	4.080	6211	4.080	6261	4.080
6062	4.080	6112	4.080	6162	4.080	6212	4.080	6262	4.080
6063	4.080	6113	4.080	6163	4.080	6213	4.080	6263	4.080
6064	4.080	6114	4.080	6164	4.080	6214	4.080	6264	4.080
6065	4.080	6115	4.080	6165	4.080	6215	4.080	6265	4.080
6066	4.080	6116	4.080	6166	4.080	6216	4.080	6266	4.080
6067	4.080	6117	4.080	6167	4.080	6217	4.080	6267	4.080
6068	4.080	6118	4.080	6168	4.080	6218	4.080	6268	4.080
6069	4.080	6119	4.080	6169	4.080	6219	4.080	6269	4.080
6070	4.080	6120	4.080	6170	4.080	6220	4.080	6270	4.080
6071	4.080	6121	4.080	6171	4.080	6221	4.080	6271	4.080
6072	4.080	6122	4.080	6172	4.080	6222	4.080	6272	4.080
6073	4.080	6123	4.080	6173	4.080	6223	4.080	6273	4.080
6074	4.080	6124	4.080	6174	4.080	6224	4.080	6274	4.080
6275	4.080	6275	4.080	6325	4.080	6375	4.080	6275	4.080
6276	4.080	6276	4.080	6326	4.080	6376	4.080	6276	4.080
6277	4.080	6277	4.080	6327	4.080	6377	4.080	6277	4.080
6278	4.080	6278	4.080	6328	4.080	6378	4.080	6278	4.080
6279	4.080	6279	4.080	6329	4.080	6379	4.080	6279	4.080
6280	4.080	6280	4.080	6330	4.080	6380	4.080	6280	4.080
6281	4.080	6281	4.080	6331	4.080	6381	4.080	6281	4.080
6282	4.080	6282	4.080	6332	4.080	6382	4.080	6282	4.080
6283	4.080	6283	4.080	6333	4.080	6383	4.080	6283	4.080
6284	4.080	6284	4.080	6334	4.080	6384	4.080	6284	4.080
6285	4.080	6285	4.080	6335	4.080	6385	4.080	6285	4.080
6286	4.080	6286	4.080	6336	4.080	6386	4.080	6286	4.080
6287	4.080	6287	4.080	6337	4.080	6387	4.080	6287	4.080
6288	4.080	6288	4.080	6338	4.080	6388	4.080	6288	4.080
6289	4.080	6289	4.080	6339	4.080	6389	4.080	6289	4.080
6290	4.080	6290	4.080	6340	4.080	6390	4.080	6290	4.080
6291	4.080	6291	4.080	6341	4.080	6391	4.080	6291	4.080
6292	4.080	6292	4.080	6342	4.080	6392	4.080	6292	4.080
6293	4.080	6293	4.080	6343	4.080	6393	4.080	6293	4.080
6294	4.080	6294	4.080	6344	4.080	6394	4.080	6294	4.080
6295	4.080	6295	4.080	6345	4.080	6395	4.080	6295	4.080
6296	4.080	6296	4.080	6346	4.080	6396	4.080	6296	4.080
6297	4.080	6297	4.080	6347	4.080	6397	4.080	6297	4.080
6298	4.080	6298	4.080	6348	4.080	6398	4.080	6298	4.080
6299	4.080	6299	4.080	6349	4.080	6399	4.080	6299	4.080
6300	4.080	6300	4.080	6350	4.080	6400	4.080	6300	4.080
6301	4.080	6301	4.080	6351	4.080	6401	4.080	6301	4.080
6302	4.080	6302	4.080	6352	4.080	6402	4.080	6302	4.080
6303	4.080	6303	4.080	6353	4.080	6403	4.080	6303	4.080
6304	4.080	6304	4.080	6354	4.080	6404	4.080	6304	4.080
6305	4.080	6305	4.080	6355	4.080	6405	4.080	6305	4.080
6306	4.080	6306	4.080	6356	4.080	6406	4.080	6306	4.080
6307	4.080	6307	4.080	6357	4.080	6407	4.080	6307	4.080
6308	4.080	6308	4.080	6358	4.080	6408	4.080	6308	4.080
6309	4.080	6309	4.080	6359	4.080	6409	4.080	6309	4.080
6310	4.080	6310	4.080	6360	4.080	6410	4.080	6310	4.080
6311	4.080	6311	4.080	6361	4.080	6411	4.080	6311	4.080
6312	4.080	6312	4.080	6362	4.080	6412	4.080	6312	4.080
6313	4.080	6313	4.080	6363	4.080	6413	4.080	6313	4.080
6314	4.080	6314	4.080	6364	4.080	6414	4.080	6314	4.080
6315	4.080	6315	4.080	6365	4.080	6415	4.080	6315	4.080
6316	4.080	6316	4.080	6366	4.080	6416	4.080	6316	4.080
6317	4.080	6317	4.080	6367	4.080	6417	4.080	6317	4.080
6318	4.080	6318	4.080	6368	4.080	6418	4.080	6318	4.080
6319	4.080	6319	4.080	6369	4.080	6419	4.080	6319	4.080
6320	4.080	6320	4.080	6370	4.080	6420	4.080	6320	4.080
6321	4.080	6321	4.080	6371	4.080	6421	4.080	6321	4.080
6322	4.080	6322	4.080	6372	4.080	6422	4.080	6322	4.080
6323	4.080	6323	4.080	6373	4.080	6423	4.080	6323	4.080
6324	4.080	6324	4.080	6374	4.080	6424	4.080	6324	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 25			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
6325	4.080	6375	4.080	6425	4.080	6475	4.080	6525	4.080
6326	4.080	6376	4.080	6426	4.080	6476	4.080	6526	4.080
6327	4.080	6377	4.080	6427	4.080	6477	4.080	6527	4.080
6328	4.080	6378	4.080	6428	4.080	6478	4.080	6528	4.080
6329	4.080	6379	4.080	6429	4.080	6479	4.080	6529	4.080
6330	4.080	6380	4.080	6430	4.080	6480	4.080	6530	4.080
6331	4.080	6381	4.080	6431	4.080	6481	4.080	6531	4.080
6332	4.080	6382	4.080	6432	4.080	6482	4.080	6532	4.080
6333	4.080	6383	4.080	6433	4.080	6483	4.080	6533	4.080
6334	4.080	6384	4.080	6434	4.080	6484	4.080	6534	4.080
6335	4.080	6385	4.080	6435	4.080	6485	4.080	6535	4.080
6336	4.080	6386	4.080	6436	4.080	6486	4.080	6536	4.080
6337	4.080	6387	4.080	6437	4.080	6487	4.080	6537	4.080
6338	4.080	6388	4.080	6438	4.080	6488	4.080	6538	4.080
6339	4.080	6389	4.080	6439	4.080	6489	4.080	6539	4.080
6340	4.080	6390	4.080	6440	4.080	6490	4.080	6540	4.080
6341	4.080	6391	4.080	6441	4.080	6491	4.080	6541	4.080
6342	4.080	6392	4.080	6442	4.080	6492	4.080	6542	4.080
6343	4.080	6393	4.080	6443	4.080	6493	4.080	6543	4.080
6344	4.080	6394	4.080	6444	4.080	6494	4.080	6544	4.080
6345	4.080	6395	4.080	6445	4.080	6495	4.080	6545	4.080
6346	4.080	6396	4.080	6446	4.080	6496	4.080	6546	4.080
6347	4.080	6397	4.080	6447	4.080	6497	4.080	6547	4.080
6348	4.080	6398	4.080	6448	4.080	6498	4.080	6548	4.080
6349	4.080	6399	4.080	6449	4.080	6499	4.080	6549	4.080
6350	4.080	6400	4.080	6450	4.080	6500	4.080	6550	4.080
6351	4.080	6401	4.080	6451	4.080	6501	4.080	6551	4.080
6352	4.080	6402	4.080	6452	4.080	6502	4.080	6552	4.080
6353	4.080	6403	4.080	6453	4.080	6503	4.080	6553	4.080
6354	4.080	6404	4.080	6454	4.080	6504	4.080	6554	4.080
6355	4.080	6405	4.080	6455	4.080	6505	4.080	6555	4.080
6356	4.080	6406	4.080	6456	4.080	6506	4.080	6556	4.080
6357	4.080	6407	4.080	6457	4.080	6507	4.080	6557	4.080
6358	4.080	6408	4.080	6458	4.080	6508	4.080	6558	4.080
6359	4.080	6409	4.080	6459	4.080	6509	4.080	6559	4.080
6360	4.080	6410	4.080	6460	4.080	6510	4.080	6560	4.080
6361	4.080	6411	4.080	6461	4.080	6511	4.080	6561	4.080
6362	4.080	6412	4.080	6462	4.080	6512	4.080	6562	4.080
6363	4.080	6413	4.080	6463	4.080	6513	4.080	6563	4.080
6364	4.080	6414	4.080	6464	4.080	6514	4.080	6564	4.080
6365	4.080	6415	4.080	6465	4.080	6515	4.080	6565	4.080
6366	4.080	6416	4.080	6466	4.080	6516	4.080	6566	4.080
6367	4.080	6417	4.080	6467	4.080	6517	4.080	6567	4.080
6368	4.080	6418	4.080	6468	4.080	6518	4.080	6568	4.080
6369	4.080	6419	4.080	6469	4.080	6519	4.080	6569	4.080
6370	4.080	6420	4.080	6470	4.080	6520	4.080	6570	4.080
6371	4.080	6421	4.080	6471	4.080	6521	4.080	6571	4.080
6372	4.080	6422	4.080	6472	4.080	6522	4.080	6572	4.080
6373	4.080	6423	4.080	6473	4.080	6523	4.080	6573	4.080
6374	4.080	6424	4.080	6474	4.080	6524	4.080	6574	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 26			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
6625	4.080	6675	4.080	6725	4.080	6775	4.080	6825	4.080
6626	4.080	6676	4.080	6726	4.080	6776	4.080	6826	4.080
6627	4.080	6677	4.080	6727	4.080	6777	4.080	6827	4.080
6628	4.080	6678	4.080	6728	4.080	6778	4.080	6828	4.080
6629	4.080	6679	4.080	6729	4.080	6779	4.080	6829	4.080
6630	4.080	6680	4.080	6730	4.080	6780	4.080	6830	4.080
6631	4.080	6681	4.080	6731	4.080	6781	4.080	6831	4.080
6632	4.080	6682	4.080	6732	4.080	6782	4.080	6832	4.080
6633	4.080	6683	4.080	6733	4.080	6783	4.080	6833	4.080
6634	4.080	6684	4.080	6734	4.080	6784	4.080	6834	4.080
6635	4.080	6685	4.080	6735	4.080	6785	4.080	6835	4.080
6636	4.080	6686	4.080	6736	4.080	6786	4.080	6836	4.080
6637	4.080	6687	4.080	6737	4.080	6787	4.080	6837	4.080
6638	4.080	6688	4.080	6738	4.080	6788	4.080	6838	4.080
6639	4.080	6689	4.080	6739	4.080	6789	4.080	6839	4.080
6640	4.080	6690	4.080	6740	4.080	6790	4.080	6840	4.080
6641	4.080	6691	4.080	6741	4.080	6791	4.080	6841	4.080
6642	4.080	6692	4.080	6742	4.080	6792	4.080	6842	4.080
6643	4.080	6693	4.080	6743	4.080	6793	4.080	6843	4.080
6644	4.080	6694	4.080	6744	4.080	6794	4.080	6844	4.080
6645	4.080	6695	4.080	6745	4.080	6795	4.080	6845	4.080
6646	4.080	6696	4.080	6746	4.080	6796	4.080	6846	4.080
6647	4.080	6697	4.080	6747	4.080	6797	4.080	6847	4.080
6648	4.080	6698	4.080	6748	4.080	6798	4.080	6848	4.080
6649	4.080	6699	4.080	6749	4.080	6799	4.080	6849	4.080
6650	4.080	6700	4.080	6750	4.080	6800	4.080	6850	4.080
6651	4.080	6701	4.080	6751	4.080	6801	4.080	6851	4.080
6652	4.080	6702	4.080	6752	4.080	6802	4.080	6852	4.080
6653	4.080	6703	4.080	6753	4.080	6803	4.080	6853	4.080
6654	4.080	6704	4.080	6754	4.080	6804	4.080	6854	4.080
6655	4.080	6705	4.080	6755	4.080	6805	4.080	6855	4.080
6656	4.080	6706	4.080	6756	4.080	6806	4.080	6856	4.080
6657	4.080	6707	4.080	6757	4.080	6807	4.080	6857	4.080
6658	4.080	6708	4.080	6758	4.080	6808	4.080	6858	4.080
6659	4.080	6709	4.080	6759	4.080	6809	4.080	6859	4.080
6660	4.080	6710	4.080	6760	4.080	6810	4.080	6860	4.080
6661	4.080	6711	4.080	6761	4.080	6811	4.080	6861	4.080
6662	4.080	6712	4.080	6762	4.080	6812	4.080	6862	4.080
6663	4.080	6713	4.080	6763	4.080	6813	4.080	6863	4.080
6664	4.080	6714	4.080	6764	4.080	6814	4.080	6864	4.080
6665	4.080	6715	4.080	6765	4.080	6815	4.080	6865	4.080
6666	4.080	6716	4.080	6766	4.080	6816	4.080	6866	4.080
6667	4.080	6717	4.080	6767	4.080	6817	4.080	6867	4.080
6668	4.080	6718	4.080	6768	4.080	6818	4.080	6868	4.080
6669	4.080	6719	4.080	6769	4.080	6819	4.080	6869	4.080
6670	4.080	6720	4.080	6770	4.080	6820	4.080	6870	4.080
6671	4.080	6721	4.080	6771	4.080	6821	4.080	6871	4.080
6672	4.080	6722	4.080	6772	4.080	6822	4.080	6872	4.080
6673	4.080	6723	4.080	6773	4.080	6823	4.080	6873	4.080
6674	4.080	6724	4.080	6774	4.080	6824	4.080	6874	4.080
								6875	4.080
								6876	4.080
								6877	4.080
								6878	4.080
								6879	4.080
								6880	4.080
								6881	4.080
								6882	4.080
								6883	4.080
								6884	4.080
								6885	4.080
								6886	4.080
								6887	4.080
								6888	4.080
								6889	4.080
								6890	4.080
								6891	4.080
								6892	4.080
								6893	4.080
								6894	4.080
								6895	4.080
								6896	4.080
								6897	4.080
								6898	4.080
								6899	4.080
								6900	4.080
								6901	4.080
								6902	4.080
								6903	4.080
								6904	4.080
								6905	4.080
								6906	4.080
								6907	4.080
								6908	4.080
								6909	4.080
								6910	4.080
								6911	4.080
								6912	4.080
								6913	4.080
								6914	4.080
								6915	4.080
								6916	4.080
								6917	4.080
								6918	4.080
								6919	4.080
								6920	4.080
								6921	4.080
								6922	4.080
								6923	4.080
								6924	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 27			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
6925	4.080	6975	4.080	7025	4.080	7075	4.080	7125	4.080	7175	4.080
6926	4.080	6976	4.080	7026	4.080	7076	4.080	7126	4.080	7176	4.080
6927	4.080	6977	4.080	7027	4.080	7077	4.080	7127	4.080	7177	4.080
6928	4.080	6978	4.080	7028	4.080	7078	4.080	7128	4.080	7178	4.080
6929	4.080	6979	4.080	7029	4.080	7079	4.080	7129	4.080	7179	4.080
6930	4.080	6980	4.080	7030	4.080	7080	4.080	7130	4.080	7180	4.080
6931	4.080	6981	4.080	7031	4.080	7081	4.080	7131	4.080	7181	4.080
6932	4.080	6982	4.080	7032	4.080	7082	4.080	7132	4.080	7182	4.080
6933	4.080	6983	4.080	7033	4.080	7083	4.080	7133	4.080	7183	4.080
6934	4.080	6984	4.080	7034	4.080	7084	4.080	7134	4.080	7184	4.080
6935	4.080	6985	4.080	7035	4.080	7085	4.080	7135	4.080	7185	4.080
6936	4.080	6986	4.080	7036	4.080	7086	4.080	7136	4.080	7186	4.080
6937	4.080	6987	4.080	7037	4.080	7087	4.080	7137	4.080	7187	4.080
6938	4.080	6988	4.080	7038	4.080	7088	4.080	7138	4.080	7188	4.080
6939	4.080	6989	4.080	7039	4.080	7089	4.080	7139	4.080	7189	4.080
6940	4.080	6990	4.080	7040	4.080	7090	4.080	7140	4.080	7190	4.080
6941	4.080	6991	4.080	7041	4.080	7091	4.080	7141	4.080	7191	4.080
6942	4.080	6992	4.080	7042	4.080	7092	4.080	7142	4.080	7192	4.080
6943	4.080	6993	4.080	7043	4.080	7093	4.080	7143	4.080	7193	4.080
6944	4.080	6994	4.080	7044	4.080	7094	4.080	7144	4.080	7194	4.080
6945	4.080	6995	4.080	7045	4.080	7095	4.080	7145	4.080	7195	4.080
6946	4.080	6996	4.080	7046	4.080	7096	4.080	7146	4.080	7196	4.080
6947	4.080	6997	4.080	7047	4.080	7097	4.080	7147	4.080	7197	4.080
6948	4.080	6998	4.080	7048	4.080	7098	4.080	7148	4.080	7198	4.080
6949	4.080	6999	4.080	7049	4.080	7099	4.080	7149	4.080	7199	4.080
6950	4.080	7000	4.080	7050	4.080	7100	4.080	7150	4.080	7200	4.080
6951	4.080	7001	4.080	7051	4.080	7101	4.080	7151	4.080	7201	4.080
6952	4.080	7002	4.080	7052	4.080	7102	4.080	7152	4.080	7202	4.080
6953	4.080	7003	4.080	7053	4.080	7103	4.080	7153	4.080	7203	4.080
6954	4.080	7004	4.080	7054	4.080	7104	4.080	7154	4.080	7204	4.080
6955	4.080	7005	4.080	7055	4.080	7105	4.080	7155	4.080	7205	4.080
6956	4.080	7006	4.080	7056	4.080	7106	4.080	7156	4.080	7206	4.080
6957	4.080	7007	4.080	7057	4.080	7107	4.080	7157	4.080	7207	4.080
6958	4.080	7008	4.080	7058	4.080	7108	4.080	7158	4.080	7208	4.080
6959	4.080	7009	4.080	7059	4.080	7109	4.080	7159	4.080	7209	4.080
6960	4.080	7010	4.080	7060	4.080	7110	4.080	7160	4.080	7210	4.080
6961	4.080	7011	4.080	7061	4.080	7111	4.080	7161	4.080	7211	4.080
6962	4.080	7012	4.080	7062	4.080	7112	4.080	7162	4.080	7212	4.080
6963	4.080	7013	4.080	7063	4.080	7113	4.080	7163	4.080	7213	4.080
6964	4.080	7014	4.080	7064	4.080	7114	4.080	7164	4.080	7214	4.080
6965	4.080	7015	4.080	7065	4.080	7115	4.080	7165	4.080	7215	4.080
6966	4.080	7016	4.080	7066	4.080	7116	4.080	7166	4.080	7216	4.080
6967	4.080	7017	4.080	7067	4.080	7117	4.080	7167	4.080	7217	4.080
6968	4.080	7018	4.080	7068	4.080	7118	4.080	7168	4.080	7218	4.080
6969	4.080	7019	4.080	7069	4.080	7119	4.080	7169	4.080	7219	4.080
6970	4.080	7020	4.080	7070	4.080	7120	4.080	7170	4.080	7220	4.080
6971	4.080	7021	4.080	7071	4.080	7121	4.080	7171	4.080	7221	4.080
6972	4.080	7022	4.080	7072	4.080	7122	4.080	7172	4.080	7222	4.080
6973	4.080	7023	4.080	7073	4.080	7123	4.080	7173	4.080	7223	4.080
6974	4.080	7024	4.080	7074	4.080	7124	4.080	7174	4.080	7224	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership						Page 28			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
7225	4.080	7275	4.080	7325	4.080	7375	4.080	7425	4.080
7226	4.080	7276	4.080	7326	4.080	7376	4.080	7426	4.080
7227	4.080	7277	4.080	7327	4.080	7377	4.080	7427	4.080
7228	4.080	7278	4.080	7328	4.080	7378	4.080	7428	4.080
7229	4.080	7279	4.080	7329	4.080	7379	4.080	7429	4.080
7230	4.080	7280	4.080	7330	4.080	7380	4.080	7430	4.080
7231	4.080	7281	4.080	7331	4.080	7381	4.080	7431	4.080
7232	4.080	7282	4.080	7332	4.080	7382	4.080	7432	4.080
7233	4.080	7283	4.080	7333	4.080	7383	4.080	7433	4.080
7234	4.080	7284	4.080	7334	4.080	7384	4.080	7434	4.080
7235	4.080	7285	4.080	7335	4.080	7385	4.080	7435	4.080
7236	4.080	7286	4.080	7336	4.080	7386	4.080	7436	4.080
7237	4.080	7287	4.080	7337	4.080	7387	4.080	7437	4.080
7238	4.080	7288	4.080	7338	4.080	7388	4.080	7438	4.080
7239	4.080	7289	4.080	7339	4.080	7389	4.080	7439	4.080
7240	4.080	7290	4.080	7340	4.080	7390	4.080	7440	4.080
7241	4.080	7291	4.080	7341	4.080	7391	4.080	7441	4.080
7242	4.080	7292	4.080	7342	4.080	7392	4.080	7442	4.080
7243	4.080	7293	4.080	7343	4.080	7393	4.080	7443	4.080
7244	4.080	7294	4.080	7344	4.080	7394	4.080	7444	4.080
7245	4.080	7295	4.080	7345	4.080	7395	4.080	7445	4.080
7246	4.080	7296	4.080	7346	4.080	7396	4.080	7446	4.080
7247	4.080	7297	4.080	7347	4.080	7397	4.080	7447	4.080
7248	4.080	7298	4.080	7348	4.080	7398	4.080	7448	4.080
7249	4.080	7299	4.080	7349	4.080	7399	4.080	7449	4.080
7250	4.080	7300	4.080	7350	4.080	7400	4.080	7450	4.080
7251	4.080	7301	4.080	7351	4.080	7401	4.080	7451	4.080
7252	4.080	7302	4.080	7352	4.080	7402	4.080	7452	4.080
7253	4.080	7303	4.080	7353	4.080	7403	4.080	7453	4.080
7254	4.080	7304	4.080	7354	4.080	7404	4.080	7454	4.080
7255	4.080	7305	4.080	7355	4.080	7405	4.080	7455	4.080
7256	4.080	7306	4.080	7356	4.080	7406	4.080	7456	4.080
7257	4.080	7307	4.080	7357	4.080	7407	4.080	7457	4.080
7258	4.080	7308	4.080	7358	4.080	7408	4.080	7458	4.080
7259	4.080	7309	4.080	7359	4.080	7409	4.080	7459	4.080
7260	4.080	7310	4.080	7360	4.080	7410	4.080	7460	4.080
7261	4.080	7311	4.080	7361	4.080	7411	4.080	7461	4.080
7262	4.080	7312	4.080	7362	4.080	7412	4.080	7462	4.080
7263	4.080	7313	4.080	7363	4.080	7413	4.080	7463	4.080
7264	4.080	7314	4.080	7364	4.080	7414	4.080	7464	4.080
7265	4.080	7315	4.080	7365	4.080	7415	4.080	7465	4.080
7266	4.080	7316	4.080	7366	4.080	7416	4.080	7466	4.080
7267	4.080	7317	4.080	7367	4.080	7417	4.080	7467	4.080
7268	4.080	7318	4.080	7368	4.080	7418	4.080	7468	4.080
7269	4.080	7319	4.080	7369	4.080	7419	4.080	7469	4.080
7270	4.080	7320	4.080	7370	4.080	7420	4.080	7470	4.080
7271	4.080	7321	4.080	7371	4.080	7421	4.080	7471	4.080
7272	4.080	7322	4.080	7372	4.080	7422	4.080	7472	4.080
7273	4.080	7323	4.080	7373	4.080	7423	4.080	7473	4.080
7274	4.080	7324	4.080	7374	4.080	7424	4.080	7474	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 29			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
7525	4.080	7575	4.080	7625	4.080	7675	4.080	7725	4.080
7526	4.080	7576	4.080	7626	4.080	7676	4.080	7726	4.080
7527	4.080	7577	4.080	7627	4.080	7677	4.080	7727	4.080
7528	4.080	7578	4.080	7628	4.080	7678	4.080	7728	4.080
7529	4.080	7579	4.080	7629	4.080	7679	4.080	7729	4.080
7530	4.080	7580	4.080	7630	4.080	7680	4.080	7730	4.080
7531	4.080	7581	4.080	7631	4.080	7681	4.080	7731	4.080
7532	4.080	7582	4.080	7632	4.080	7682	4.080	7732	4.080
7533	4.080	7583	4.080	7633	4.080	7683	4.080	7733	4.080
7534	4.080	7584	4.080	7634	4.080	7684	4.080	7734	4.080
7535	4.080	7585	4.080	7635	4.080	7685	4.080	7735	4.080
7536	4.080	7586	4.080	7636	4.080	7686	4.080	7736	4.080
7537	4.080	7587	4.080	7637	4.080	7687	4.080	7737	4.080
7538	4.080	7588	4.080	7638	4.080	7688	4.080	7738	4.080
7539	4.080	7589	4.080	7639	4.080	7689	4.080	7739	4.080
7540	4.080	7590	4.080	7640	4.080	7690	4.080	7740	4.080
7541	4.080	7591	4.080	7641	4.080	7691	4.080	7741	4.080
7542	4.080	7592	4.080	7642	4.080	7692	4.080	7742	4.080
7543	4.080	7593	4.080	7643	4.080	7693	4.080	7743	4.080
7544	4.080	7594	4.080	7644	4.080	7694	4.080	7744	4.080
7545	4.080	7595	4.080	7645	4.080	7695	4.080	7745	4.080
7546	4.080	7596	4.080	7646	4.080	7696	4.080	7746	4.080
7547	4.080	7597	4.080	7647	4.080	7697	4.080	7747	4.080
7548	4.080	7598	4.080	7648	4.080	7698	4.080	7748	4.080
7549	4.080	7599	4.080	7649	4.080	7699	4.080	7749	4.080
7550	4.080	7600	4.080	7650	4.080	7700	4.080	7750	4.080
7551	4.080	7601	4.080	7651	4.080	7701	4.080	7751	4.080
7552	4.080	7602	4.080	7652	4.080	7702	4.080	7752	4.080
7553	4.080	7603	4.080	7653	4.080	7703	4.080	7753	4.080
7554	4.080	7604	4.080	7654	4.080	7704	4.080	7754	4.080
7555	4.080	7605	4.080	7655	4.080	7705	4.080	7755	4.080
7556	4.080	7606	4.080	7656	4.080	7706	4.080	7756	4.080
7557	4.080	7607	4.080	7657	4.080	7707	4.080	7757	4.080
7558	4.080	7608	4.080	7658	4.080	7708	4.080	7758	4.080
7559	4.080	7609	4.080	7659	4.080	7709	4.080	7759	4.080
7560	4.080	7610	4.080	7660	4.080	7710	4.080	7760	4.080
7561	4.080	7611	4.080	7661	4.080	7711	4.080	7761	4.080
7562	4.080	7612	4.080	7662	4.080	7712	4.080	7762	4.080
7563	4.080	7613	4.080	7663	4.080	7713	4.080	7763	4.080
7564	4.080	7614	4.080	7664	4.080	7714	4.080	7764	4.080
7565	4.080	7615	4.080	7665	4.080	7715	4.080	7765	4.080
7566	4.080	7616	4.080	7666	4.080	7716	4.080	7766	4.080
7567	4.080	7617	4.080	7667	4.080	7717	4.080	7767	4.080
7568	4.080	7618	4.080	7668	4.080	7718	4.080	7768	4.080
7569	4.080	7619	4.080	7669	4.080	7719	4.080	7769	4.080
7570	4.080	7620	4.080	7670	4.080	7720	4.080	7770	4.080
7571	4.080	7621	4.080	7671	4.080	7721	4.080	7771	4.080
7572	4.080	7622	4.080	7672	4.080	7722	4.080	7772	4.080
7573	4.080	7623	4.080	7673	4.080	7723	4.080	7773	4.080
7574	4.080	7624	4.080	7674	4.080	7724	4.080	7774	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 30			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
7825	4.080	7875	4.080	7925	4.080	7975	4.080	8025	4.080
7826	4.080	7876	4.080	7926	4.080	7976	4.080	8026	4.080
7827	4.080	7877	4.080	7927	4.080	7977	4.080	8027	4.080
7828	4.080	7878	4.080	7928	4.080	7978	4.080	8028	4.080
7829	4.080	7879	4.080	7929	4.080	7979	4.080	8029	4.080
7830	4.080	7880	4.080	7930	4.080	7980	4.080	8030	4.080
7831	4.080	7881	4.080	7931	4.080	7981	4.080	8031	4.080
7832	4.080	7882	4.080	7932	4.080	7982	4.080	8032	4.080
7833	4.080	7883	4.080	7933	4.080	7983	4.080	8033	4.080
7834	4.080	7884	4.080	7934	4.080	7984	4.080	8034	4.080
7835	4.080	7885	4.080	7935	4.080	7985	4.080	8035	4.080
7836	4.080	7886	4.080	7936	4.080	7986	4.080	8036	4.080
7837	4.080	7887	4.080	7937	4.080	7987	4.080	8037	4.080
7838	4.080	7888	4.080	7938	4.080	7988	4.080	8038	4.080
7839	4.080	7889	4.080	7939	4.080	7989	4.080	8039	4.080
7840	4.080	7890	4.080	7940	4.080	7990	4.080	8040	4.080
7841	4.080	7891	4.080	7941	4.080	7991	4.080	8041	4.080
7842	4.080	7892	4.080	7942	4.080	7992	4.080	8042	4.080
7843	4.080	7893	4.080	7943	4.080	7993	4.080	8043	4.080
7844	4.080	7894	4.080	7944	4.080	7994	4.080	8044	4.080
7845	4.080	7895	4.080	7945	4.080	7995	4.080	8045	4.080
7846	4.080	7896	4.080	7946	4.080	7996	4.080	8046	4.080
7847	4.080	7897	4.080	7947	4.080	7997	4.080	8047	4.080
7848	4.080	7898	4.080	7948	4.080	7998	4.080	8048	4.080
7849	4.080	7899	4.080	7949	4.080	7999	4.080	8049	4.080
7850	4.080	7900	4.080	7950	4.080	8000	4.080	8050	4.080
7851	4.080	7901	4.080	7951	4.080	8001	4.080	8051	4.080
7852	4.080	7902	4.080	7952	4.080	8002	4.080	8052	4.080
7853	4.080	7903	4.080	7953	4.080	8003	4.080	8053	4.080
7854	4.080	7904	4.080	7954	4.080	8004	4.080	8054	4.080
7855	4.080	7905	4.080	7955	4.080	8005	4.080	8055	4.080
7856	4.080	7906	4.080	7956	4.080	8006	4.080	8056	4.080
7857	4.080	7907	4.080	7957	4.080	8007	4.080	8057	4.080
7858	4.080	7908	4.080	7958	4.080	8008	4.080	8058	4.080
7859	4.080	7909	4.080	7959	4.080	8009	4.080	8059	4.080
7860	4.080	7910	4.080	7960	4.080	8010	4.080	8060	4.080
7861	4.080	7911	4.080	7961	4.080	8011	4.080	8061	4.080
7862	4.080	7912	4.080	7962	4.080	8012	4.080	8062	4.080
7863	4.080	7913	4.080	7963	4.080	8013	4.080	8063	4.080
7864	4.080	7914	4.080	7964	4.080	8014	4.080	8064	4.080
7865	4.080	7915	4.080	7965	4.080	8015	4.080	8065	4.080
7866	4.080	7916	4.080	7966	4.080	8016	4.080	8066	4.080
7867	4.080	7917	4.080	7967	4.080	8017	4.080	8067	4.080
7868	4.080	7918	4.080	7968	4.080	8018	4.080	8068	4.080
7869	4.080	7919	4.080	7969	4.080	8019	4.080	8069	4.080
7870	4.080	7920	4.080	7970	4.080	8020	4.080	8070	4.080
7871	4.080	7921	4.080	7971	4.080	8021	4.080	8071	4.080
7872	4.080	7922	4.080	7972	4.080	8022	4.080	8072	4.080
7873	4.080	7923	4.080	7973	4.080	8023	4.080	8073	4.080
7874	4.080	7924	4.080	7974	4.080	8024	4.080	8074	4.080
8075	4.080	8075	4.080	8075	4.080	8075	4.080	8075	4.080
8076	4.080	8076	4.080	8076	4.080	8076	4.080	8076	4.080
8077	4.080	8077	4.080	8077	4.080	8077	4.080	8077	4.080
8078	4.080	8078	4.080	8078	4.080	8078	4.080	8078	4.080
8079	4.080	8079	4.080	8079	4.080	8079	4.080	8079	4.080
8080	4.080	8080	4.080	8080	4.080	8080	4.080	8080	4.080
8081	4.080	8081	4.080	8081	4.080	8081	4.080	8081	4.080
8082	4.080	8082	4.080	8082	4.080	8082	4.080	8082	4.080
8083	4.080	8083	4.080	8083	4.080	8083	4.080	8083	4.080
8084	4.080	8084	4.080	8084	4.080	8084	4.080	8084	4.080
8085	4.080	8085	4.080	8085	4.080	8085	4.080	8085	4.080
8086	4.080	8086	4.080	8086	4.080	8086	4.080	8086	4.080
8087	4.080	8087	4.080	8087	4.080	8087	4.080	8087	4.080
8088	4.080	8088	4.080	8088	4.080	8088	4.080	8088	4.080
8089	4.080	8089	4.080	8089	4.080	8089	4.080	8089	4.080
8090	4.080	8090	4.080	8090	4.080	8090	4.080	8090	4.080
8091	4.080	8091	4.080	8091	4.080	8091	4.080	8091	4.080
8092	4.080	8092	4.080	8092	4.080	8092	4.080	8092	4.080
8093	4.080	8093	4.080	8093	4.080	8093	4.080	8093	4.080
8094	4.080	8094	4.080	8094	4.080	8094	4.080	8094	4.080
8095	4.080	8095	4.080	8095	4.080	8095	4.080	8095	4.080
8096	4.080	8096	4.080	8096	4.080	8096	4.080	8096	4.080
8097	4.080	8097	4.080	8097	4.080	8097	4.080	8097	4.080
8098	4.080	8098	4.080	8098	4.080	8098	4.080	8098	4.080
8099	4.080	8099	4.080	8099	4.080	8099	4.080	8099	4.080
8100	4.080	8100	4.080	8100	4.080	8100	4.080	8100	4.080
8101	4.080	8101	4.080	8101	4.080	8101	4.080	8101	4.080
8102	4.080	8102	4.080	8102	4.080	8102	4.080	8102	4.080
8103	4.080	8103	4.080	8103	4.080	8103	4.080	8103	4.080
8104	4.080	8104	4.080	8104	4.080	8104	4.080	8104	4.080
8105	4.080	8105	4.080	8105	4.080	8105	4.080	8105	4.080
8106	4.080	8106	4.080	8106	4.080	8106	4.080	8106	4.080
8107	4.080	8107	4.080	8107	4.080	8107	4.080	8107	4.080
8108	4.080	8108	4.080	8108	4.080	8108	4.080	8108	4.080
8109	4.080	8109	4.080	8109	4.080	8109	4.080	8109	4.080
8110	4.080	8110	4.080	8110	4.080	8110	4.080	8110	4.080
8111	4.080	8111	4.080	8111	4.080	8111	4.080	8111	4.080
8112	4.080	8112	4.080	8112	4.080	8112	4.080	8112	4.080
8113	4.080	8113	4.080	8113	4.080	8113	4.080	8113	4.080
8114	4.080	8114	4.080	8114	4.080	8114	4.080	8114	4.080
8115	4.080	8115	4.080	8115	4.080	8115	4.080	8115	4.080
8116	4.080	8116	4.080	8116	4.080	8116	4.080	8116	4.080
8117	4.080	8117	4.080	8117	4.080	8117	4.080	8117	4.080
8118	4.080	8118	4.080	8118	4.080	8118	4.080	8118	4.080
8119	4.080	8119	4.080	8119	4.080	8119	4.080	8119	4.080
8120	4.080	8120	4.080	8120	4.080	8120	4.080	8120	4.080
8121	4.080	8121	4.080	8121	4.080	8121	4.080	8121	4.080
8122	4.080	8122	4.080	8122	4.080	8122	4.080	8122	4.080
8123	4.080	8123	4.080	8123	4.080	8123	4.080	8123	4.080
8124	4.080	8124	4.080	8124	4.080	8124	4.080	8124	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 31			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
8125	4.080	8175	4.080	8225	4.080	8275	4.080	8325	4.080
8126	4.080	8176	4.080	8226	4.080	8276	4.080	8326	4.080
8127	4.080	8177	4.080	8227	4.080	8277	4.080	8327	4.080
8128	4.080	8178	4.080	8228	4.080	8278	4.080	8328	4.080
8129	4.080	8179	4.080	8229	4.080	8279	4.080	8329	4.080
8130	4.080	8180	4.080	8230	4.080	8280	4.080	8330	4.080
8131	4.080	8181	4.080	8231	4.080	8281	4.080	8331	4.080
8132	4.080	8182	4.080	8232	4.080	8282	4.080	8332	4.080
8133	4.080	8183	4.080	8233	4.080	8283	4.080	8333	4.080
8134	4.080	8184	4.080	8234	4.080	8284	4.080	8334	4.080
8135	4.080	8185	4.080	8235	4.080	8285	4.080	8335	4.080
8136	4.080	8186	4.080	8236	4.080	8286	4.080	8336	4.080
8137	4.080	8187	4.080	8237	4.080	8287	4.080	8337	4.080
8138	4.080	8188	4.080	8238	4.080	8288	4.080	8338	4.080
8139	4.080	8189	4.080	8239	4.080	8289	4.080	8339	4.080
8140	4.080	8190	4.080	8240	4.080	8290	4.080	8340	4.080
8141	4.080	8191	4.080	8241	4.080	8291	4.080	8341	4.080
8142	4.080	8192	4.080	8242	4.080	8292	4.080	8342	4.080
8143	4.080	8193	4.080	8243	4.080	8293	4.080	8343	4.080
8144	4.080	8194	4.080	8244	4.080	8294	4.080	8344	4.080
8145	4.080	8195	4.080	8245	4.080	8295	4.080	8345	4.080
8146	4.080	8196	4.080	8246	4.080	8296	4.080	8346	4.080
8147	4.080	8197	4.080	8247	4.080	8297	4.080	8347	4.080
8148	4.080	8198	4.080	8248	4.080	8298	4.080	8348	4.080
8149	4.080	8199	4.080	8249	4.080	8299	4.080	8349	4.080
8150	4.080	8200	4.080	8250	4.080	8300	4.080	8350	4.080
8151	4.080	8201	4.080	8251	4.080	8301	4.080	8351	4.080
8152	4.080	8202	4.080	8252	4.080	8302	4.080	8352	4.080
8153	4.080	8203	4.080	8253	4.080	8303	4.080	8353	4.080
8154	4.080	8204	4.080	8254	4.080	8304	4.080	8354	4.080
8155	4.080	8205	4.080	8255	4.080	8305	4.080	8355	4.080
8156	4.080	8206	4.080	8256	4.080	8306	4.080	8356	4.080
8157	4.080	8207	4.080	8257	4.080	8307	4.080	8357	4.080
8158	4.080	8208	4.080	8258	4.080	8308	4.080	8358	4.080
8159	4.080	8209	4.080	8259	4.080	8309	4.080	8359	4.080
8160	4.080	8210	4.080	8260	4.080	8310	4.080	8360	4.080
8161	4.080	8211	4.080	8261	4.080	8311	4.080	8361	4.080
8162	4.080	8212	4.080	8262	4.080	8312	4.080	8362	4.080
8163	4.080	8213	4.080	8263	4.080	8313	4.080	8363	4.080
8164	4.080	8214	4.080	8264	4.080	8314	4.080	8364	4.080
8165	4.080	8215	4.080	8265	4.080	8315	4.080	8365	4.080
8166	4.080	8216	4.080	8266	4.080	8316	4.080	8366	4.080
8167	4.080	8217	4.080	8267	4.080	8317	4.080	8367	4.080
8168	4.080	8218	4.080	8268	4.080	8318	4.080	8368	4.080
8169	4.080	8219	4.080	8269	4.080	8319	4.080	8369	4.080
8170	4.080	8220	4.080	8270	4.080	8320	4.080	8370	4.080
8171	4.080	8221	4.080	8271	4.080	8321	4.080	8371	4.080
8172	4.080	8222	4.080	8272	4.080	8322	4.080	8372	4.080
8173	4.080	8223	4.080	8273	4.080	8323	4.080	8373	4.080
8174	4.080	8224	4.080	8274	4.080	8324	4.080	8374	4.080
								8375	4.080
								8376	4.080
								8377	4.080
								8378	4.080
								8379	4.080
								8380	4.080
								8381	4.080
								8382	4.080
								8383	4.080
								8384	4.080
								8385	4.080
								8386	4.080
								8387	4.080
								8388	4.080
								8389	4.080
								8390	4.080
								8391	4.080
								8392	4.080
								8393	4.080
								8394	4.080
								8395	4.080
								8396	4.080
								8397	4.080
								8398	4.080
								8399	4.080
								8400	4.080
								8401	4.080
								8402	4.080
								8403	4.080
								8404	4.080
								8405	4.080
								8406	4.080
								8407	4.080
								8408	4.080
								8409	4.080
								8410	4.080
								8411	4.080
								8412	4.080
								8413	4.080
								8414	4.080
								8415	4.080
								8416	4.080
								8417	4.080
								8418	4.080
								8419	4.080
								8420	4.080
								8421	4.080
								8422	4.080
								8423	4.080
								8424	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 32			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
8425	4.080	8475	4.080	8525	4.080	8575	4.080	8625	4.080	8675	4.080
8426	4.080	8476	4.080	8526	4.080	8576	4.080	8626	4.080	8676	4.080
8427	4.080	8477	4.080	8527	4.080	8577	4.080	8627	4.080	8677	4.080
8428	4.080	8478	4.080	8528	4.080	8578	4.080	8628	4.080	8678	4.080
8429	4.080	8479	4.080	8529	4.080	8579	4.080	8629	4.080	8679	4.080
8430	4.080	8480	4.080	8530	4.080	8580	4.080	8630	4.080	8680	4.080
8431	4.080	8481	4.080	8531	4.080	8581	4.080	8631	4.080	8681	4.080
8432	4.080	8482	4.080	8532	4.080	8582	4.080	8632	4.080	8682	4.080
8433	4.080	8483	4.080	8533	4.080	8583	4.080	8633	4.080	8683	4.080
8434	4.080	8484	4.080	8534	4.080	8584	4.080	8634	4.080	8684	4.080
8435	4.080	8485	4.080	8535	4.080	8585	4.080	8635	4.080	8685	4.080
8436	4.080	8486	4.080	8536	4.080	8586	4.080	8636	4.080	8686	4.080
8437	4.080	8487	4.080	8537	4.080	8587	4.080	8637	4.080	8687	4.080
8438	4.080	8488	4.080	8538	4.080	8588	4.080	8638	4.080	8688	4.080
8439	4.080	8489	4.080	8539	4.080	8589	4.080	8639	4.080	8689	4.080
8440	4.080	8490	4.080	8540	4.080	8590	4.080	8640	4.080	8690	4.080
8441	4.080	8491	4.080	8541	4.080	8591	4.080	8641	4.080	8691	4.080
8442	4.080	8492	4.080	8542	4.080	8592	4.080	8642	4.080	8692	4.080
8443	4.080	8493	4.080	8543	4.080	8593	4.080	8643	4.080	8693	4.080
8444	4.080	8494	4.080	8544	4.080	8594	4.080	8644	4.080	8694	4.080
8445	4.080	8495	4.080	8545	4.080	8595	4.080	8645	4.080	8695	4.080
8446	4.080	8496	4.080	8546	4.080	8596	4.080	8646	4.080	8696	4.080
8447	4.080	8497	4.080	8547	4.080	8597	4.080	8647	4.080	8697	4.080
8448	4.080	8498	4.080	8548	4.080	8598	4.080	8648	4.080	8698	4.080
8449	4.080	8499	4.080	8549	4.080	8599	4.080	8649	4.080	8699	4.080
8450	4.080	8500	4.080	8550	4.080	8600	4.080	8650	4.080	8700	4.080
8451	4.080	8501	4.080	8551	4.080	8601	4.080	8651	4.080	8701	4.080
8452	4.080	8502	4.080	8552	4.080	8602	4.080	8652	4.080	8702	4.080
8453	4.080	8503	4.080	8553	4.080	8603	4.080	8653	4.080	8703	4.080
8454	4.080	8504	4.080	8554	4.080	8604	4.080	8654	4.080	8704	4.080
8455	4.080	8505	4.080	8555	4.080	8605	4.080	8655	4.080	8705	4.080
8456	4.080	8506	4.080	8556	4.080	8606	4.080	8656	4.080	8706	4.080
8457	4.080	8507	4.080	8557	4.080	8607	4.080	8657	4.080	8707	4.080
8458	4.080	8508	4.080	8558	4.080	8608	4.080	8658	4.080	8708	4.080
8459	4.080	8509	4.080	8559	4.080	8609	4.080	8659	4.080	8709	4.080
8460	4.080	8510	4.080	8560	4.080	8610	4.080	8660	4.080	8710	4.080
8461	4.080	8511	4.080	8561	4.080	8611	4.080	8661	4.080	8711	4.080
8462	4.080	8512	4.080	8562	4.080	8612	4.080	8662	4.080	8712	4.080
8463	4.080	8513	4.080	8563	4.080	8613	4.080	8663	4.080	8713	4.080
8464	4.080	8514	4.080	8564	4.080	8614	4.080	8664	4.080	8714	4.080
8465	4.080	8515	4.080	8565	4.080	8615	4.080	8665	4.080	8715	4.080
8466	4.080	8516	4.080	8566	4.080	8616	4.080	8666	4.080	8716	4.080
8467	4.080	8517	4.080	8567	4.080	8617	4.080	8667	4.080	8717	4.080
8468	4.080	8518	4.080	8568	4.080	8618	4.080	8668	4.080	8718	4.080
8469	4.080	8519	4.080	8569	4.080	8619	4.080	8669	4.080	8719	4.080
8470	4.080	8520	4.080	8570	4.080	8620	4.080	8670	4.080	8720	4.080
8471	4.080	8521	4.080	8571	4.080	8621	4.080	8671	4.080	8721	4.080
8472	4.080	8522	4.080	8572	4.080	8622	4.080	8672	4.080	8722	4.080
8473	4.080	8523	4.080	8573	4.080	8623	4.080	8673	4.080	8723	4.080
8474	4.080	8524	4.080	8574	4.080	8624	4.080	8674	4.080	8724	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership								Page 33			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham							
Date 25/06/2019 15:38				Designed by Terry Seymour							
File SW1-with Crayfern site.MDX				Checked by Terry Seymour							
Innovyze				Network 2017.1.2							
<u>Surcharged Outfall Details for SW-1.SWS</u>											
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
8725	4.080	8775	4.080	8825	4.080	8875	4.080	8925	4.080	8975	4.080
8726	4.080	8776	4.080	8826	4.080	8876	4.080	8926	4.080	8976	4.080
8727	4.080	8777	4.080	8827	4.080	8877	4.080	8927	4.080	8977	4.080
8728	4.080	8778	4.080	8828	4.080	8878	4.080	8928	4.080	8978	4.080
8729	4.080	8779	4.080	8829	4.080	8879	4.080	8929	4.080	8979	4.080
8730	4.080	8780	4.080	8830	4.080	8880	4.080	8930	4.080	8980	4.080
8731	4.080	8781	4.080	8831	4.080	8881	4.080	8931	4.080	8981	4.080
8732	4.080	8782	4.080	8832	4.080	8882	4.080	8932	4.080	8982	4.080
8733	4.080	8783	4.080	8833	4.080	8883	4.080	8933	4.080	8983	4.080
8734	4.080	8784	4.080	8834	4.080	8884	4.080	8934	4.080	8984	4.080
8735	4.080	8785	4.080	8835	4.080	8885	4.080	8935	4.080	8985	4.080
8736	4.080	8786	4.080	8836	4.080	8886	4.080	8936	4.080	8986	4.080
8737	4.080	8787	4.080	8837	4.080	8887	4.080	8937	4.080	8987	4.080
8738	4.080	8788	4.080	8838	4.080	8888	4.080	8938	4.080	8988	4.080
8739	4.080	8789	4.080	8839	4.080	8889	4.080	8939	4.080	8989	4.080
8740	4.080	8790	4.080	8840	4.080	8890	4.080	8940	4.080	8990	4.080
8741	4.080	8791	4.080	8841	4.080	8891	4.080	8941	4.080	8991	4.080
8742	4.080	8792	4.080	8842	4.080	8892	4.080	8942	4.080	8992	4.080
8743	4.080	8793	4.080	8843	4.080	8893	4.080	8943	4.080	8993	4.080
8744	4.080	8794	4.080	8844	4.080	8894	4.080	8944	4.080	8994	4.080
8745	4.080	8795	4.080	8845	4.080	8895	4.080	8945	4.080	8995	4.080
8746	4.080	8796	4.080	8846	4.080	8896	4.080	8946	4.080	8996	4.080
8747	4.080	8797	4.080	8847	4.080	8897	4.080	8947	4.080	8997	4.080
8748	4.080	8798	4.080	8848	4.080	8898	4.080	8948	4.080	8998	4.080
8749	4.080	8799	4.080	8849	4.080	8899	4.080	8949	4.080	8999	4.080
8750	4.080	8800	4.080	8850	4.080	8900	4.080	8950	4.080	9000	4.080
8751	4.080	8801	4.080	8851	4.080	8901	4.080	8951	4.080	9001	4.080
8752	4.080	8802	4.080	8852	4.080	8902	4.080	8952	4.080	9002	4.080
8753	4.080	8803	4.080	8853	4.080	8903	4.080	8953	4.080	9003	4.080
8754	4.080	8804	4.080	8854	4.080	8904	4.080	8954	4.080	9004	4.080
8755	4.080	8805	4.080	8855	4.080	8905	4.080	8955	4.080	9005	4.080
8756	4.080	8806	4.080	8856	4.080	8906	4.080	8956	4.080	9006	4.080
8757	4.080	8807	4.080	8857	4.080	8907	4.080	8957	4.080	9007	4.080
8758	4.080	8808	4.080	8858	4.080	8908	4.080	8958	4.080	9008	4.080
8759	4.080	8809	4.080	8859	4.080	8909	4.080	8959	4.080	9009	4.080
8760	4.080	8810	4.080	8860	4.080	8910	4.080	8960	4.080	9010	4.080
8761	4.080	8811	4.080	8861	4.080	8911	4.080	8961	4.080	9011	4.080
8762	4.080	8812	4.080	8862	4.080	8912	4.080	8962	4.080	9012	4.080
8763	4.080	8813	4.080	8863	4.080	8913	4.080	8963	4.080	9013	4.080
8764	4.080	8814	4.080	8864	4.080	8914	4.080	8964	4.080	9014	4.080
8765	4.080	8815	4.080	8865	4.080	8915	4.080	8965	4.080	9015	4.080
8766	4.080	8816	4.080	8866	4.080	8916	4.080	8966	4.080	9016	4.080
8767	4.080	8817	4.080	8867	4.080	8917	4.080	8967	4.080	9017	4.080
8768	4.080	8818	4.080	8868	4.080	8918	4.080	8968	4.080	9018	4.080
8769	4.080	8819	4.080	8869	4.080	8919	4.080	8969	4.080	9019	4.080
8770	4.080	8820	4.080	8870	4.080	8920	4.080	8970	4.080	9020	4.080
8771	4.080	8821	4.080	8871	4.080	8921	4.080	8971	4.080	9021	4.080
8772	4.080	8822	4.080	8872	4.080	8922	4.080	8972	4.080	9022	4.080
8773	4.080	8823	4.080	8873	4.080	8923	4.080	8973	4.080	9023	4.080
8774	4.080	8824	4.080	8874	4.080	8924	4.080	8974	4.080	9024	4.080
©1982-2017 XP Solutions											

Rogers Cory Partnership						Page 34			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
Surcharged Outfall Details for SW-1.SWS									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
9025	4.080	9075	4.080	9125	4.080	9175	4.080	9225	4.080
9026	4.080	9076	4.080	9126	4.080	9176	4.080	9226	4.080
9027	4.080	9077	4.080	9127	4.080	9177	4.080	9227	4.080
9028	4.080	9078	4.080	9128	4.080	9178	4.080	9228	4.080
9029	4.080	9079	4.080	9129	4.080	9179	4.080	9229	4.080
9030	4.080	9080	4.080	9130	4.080	9180	4.080	9230	4.080
9031	4.080	9081	4.080	9131	4.080	9181	4.080	9231	4.080
9032	4.080	9082	4.080	9132	4.080	9182	4.080	9232	4.080
9033	4.080	9083	4.080	9133	4.080	9183	4.080	9233	4.080
9034	4.080	9084	4.080	9134	4.080	9184	4.080	9234	4.080
9035	4.080	9085	4.080	9135	4.080	9185	4.080	9235	4.080
9036	4.080	9086	4.080	9136	4.080	9186	4.080	9236	4.080
9037	4.080	9087	4.080	9137	4.080	9187	4.080	9237	4.080
9038	4.080	9088	4.080	9138	4.080	9188	4.080	9238	4.080
9039	4.080	9089	4.080	9139	4.080	9189	4.080	9239	4.080
9040	4.080	9090	4.080	9140	4.080	9190	4.080	9240	4.080
9041	4.080	9091	4.080	9141	4.080	9191	4.080	9241	4.080
9042	4.080	9092	4.080	9142	4.080	9192	4.080	9242	4.080
9043	4.080	9093	4.080	9143	4.080	9193	4.080	9243	4.080
9044	4.080	9094	4.080	9144	4.080	9194	4.080	9244	4.080
9045	4.080	9095	4.080	9145	4.080	9195	4.080	9245	4.080
9046	4.080	9096	4.080	9146	4.080	9196	4.080	9246	4.080
9047	4.080	9097	4.080	9147	4.080	9197	4.080	9247	4.080
9048	4.080	9098	4.080	9148	4.080	9198	4.080	9248	4.080
9049	4.080	9099	4.080	9149	4.080	9199	4.080	9249	4.080
9050	4.080	9100	4.080	9150	4.080	9200	4.080	9250	4.080
9051	4.080	9101	4.080	9151	4.080	9201	4.080	9251	4.080
9052	4.080	9102	4.080	9152	4.080	9202	4.080	9252	4.080
9053	4.080	9103	4.080	9153	4.080	9203	4.080	9253	4.080
9054	4.080	9104	4.080	9154	4.080	9204	4.080	9254	4.080
9055	4.080	9105	4.080	9155	4.080	9205	4.080	9255	4.080
9056	4.080	9106	4.080	9156	4.080	9206	4.080	9256	4.080
9057	4.080	9107	4.080	9157	4.080	9207	4.080	9257	4.080
9058	4.080	9108	4.080	9158	4.080	9208	4.080	9258	4.080
9059	4.080	9109	4.080	9159	4.080	9209	4.080	9259	4.080
9060	4.080	9110	4.080	9160	4.080	9210	4.080	9260	4.080
9061	4.080	9111	4.080	9161	4.080	9211	4.080	9261	4.080
9062	4.080	9112	4.080	9162	4.080	9212	4.080	9262	4.080
9063	4.080	9113	4.080	9163	4.080	9213	4.080	9263	4.080
9064	4.080	9114	4.080	9164	4.080	9214	4.080	9264	4.080
9065	4.080	9115	4.080	9165	4.080	9215	4.080	9265	4.080
9066	4.080	9116	4.080	9166	4.080	9216	4.080	9266	4.080
9067	4.080	9117	4.080	9167	4.080	9217	4.080	9267	4.080
9068	4.080	9118	4.080	9168	4.080	9218	4.080	9268	4.080
9069	4.080	9119	4.080	9169	4.080	9219	4.080	9269	4.080
9070	4.080	9120	4.080	9170	4.080	9220	4.080	9270	4.080
9071	4.080	9121	4.080	9171	4.080	9221	4.080	9271	4.080
9072	4.080	9122	4.080	9172	4.080	9222	4.080	9272	4.080
9073	4.080	9123	4.080	9173	4.080	9223	4.080	9273	4.080
9074	4.080	9124	4.080	9174	4.080	9224	4.080	9274	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 35			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
9325	4.080	9375	4.080	9425	4.080	9475	4.080	9525	4.080
9326	4.080	9376	4.080	9426	4.080	9476	4.080	9526	4.080
9327	4.080	9377	4.080	9427	4.080	9477	4.080	9527	4.080
9328	4.080	9378	4.080	9428	4.080	9478	4.080	9528	4.080
9329	4.080	9379	4.080	9429	4.080	9479	4.080	9529	4.080
9330	4.080	9380	4.080	9430	4.080	9480	4.080	9530	4.080
9331	4.080	9381	4.080	9431	4.080	9481	4.080	9531	4.080
9332	4.080	9382	4.080	9432	4.080	9482	4.080	9532	4.080
9333	4.080	9383	4.080	9433	4.080	9483	4.080	9533	4.080
9334	4.080	9384	4.080	9434	4.080	9484	4.080	9534	4.080
9335	4.080	9385	4.080	9435	4.080	9485	4.080	9535	4.080
9336	4.080	9386	4.080	9436	4.080	9486	4.080	9536	4.080
9337	4.080	9387	4.080	9437	4.080	9487	4.080	9537	4.080
9338	4.080	9388	4.080	9438	4.080	9488	4.080	9538	4.080
9339	4.080	9389	4.080	9439	4.080	9489	4.080	9539	4.080
9340	4.080	9390	4.080	9440	4.080	9490	4.080	9540	4.080
9341	4.080	9391	4.080	9441	4.080	9491	4.080	9541	4.080
9342	4.080	9392	4.080	9442	4.080	9492	4.080	9542	4.080
9343	4.080	9393	4.080	9443	4.080	9493	4.080	9543	4.080
9344	4.080	9394	4.080	9444	4.080	9494	4.080	9544	4.080
9345	4.080	9395	4.080	9445	4.080	9495	4.080	9545	4.080
9346	4.080	9396	4.080	9446	4.080	9496	4.080	9546	4.080
9347	4.080	9397	4.080	9447	4.080	9497	4.080	9547	4.080
9348	4.080	9398	4.080	9448	4.080	9498	4.080	9548	4.080
9349	4.080	9399	4.080	9449	4.080	9499	4.080	9549	4.080
9350	4.080	9400	4.080	9450	4.080	9500	4.080	9550	4.080
9351	4.080	9401	4.080	9451	4.080	9501	4.080	9551	4.080
9352	4.080	9402	4.080	9452	4.080	9502	4.080	9552	4.080
9353	4.080	9403	4.080	9453	4.080	9503	4.080	9553	4.080
9354	4.080	9404	4.080	9454	4.080	9504	4.080	9554	4.080
9355	4.080	9405	4.080	9455	4.080	9505	4.080	9555	4.080
9356	4.080	9406	4.080	9456	4.080	9506	4.080	9556	4.080
9357	4.080	9407	4.080	9457	4.080	9507	4.080	9557	4.080
9358	4.080	9408	4.080	9458	4.080	9508	4.080	9558	4.080
9359	4.080	9409	4.080	9459	4.080	9509	4.080	9559	4.080
9360	4.080	9410	4.080	9460	4.080	9510	4.080	9560	4.080
9361	4.080	9411	4.080	9461	4.080	9511	4.080	9561	4.080
9362	4.080	9412	4.080	9462	4.080	9512	4.080	9562	4.080
9363	4.080	9413	4.080	9463	4.080	9513	4.080	9563	4.080
9364	4.080	9414	4.080	9464	4.080	9514	4.080	9564	4.080
9365	4.080	9415	4.080	9465	4.080	9515	4.080	9565	4.080
9366	4.080	9416	4.080	9466	4.080	9516	4.080	9566	4.080
9367	4.080	9417	4.080	9467	4.080	9517	4.080	9567	4.080
9368	4.080	9418	4.080	9468	4.080	9518	4.080	9568	4.080
9369	4.080	9419	4.080	9469	4.080	9519	4.080	9569	4.080
9370	4.080	9420	4.080	9470	4.080	9520	4.080	9570	4.080
9371	4.080	9421	4.080	9471	4.080	9521	4.080	9571	4.080
9372	4.080	9422	4.080	9472	4.080	9522	4.080	9572	4.080
9373	4.080	9423	4.080	9473	4.080	9523	4.080	9573	4.080
9374	4.080	9424	4.080	9474	4.080	9524	4.080	9574	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 36			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>Surcharged Outfall Details for SW-1.SWS</u>									
Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
9625	4.080	9675	4.080	9725	4.080	9775	4.080	9825	4.080
9626	4.080	9676	4.080	9726	4.080	9776	4.080	9826	4.080
9627	4.080	9677	4.080	9727	4.080	9777	4.080	9827	4.080
9628	4.080	9678	4.080	9728	4.080	9778	4.080	9828	4.080
9629	4.080	9679	4.080	9729	4.080	9779	4.080	9829	4.080
9630	4.080	9680	4.080	9730	4.080	9780	4.080	9830	4.080
9631	4.080	9681	4.080	9731	4.080	9781	4.080	9831	4.080
9632	4.080	9682	4.080	9732	4.080	9782	4.080	9832	4.080
9633	4.080	9683	4.080	9733	4.080	9783	4.080	9833	4.080
9634	4.080	9684	4.080	9734	4.080	9784	4.080	9834	4.080
9635	4.080	9685	4.080	9735	4.080	9785	4.080	9835	4.080
9636	4.080	9686	4.080	9736	4.080	9786	4.080	9836	4.080
9637	4.080	9687	4.080	9737	4.080	9787	4.080	9837	4.080
9638	4.080	9688	4.080	9738	4.080	9788	4.080	9838	4.080
9639	4.080	9689	4.080	9739	4.080	9789	4.080	9839	4.080
9640	4.080	9690	4.080	9740	4.080	9790	4.080	9840	4.080
9641	4.080	9691	4.080	9741	4.080	9791	4.080	9841	4.080
9642	4.080	9692	4.080	9742	4.080	9792	4.080	9842	4.080
9643	4.080	9693	4.080	9743	4.080	9793	4.080	9843	4.080
9644	4.080	9694	4.080	9744	4.080	9794	4.080	9844	4.080
9645	4.080	9695	4.080	9745	4.080	9795	4.080	9845	4.080
9646	4.080	9696	4.080	9746	4.080	9796	4.080	9846	4.080
9647	4.080	9697	4.080	9747	4.080	9797	4.080	9847	4.080
9648	4.080	9698	4.080	9748	4.080	9798	4.080	9848	4.080
9649	4.080	9699	4.080	9749	4.080	9799	4.080	9849	4.080
9650	4.080	9700	4.080	9750	4.080	9800	4.080	9850	4.080
9651	4.080	9701	4.080	9751	4.080	9801	4.080	9851	4.080
9652	4.080	9702	4.080	9752	4.080	9802	4.080	9852	4.080
9653	4.080	9703	4.080	9753	4.080	9803	4.080	9853	4.080
9654	4.080	9704	4.080	9754	4.080	9804	4.080	9854	4.080
9655	4.080	9705	4.080	9755	4.080	9805	4.080	9855	4.080
9656	4.080	9706	4.080	9756	4.080	9806	4.080	9856	4.080
9657	4.080	9707	4.080	9757	4.080	9807	4.080	9857	4.080
9658	4.080	9708	4.080	9758	4.080	9808	4.080	9858	4.080
9659	4.080	9709	4.080	9759	4.080	9809	4.080	9859	4.080
9660	4.080	9710	4.080	9760	4.080	9810	4.080	9860	4.080
9661	4.080	9711	4.080	9761	4.080	9811	4.080	9861	4.080
9662	4.080	9712	4.080	9762	4.080	9812	4.080	9862	4.080
9663	4.080	9713	4.080	9763	4.080	9813	4.080	9863	4.080
9664	4.080	9714	4.080	9764	4.080	9814	4.080	9864	4.080
9665	4.080	9715	4.080	9765	4.080	9815	4.080	9865	4.080
9666	4.080	9716	4.080	9766	4.080	9816	4.080	9866	4.080
9667	4.080	9717	4.080	9767	4.080	9817	4.080	9867	4.080
9668	4.080	9718	4.080	9768	4.080	9818	4.080	9868	4.080
9669	4.080	9719	4.080	9769	4.080	9819	4.080	9869	4.080
9670	4.080	9720	4.080	9770	4.080	9820	4.080	9870	4.080
9671	4.080	9721	4.080	9771	4.080	9821	4.080	9871	4.080
9672	4.080	9722	4.080	9772	4.080	9822	4.080	9872	4.080
9673	4.080	9723	4.080	9773	4.080	9823	4.080	9873	4.080
9674	4.080	9724	4.080	9774	4.080	9824	4.080	9874	4.080
©1982-2017 XP Solutions									

Rogers Cory Partnership		Page 37
The Old School Old School Road Hook Hampshire RG27 9NJ		Summer Lane Pagham
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX		
Designed by Terry Seymour Checked by Terry Seymour		
Innovyze		Network 2017.1.2

Surcharged Outfall Details for SW-1.SWS

Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)	Time (mins)	Depth (m)
9925	4.080	9951	4.080	9977	4.080	10003	4.080	10029	4.080	10055	4.080
9926	4.080	9952	4.080	9978	4.080	10004	4.080	10030	4.080	10056	4.080
9927	4.080	9953	4.080	9979	4.080	10005	4.080	10031	4.080	10057	4.080
9928	4.080	9954	4.080	9980	4.080	10006	4.080	10032	4.080	10058	4.080
9929	4.080	9955	4.080	9981	4.080	10007	4.080	10033	4.080	10059	4.080
9930	4.080	9956	4.080	9982	4.080	10008	4.080	10034	4.080	10060	4.080
9931	4.080	9957	4.080	9983	4.080	10009	4.080	10035	4.080	10061	4.080
9932	4.080	9958	4.080	9984	4.080	10010	4.080	10036	4.080	10062	4.080
9933	4.080	9959	4.080	9985	4.080	10011	4.080	10037	4.080	10063	4.080
9934	4.080	9960	4.080	9986	4.080	10012	4.080	10038	4.080	10064	4.080
9935	4.080	9961	4.080	9987	4.080	10013	4.080	10039	4.080	10065	4.080
9936	4.080	9962	4.080	9988	4.080	10014	4.080	10040	4.080	10066	4.080
9937	4.080	9963	4.080	9989	4.080	10015	4.080	10041	4.080	10067	4.080
9938	4.080	9964	4.080	9990	4.080	10016	4.080	10042	4.080	10068	4.080
9939	4.080	9965	4.080	9991	4.080	10017	4.080	10043	4.080	10069	4.080
9940	4.080	9966	4.080	9992	4.080	10018	4.080	10044	4.080	10070	4.080
9941	4.080	9967	4.080	9993	4.080	10019	4.080	10045	4.080	10071	4.080
9942	4.080	9968	4.080	9994	4.080	10020	4.080	10046	4.080	10072	4.080
9943	4.080	9969	4.080	9995	4.080	10021	4.080	10047	4.080	10073	4.080
9944	4.080	9970	4.080	9996	4.080	10022	4.080	10048	4.080	10074	4.080
9945	4.080	9971	4.080	9997	4.080	10023	4.080	10049	4.080	10075	4.080
9946	4.080	9972	4.080	9998	4.080	10024	4.080	10050	4.080	10076	4.080
9947	4.080	9973	4.080	9999	4.080	10025	4.080	10051	4.080	10077	4.080
9948	4.080	9974	4.080	10000	4.080	10026	4.080	10052	4.080	10078	4.080
9949	4.080	9975	4.080	10001	4.080	10027	4.080	10053	4.080	10079	4.080
9950	4.080	9976	4.080	10002	4.080	10028	4.080	10054	4.080	10080	4.080

Simulation Criteria for SW-1.SWS

Volumetric Runoff Coeff	0.840	Additional Flow - % of Total Flow	10.000
Areal Reduction Factor	1.000	MADD Factor * 10m³/ha Storage	2.000
Hot Start (mins)	0	Inlet Coefficient	0.800
Hot Start Level (mm)	0	Flow per Person per Day (l/per/day)	0.000
Manhole Headloss Coeff (Global)	0.500	Run Time (mins)	2880
Foul Sewage per hectare (l/s)	0.000	Output Interval (mins)	24

Number of Input Hydrographs	0	Number of Storage Structures	6
Number of Online Controls	4	Number of Time/Area Diagrams	0
Number of Offline Controls	2	Number of Real Time Controls	0

Synthetic Rainfall Details

Rainfall Model	FSR	Profile Type	Winter
Return Period (years)	100	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	19.000	Storm Duration (mins)	1440
Ratio R	0.350		

©1982-2017 XP Solutions

Rogers Cory Partnership		Page 38
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		

Online Controls for SW-1.SWS

Hydro-Brake® Optimum Manhole: SCF-02, DS/PN: S5.001, Volume (m³): 1.9

Unit Reference	MD-SHE-0132-8000-1000-8000
Design Head (m)	1.000
Design Flow (l/s)	8.0
Flush-Flo™	Calculated
Objective	Minimise upstream storage
Application	Surface
Sump Available	Yes
Diameter (mm)	132
Invert Level (m)	3.960
Minimum Outlet Pipe Diameter (mm)	150
Suggested Manhole Diameter (mm)	1200

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.000	8.0
Flush-Flo™	0.302	8.0
Kick-Flo®	0.664	6.6
Mean Flow over Head Range	-	6.9

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	4.7	1.200	8.7	3.000	13.4	7.000	20.1
0.200	7.8	1.400	9.4	3.500	14.5	7.500	20.8
0.300	8.0	1.600	10.0	4.000	15.4	8.000	21.5
0.400	7.9	1.800	10.5	4.500	16.3	8.500	22.1
0.500	7.7	2.000	11.1	5.000	17.1	9.000	22.7
0.600	7.2	2.200	11.6	5.500	17.9	9.500	23.3
0.800	7.2	2.400	12.1	6.000	18.7		
1.000	8.0	2.600	12.6	6.500	19.4		

Hydro-Brake® Optimum Manhole: SCF-04, DS/PN: S6.001, Volume (m³): 15.4

Unit Reference	MD-SHE-0101-4600-1000-4600
Design Head (m)	1.000
Design Flow (l/s)	4.6
Flush-Flo™	Calculated
Objective	Minimise upstream storage
Application	Surface
Sump Available	Yes
Diameter (mm)	101
Invert Level (m)	3.960
Minimum Outlet Pipe Diameter (mm)	150
Suggested Manhole Diameter (mm)	1200

©1982-2017 XP Solutions

Rogers Cory Partnership		Page 39
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		

Hydro-Brake® Optimum Manhole: SCF-04, DS/PN: S6.001, Volume (m³): 15.4

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.000	4.6
Flush-Flo™	0.293	4.6
Kick-Flo®	0.633	3.7
Mean Flow over Head Range	-	4.0

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	3.4	1.200	5.0	3.000	7.7	7.000	11.5
0.200	4.5	1.400	5.4	3.500	8.3	7.500	11.9
0.300	4.6	1.600	5.7	4.000	8.8	8.000	12.2
0.400	4.5	1.800	6.0	4.500	9.3	8.500	12.6
0.500	4.4	2.000	6.3	5.000	9.8	9.000	12.9
0.600	4.0	2.200	6.6	5.500	10.2	9.500	13.3
0.800	4.1	2.400	6.9	6.000	10.7		
1.000	4.6	2.600	7.2	6.500	11.1		

Hydro-Brake® Optimum Manhole: SW-10, DS/PN: S1.015, Volume (m³): 27.7

Unit Reference	MD-SHE-0192-2000-1500-2000
Design Head (m)	1.500
Design Flow (l/s)	20.0
Flush-Flo™	Calculated
Objective	Minimise upstream storage
Application	Surface
Sump Available	Yes
Diameter (mm)	192
Invert Level (m)	3.270
Minimum Outlet Pipe Diameter (mm)	225
Suggested Manhole Diameter (mm)	1500

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.500	20.0
Flush-Flo™	0.452	20.0
Kick-Flo®	0.984	16.4
Mean Flow over Head Range	-	17.3

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	6.7	0.300	19.4	0.500	20.0	0.800	18.8
0.200	17.7	0.400	19.9	0.600	19.7	1.000	16.5

©1982-2017 XP Solutions

Rogers Cory Partnership		Page 40
The Old School Old School Road Hook Hampshire RG27 9NJ		Summer Lane Pagham
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX		
Designed by Terry Seymour Checked by Terry Seymour		
Innovyze		Network 2017.1.2

Hydro-Brake® Optimum Manhole: SW-10, DS/PN: S1.015, Volume (m³): 27.7

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
1.200	18.0	2.400	25.0	5.000	35.6	8.000	44.7
1.400	19.3	2.600	26.0	5.500	37.3	8.500	46.0
1.600	20.6	3.000	27.8	6.000	38.9	9.000	47.3
1.800	21.8	3.500	30.0	6.500	40.4	9.500	48.6
2.000	22.9	4.000	32.0	7.000	41.9		
2.200	24.0	4.500	33.8	7.500	43.3		

Hydro-Brake® Optimum Manhole: SW-2, DS/PN: S1.022, Volume (m³): 8.0

Unit Reference	MD-SHE-0124-7900-1450-7900
Design Head (m)	1.450
Design Flow (l/s)	7.9
Flush-Flo™	Calculated
Objective	Minimise upstream storage
Application	Surface
Sump Available	Yes
Diameter (mm)	124
Invert Level (m)	2.803
Minimum Outlet Pipe Diameter (mm)	150
Suggested Manhole Diameter (mm)	1200

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.450	7.9
Flush-Flo™	0.425	7.9
Kick-Flo®	0.896	6.3
Mean Flow over Head Range	-	6.9

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	4.4	1.200	7.2	3.000	11.1	7.000	16.7
0.200	7.2	1.400	7.8	3.500	12.0	7.500	17.2
0.300	7.7	1.600	8.3	4.000	12.7	8.000	17.8
0.400	7.9	1.800	8.7	4.500	13.5	8.500	18.3
0.500	7.9	2.000	9.2	5.000	14.2	9.000	18.8
0.600	7.7	2.200	9.6	5.500	14.8	9.500	19.3
0.800	7.1	2.400	10.0	6.000	15.5		
1.000	6.6	2.600	10.4	6.500	16.1		

©1982-2017 XP Solutions

Rogers Cory Partnership		Page 41
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		
<u>Offline Controls for SW-1.SWS</u> <u>Weir Manhole: SW-10, DS/PN: S1.015, Loop to PN: S1.016</u> Discharge Coef 0.544 Width (m) 1.500 Invert Level (m) 4.500 <u>Weir Manhole: SW-2, DS/PN: S1.022, Loop to PN: None</u> Discharge Coef 0.544 Width (m) 10.000 Invert Level (m) 5.050		
©1982-2017 XP Solutions		

Rogers Cory Partnership		Page 42
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		

Storage Structures for SW-1.SWS

Porous Car Park Manhole: SW-25, DS/PN: S1.000

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	5.5
Membrane Percolation (mm/hr)	1000	Length (m)	51.0
Max Percolation (l/s)	77.9	Slope (1:X)	100.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	4.412	Cap Volume Depth (m)	0.600

Porous Car Park Manhole: SW-18, DS/PN: S1.007

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	10.0
Membrane Percolation (mm/hr)	1000	Length (m)	10.0
Max Percolation (l/s)	27.8	Slope (1:X)	500.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	4.333	Cap Volume Depth (m)	0.450

Tank or Pond Manhole: SCF-01, DS/PN: S5.000

Invert Level (m) 4.000

Depth (m)	Area (m ²)	Depth (m)	Area (m ²)	Depth (m)	Area (m ²)
0.000	168.0	0.400	168.0	0.401	0.0

Tank or Pond Manhole: SCF-03, DS/PN: S6.000

Invert Level (m) 4.000

Depth (m)	Area (m ²)	Depth (m)	Area (m ²)	Depth (m)	Area (m ²)
0.000	294.0	0.400	294.0	0.401	0.0

Tank or Pond Manhole: SW-12, DS/PN: S1.013

Invert Level (m) 4.200

Depth (m)	Area (m ²)	Depth (m)	Area (m ²)
0.000	153.3	1.000	353.2

Tank or Pond Manhole: SW-31, DS/PN: S7.008

Invert Level (m) 4.200

Depth (m)	Area (m ²)	Depth (m)	Area (m ²)
0.000	130.1	0.700	311.4

©1982-2017 XP Solutions

Rogers Cory Partnership		Page 43																																																																																																																																																																																																																																
The Old School Old School Road Hook Hampshire RG27 9NJ		Summer Lane Pagham																																																																																																																																																																																																																																
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX		Designed by Terry Seymour Checked by Terry Seymour																																																																																																																																																																																																																																
Innovyze		Network 2017.1.2																																																																																																																																																																																																																																
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>																																																																																																																																																																																																																																		
<u>Simulation Criteria</u> <table> <tr> <td>Areal Reduction Factor</td> <td>1.000</td> <td>Additional Flow - % of Total Flow</td> <td>10.000</td> </tr> <tr> <td>Hot Start (mins)</td> <td>0</td> <td>MADD Factor * 10m³/ha Storage</td> <td>2.000</td> </tr> <tr> <td>Hot Start Level (mm)</td> <td>0</td> <td>Inlet Coefficient</td> <td>0.800</td> </tr> <tr> <td>Manhole Headloss Coeff (Global)</td> <td>0.500</td> <td>Flow per Person per Day (l/per/day)</td> <td>0.000</td> </tr> <tr> <td>Foul Sewage per hectare (l/s)</td> <td>0.000</td> <td></td> <td></td> </tr> </table> <table> <tr> <td>Number of Input Hydrographs</td> <td>0</td> <td>Number of Storage Structures</td> <td>6</td> </tr> <tr> <td>Number of Online Controls</td> <td>4</td> <td>Number of Time/Area Diagrams</td> <td>0</td> </tr> <tr> <td>Number of Offline Controls</td> <td>2</td> <td>Number of Real Time Controls</td> <td>0</td> </tr> </table> <u>Synthetic Rainfall Details</u> <table> <tr> <td>Rainfall Model</td> <td>FSR</td> <td>Ratio R</td> <td>0.350</td> </tr> <tr> <td>Region England and Wales Cv (Summer)</td> <td></td> <td></td> <td>0.750</td> </tr> <tr> <td>M5-60 (mm)</td> <td>19.000</td> <td>Cv (Winter)</td> <td>0.840</td> </tr> </table> <table> <tr> <td>Margin for Flood Risk Warning (mm)</td> <td>300.0</td> </tr> <tr> <td>Analysis Timestep</td> <td>2.5 Second Increment (Extended)</td> </tr> <tr> <td>DTS Status</td> <td>OFF</td> </tr> <tr> <td>DVD Status</td> <td>ON</td> </tr> <tr> <td>Inertia Status</td> <td>ON</td> </tr> </table> <table> <tr> <td>Profile(s)</td> <td>Summer and Winter</td> </tr> <tr> <td>Duration(s) (mins)</td> <td>15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080</td> </tr> <tr> <td>Return Period(s) (years)</td> <td>1, 30, 100</td> </tr> <tr> <td>Climate Change (%)</td> <td>0, 0, 40</td> </tr> </table> <table> <thead> <tr> <th>PN</th> <th>US/MH Name</th> <th>Storm</th> <th>Return Period</th> <th>Climate Change</th> <th>First (X) Surchage</th> <th>First (Y) Flood</th> <th>First (Z) Overflow</th> <th>Overflow Act.</th> </tr> </thead> <tbody> <tr><td>S1.000</td><td>SW-25</td><td>15 Winter</td><td>1</td><td>+0%</td><td>100/15 Summer</td><td></td><td></td><td></td></tr> <tr><td>S2.000</td><td>SW-26</td><td>15 Winter</td><td>1</td><td>+0%</td><td>100/15 Summer</td><td></td><td></td><td></td></tr> <tr><td>S1.001</td><td>SW-24</td><td>15 Winter</td><td>1</td><td>+0%</td><td>100/15 Summer</td><td></td><td></td><td></td></tr> <tr><td>S1.002</td><td>SW-23</td><td>15 Winter</td><td>1</td><td>+0%</td><td>30/15 Winter</td><td></td><td></td><td></td></tr> <tr><td>S3.000</td><td>SW-27</td><td>15 Winter</td><td>1</td><td>+0%</td><td>100/15 Summer</td><td></td><td></td><td></td></tr> <tr><td>S4.000</td><td>SW-28</td><td>15 Winter</td><td>1</td><td>+0%</td><td>30/15 Winter</td><td></td><td></td><td></td></tr> <tr><td>S1.003</td><td>SW-22</td><td>5760 Winter</td><td>1</td><td>+0%</td><td>30/15 Summer</td><td></td><td></td><td></td></tr> <tr><td>S1.004</td><td>SW-21</td><td>5760 Winter</td><td>1</td><td>+0%</td><td>1/720 Winter</td><td></td><td></td><td></td></tr> <tr><td>S1.005</td><td>SW-20</td><td>5760 Winter</td><td>1</td><td>+0%</td><td>1/600 Winter</td><td></td><td></td><td></td></tr> <tr><td>S1.006</td><td>SW-19</td><td>5760 Winter</td><td>1</td><td>+0%</td><td>1/480 Winter</td><td></td><td></td><td></td></tr> <tr><td>S1.007</td><td>SW-18</td><td>5760 Winter</td><td>1</td><td>+0%</td><td>1/240 Winter</td><td></td><td></td><td></td></tr> <tr><td>S1.008</td><td>SW-17</td><td>5760 Winter</td><td>1</td><td>+0%</td><td>1/120 Winter</td><td></td><td></td><td></td></tr> <tr><td>S1.009</td><td>SW-16</td><td>5760 Winter</td><td>1</td><td>+0%</td><td>1/120 Winter</td><td></td><td></td><td></td></tr> <tr><td>S5.000</td><td>SCF-01</td><td>4320 Winter</td><td>1</td><td>+0%</td><td>30/60 Summer</td><td>100/30 Summer</td><td></td><td></td></tr> <tr><td>S5.001</td><td>SCF-02</td><td>4320 Winter</td><td>1</td><td>+0%</td><td>1/2160 Winter</td><td>100/30 Summer</td><td></td><td></td></tr> <tr><td>S1.010</td><td>SW-15</td><td>5760 Winter</td><td>1</td><td>+0%</td><td></td><td></td><td></td><td></td></tr> <tr><td>S6.000</td><td>SCF-03</td><td>5760 Winter</td><td>1</td><td>+0%</td><td>100/720 Winter</td><td>100/720 Winter</td><td></td><td></td></tr> </tbody> </table>			Areal Reduction Factor	1.000	Additional Flow - % of Total Flow	10.000	Hot Start (mins)	0	MADD Factor * 10m³/ha Storage	2.000	Hot Start Level (mm)	0	Inlet Coefficient	0.800	Manhole Headloss Coeff (Global)	0.500	Flow per Person per Day (l/per/day)	0.000	Foul Sewage per hectare (l/s)	0.000			Number of Input Hydrographs	0	Number of Storage Structures	6	Number of Online Controls	4	Number of Time/Area Diagrams	0	Number of Offline Controls	2	Number of Real Time Controls	0	Rainfall Model	FSR	Ratio R	0.350	Region England and Wales Cv (Summer)			0.750	M5-60 (mm)	19.000	Cv (Winter)	0.840	Margin for Flood Risk Warning (mm)	300.0	Analysis Timestep	2.5 Second Increment (Extended)	DTS Status	OFF	DVD Status	ON	Inertia Status	ON	Profile(s)	Summer and Winter	Duration(s) (mins)	15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080	Return Period(s) (years)	1, 30, 100	Climate Change (%)	0, 0, 40	PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surchage	First (Y) Flood	First (Z) Overflow	Overflow Act.	S1.000	SW-25	15 Winter	1	+0%	100/15 Summer				S2.000	SW-26	15 Winter	1	+0%	100/15 Summer				S1.001	SW-24	15 Winter	1	+0%	100/15 Summer				S1.002	SW-23	15 Winter	1	+0%	30/15 Winter				S3.000	SW-27	15 Winter	1	+0%	100/15 Summer				S4.000	SW-28	15 Winter	1	+0%	30/15 Winter				S1.003	SW-22	5760 Winter	1	+0%	30/15 Summer				S1.004	SW-21	5760 Winter	1	+0%	1/720 Winter				S1.005	SW-20	5760 Winter	1	+0%	1/600 Winter				S1.006	SW-19	5760 Winter	1	+0%	1/480 Winter				S1.007	SW-18	5760 Winter	1	+0%	1/240 Winter				S1.008	SW-17	5760 Winter	1	+0%	1/120 Winter				S1.009	SW-16	5760 Winter	1	+0%	1/120 Winter				S5.000	SCF-01	4320 Winter	1	+0%	30/60 Summer	100/30 Summer			S5.001	SCF-02	4320 Winter	1	+0%	1/2160 Winter	100/30 Summer			S1.010	SW-15	5760 Winter	1	+0%					S6.000	SCF-03	5760 Winter	1	+0%	100/720 Winter	100/720 Winter		
Areal Reduction Factor	1.000	Additional Flow - % of Total Flow	10.000																																																																																																																																																																																																																															
Hot Start (mins)	0	MADD Factor * 10m³/ha Storage	2.000																																																																																																																																																																																																																															
Hot Start Level (mm)	0	Inlet Coefficient	0.800																																																																																																																																																																																																																															
Manhole Headloss Coeff (Global)	0.500	Flow per Person per Day (l/per/day)	0.000																																																																																																																																																																																																																															
Foul Sewage per hectare (l/s)	0.000																																																																																																																																																																																																																																	
Number of Input Hydrographs	0	Number of Storage Structures	6																																																																																																																																																																																																																															
Number of Online Controls	4	Number of Time/Area Diagrams	0																																																																																																																																																																																																																															
Number of Offline Controls	2	Number of Real Time Controls	0																																																																																																																																																																																																																															
Rainfall Model	FSR	Ratio R	0.350																																																																																																																																																																																																																															
Region England and Wales Cv (Summer)			0.750																																																																																																																																																																																																																															
M5-60 (mm)	19.000	Cv (Winter)	0.840																																																																																																																																																																																																																															
Margin for Flood Risk Warning (mm)	300.0																																																																																																																																																																																																																																	
Analysis Timestep	2.5 Second Increment (Extended)																																																																																																																																																																																																																																	
DTS Status	OFF																																																																																																																																																																																																																																	
DVD Status	ON																																																																																																																																																																																																																																	
Inertia Status	ON																																																																																																																																																																																																																																	
Profile(s)	Summer and Winter																																																																																																																																																																																																																																	
Duration(s) (mins)	15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080																																																																																																																																																																																																																																	
Return Period(s) (years)	1, 30, 100																																																																																																																																																																																																																																	
Climate Change (%)	0, 0, 40																																																																																																																																																																																																																																	
PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surchage	First (Y) Flood	First (Z) Overflow	Overflow Act.																																																																																																																																																																																																																										
S1.000	SW-25	15 Winter	1	+0%	100/15 Summer																																																																																																																																																																																																																													
S2.000	SW-26	15 Winter	1	+0%	100/15 Summer																																																																																																																																																																																																																													
S1.001	SW-24	15 Winter	1	+0%	100/15 Summer																																																																																																																																																																																																																													
S1.002	SW-23	15 Winter	1	+0%	30/15 Winter																																																																																																																																																																																																																													
S3.000	SW-27	15 Winter	1	+0%	100/15 Summer																																																																																																																																																																																																																													
S4.000	SW-28	15 Winter	1	+0%	30/15 Winter																																																																																																																																																																																																																													
S1.003	SW-22	5760 Winter	1	+0%	30/15 Summer																																																																																																																																																																																																																													
S1.004	SW-21	5760 Winter	1	+0%	1/720 Winter																																																																																																																																																																																																																													
S1.005	SW-20	5760 Winter	1	+0%	1/600 Winter																																																																																																																																																																																																																													
S1.006	SW-19	5760 Winter	1	+0%	1/480 Winter																																																																																																																																																																																																																													
S1.007	SW-18	5760 Winter	1	+0%	1/240 Winter																																																																																																																																																																																																																													
S1.008	SW-17	5760 Winter	1	+0%	1/120 Winter																																																																																																																																																																																																																													
S1.009	SW-16	5760 Winter	1	+0%	1/120 Winter																																																																																																																																																																																																																													
S5.000	SCF-01	4320 Winter	1	+0%	30/60 Summer	100/30 Summer																																																																																																																																																																																																																												
S5.001	SCF-02	4320 Winter	1	+0%	1/2160 Winter	100/30 Summer																																																																																																																																																																																																																												
S1.010	SW-15	5760 Winter	1	+0%																																																																																																																																																																																																																														
S6.000	SCF-03	5760 Winter	1	+0%	100/720 Winter	100/720 Winter																																																																																																																																																																																																																												
©1982-2017 XP Solutions																																																																																																																																																																																																																																		

Rogers Cory Partnership							Page 44		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>									
PN	US/MH Name	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S1.000	SW-25	4.512	-0.200	0.000	0.23		18.1	OK	
S2.000	SW-26	4.675	-0.164	0.000	0.16		10.8	OK	
S1.001	SW-24	4.449	-0.235	0.000	0.30		33.9	OK	
S1.002	SW-23	4.331	-0.206	0.000	0.41		44.1	OK	
S3.000	SW-27	4.522	-0.148	0.000	0.25		9.1	OK	
S4.000	SW-28	4.371	-0.154	0.000	0.21		7.8	OK	
S1.003	SW-22	4.278	-0.104	0.000	0.01		2.0	OK	
S1.004	SW-21	4.278	0.084	0.000	0.02		2.4	SURCHARGED	
S1.005	SW-20	4.278	0.114	0.000	0.03		2.4	SURCHARGED	
S1.006	SW-19	4.277	0.135	0.000	0.02		2.4	SURCHARGED	
S1.007	SW-18	4.277	0.181	0.000	0.02		2.5	SURCHARGED	
S1.008	SW-17	4.276	0.259	0.000	0.03		2.8	SURCHARGED	
S1.009	SW-16	4.276	0.291	0.000	0.03		2.8	SURCHARGED	
S5.000	SCF-01	4.288	-0.012	0.000	0.02		0.9	OK	26
S5.001	SCF-02	4.288	0.028	0.000	0.03		1.2	SURCHARGED	26
S1.010	SW-15	4.275	-0.925	0.000	0.00		2.9	OK	
S6.000	SCF-03	4.282	-0.818	0.000	0.00		1.7	OK	7
©1982-2017 XP Solutions									

Rogers Cory Partnership							Page 45		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>									
PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surcharge	First (Y) Flood	First (Z) Overflow		
S6.001	SCF-04	5760 Winter	1	+0%	100/720 Winter	100/720 Winter			
S1.011	SW-14	5760 Winter	1	+0%					
S1.012	SW-13	5760 Winter	1	+0%					
S1.013	SW-12	5760 Winter	1	+0%	1/15 Summer				
S1.014	SW-11	5760 Winter	1	+0%					
S1.015	SW-10	5760 Winter	1	+0%	1/15 Summer			30/480 Winter	
S1.016	SW-9	4320 Winter	1	+0%	100/2880 Winter	100/1440 Winter			
S1.017	SW-8	4320 Winter	1	+0%	100/4320 Winter	100/1440 Winter			
S7.000	SW-39	15 Winter	1	+0%	30/360 Winter	100/15 Summer			
S7.001	SW-38	4320 Winter	1	+0%	1/720 Winter	100/15 Winter			
S7.002	SW-37	4320 Winter	1	+0%	1/360 Winter				
S7.003	SW-36	4320 Winter	1	+0%	1/180 Winter				
S8.000	S26	4320 Winter	1	+0%	30/180 Winter				
S7.004	SW-35	4320 Winter	1	+0%	1/60 Winter				
S7.005	SW-34	4320 Winter	1	+0%	1/60 Summer				
S7.006	SW-33	4320 Winter	1	+0%	1/30 Summer				
S9.000	SW-42	4320 Winter	1	+0%	1/120 Winter				
S9.001	SW-41	4320 Winter	1	+0%	1/120 Summer				
S9.002	SW-40	4320 Winter	1	+0%	1/60 Summer				
S7.007	SW-32	4320 Winter	1	+0%					
S7.008	SW-31	4320 Winter	1	+0%	1/15 Summer				
S7.009	SW-30	4320 Winter	1	+0%	1/15 Summer				
S7.010	SW-29	4320 Winter	1	+0%	1/15 Summer				
S1.018	SW-7	4320 Winter	1	+0%	100/2160 Winter	100/1440 Winter			
S1.019	SW-6	4320 Winter	1	+0%		100/1440 Winter			
S10.000	SW-44	4320 Winter	1	+0%	1/15 Summer				
S10.001	SW-43	4320 Winter	1	+0%	1/15 Summer				
S1.020	SW-5	4320 Winter	1	+0%					
S11.000	SW-45	4320 Winter	1	+0%	1/120 Winter				
S1.021	SW-4	4320 Winter	1	+0%					
S1.022	SW-2	4320 Winter	1	+0%	1/15 Summer			100/1440 Winter	
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Pipe Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status
S6.001	SCF-04		4.286	-0.814	0.000	0.00		1.7	OK
S1.011	SW-14		4.275	-0.925	0.000	0.00		3.2	OK
S1.012	SW-13		4.275	-0.925	0.000	0.00		3.2	OK
S1.013	SW-12		4.275	0.439	0.000	0.08		3.4	SURCHARGED
S1.014	SW-11		4.274	-0.926	0.000	0.00		3.4	OK
S1.015	SW-10	50	4.274	0.479	0.000	0.02	0.0	3.5	SURCHARGED
S1.016	SW-9		4.236	-0.864	0.000	0.00		2.3	OK
S1.017	SW-8		4.236	-0.864	0.000	0.00		2.5	OK
S7.000	SW-39		4.243	-0.149	0.000	0.24		9.1	OK
S7.001	SW-38		4.239	0.070	0.000	0.01		0.4	SURCHARGED
S7.002	SW-37		4.238	0.147	0.000	0.01		0.4	SURCHARGED
©1982-2017 XP Solutions									

Rogers Cory Partnership							Page 46			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham						
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX				Designed by Terry Seymour Checked by Terry Seymour						
Innovyze				Network 2017.1.2						
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>										
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	
S7.003	SW-36		4.238	0.235	0.000	0.01		0.8	SURCHARGED	
S8.000	S26		4.238	-0.062	0.000	0.01		0.6	OK	
S7.004	SW-35		4.238	0.428	0.000	0.02		1.8	SURCHARGED	
S7.005	SW-34		4.237	0.544	0.000	0.02		2.5	SURCHARGED	
S7.006	SW-33		4.237	0.589	0.000	0.03		2.5	SURCHARGED	
S9.000	SW-42		4.237	0.284	0.000	0.00		0.1	SURCHARGED	
S9.001	SW-41		4.237	0.363	0.000	0.01		0.3	SURCHARGED	
S9.002	SW-40		4.237	0.473	0.000	0.01		0.5	SURCHARGED	
S7.007	SW-32		4.236	-0.964	0.000	0.00		2.9	OK	
S7.008	SW-31		4.236	0.646	0.000	0.02		2.9	SURCHARGED	
S7.009	SW-30		4.236	0.673	0.000	0.02		2.9	SURCHARGED	
S7.010	SW-29		4.236	0.686	0.000	0.02		2.9	SURCHARGED	
S1.018	SW-7		4.235	-0.865	0.000	0.00		4.2	OK	
S1.019	SW-6		4.235	-0.865	0.000	0.00		4.2	OK	
S10.000	SW-44		4.235	0.692	0.000	0.01		0.2	SURCHARGED	
S10.001	SW-43		4.235	0.781	0.000	0.01		0.4	SURCHARGED	
S1.020	SW-5		4.235	-0.865	0.000	0.00		10.9	OK	
S11.000	SW-45		4.234	0.317	0.000	0.02		0.8	SURCHARGED	
S1.021	SW-4		4.239	-0.861	0.000	0.00		13.0	OK	
S1.022	SW-2	4	4.242	0.839	0.000	0.11	0.0	4.6	SURCHARGED	
PN	US/MH Name	Level Exceeded								
S6.001	SCF-04	7								
S1.011	SW-14									
S1.012	SW-13									
S1.013	SW-12									
S1.014	SW-11									
S1.015	SW-10									
S1.016	SW-9	2								
S1.017	SW-8	1								
S7.000	SW-39	4								
S7.001	SW-38	1								
S7.002	SW-37									
S7.003	SW-36									
S8.000	S26									
S7.004	SW-35									
S7.005	SW-34									
S7.006	SW-33									
S9.000	SW-42									
S9.001	SW-41									
S9.002	SW-40									
S7.007	SW-32									
S7.008	SW-31									
S7.009	SW-30									

©1982-2017 XP Solutions

Rogers Cory Partnership		Page 47																																	
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham																																		
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX	Designed by Terry Seymour Checked by Terry Seymour																																		
Innovyze	Network 2017.1.2																																		
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>																																			
	<table><tr><td></td><td>US/MH</td><td>Level</td></tr><tr><td>PN</td><td>Name</td><td>Exceeded</td></tr><tr><td>S7.010</td><td>SW-29</td><td></td></tr><tr><td>S1.018</td><td>SW-7</td><td>1</td></tr><tr><td>S1.019</td><td>SW-6</td><td></td></tr><tr><td>S10.000</td><td>SW-44</td><td></td></tr><tr><td>S10.001</td><td>SW-43</td><td></td></tr><tr><td>S1.020</td><td>SW-5</td><td></td></tr><tr><td>S11.000</td><td>SW-45</td><td></td></tr><tr><td>S1.021</td><td>SW-4</td><td></td></tr><tr><td>S1.022</td><td>SW-2</td><td></td></tr></table>		US/MH	Level	PN	Name	Exceeded	S7.010	SW-29		S1.018	SW-7	1	S1.019	SW-6		S10.000	SW-44		S10.001	SW-43		S1.020	SW-5		S11.000	SW-45		S1.021	SW-4		S1.022	SW-2		
	US/MH	Level																																	
PN	Name	Exceeded																																	
S7.010	SW-29																																		
S1.018	SW-7	1																																	
S1.019	SW-6																																		
S10.000	SW-44																																		
S10.001	SW-43																																		
S1.020	SW-5																																		
S11.000	SW-45																																		
S1.021	SW-4																																		
S1.022	SW-2																																		
©1982-2017 XP Solutions																																			

Rogers Cory Partnership				Page 48				
The Old School Old School Road Hook Hampshire RG27 9NJ			Summer Lane Pagham					
Date 25/06/2019 15:38			Designed by Terry Seymour					
File SW1-with Crayfern site.MDX			Checked by Terry Seymour					
Innovyze			Network 2017.1.2					
<u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>								
<u>Simulation Criteria</u>								
Areal Reduction Factor		1.000	Additional Flow - % of Total Flow		10.000			
Hot Start (mins)		0	MADD Factor * 10m³/ha Storage		2.000			
Hot Start Level (mm)		0	Inlet Coefficient		0.800			
Manhole Headloss Coeff (Global)		0.500	Flow per Person per Day (l/per/day)		0.000			
Foul Sewage per hectare (l/s)		0.000						
Number of Input Hydrographs		0	Number of Storage Structures		6			
Number of Online Controls		4	Number of Time/Area Diagrams		0			
Number of Offline Controls		2	Number of Real Time Controls		0			
<u>Synthetic Rainfall Details</u>								
Rainfall Model		FSR	Ratio R		0.350			
Region England and Wales Cv (Summer)		0.750						
M5-60 (mm)		19.000	Cv (Winter)		0.840			
Margin for Flood Risk Warning (mm)					300.0			
Analysis Timestep		2.5 Second Increment (Extended)						
DTS Status					OFF			
DVD Status					ON			
Inertia Status					ON			
Profile(s)					Summer and Winter			
Duration(s) (mins)		15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080						
Return Period(s) (years)					1, 30, 100			
Climate Change (%)					0, 0, 40			
PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surchage	First (Y) Flood	First (Z) Overflow	Overflow Act.
S1.000	SW-25	15 Winter	30	+0%	100/15 Summer			
S2.000	SW-26	15 Winter	30	+0%	100/15 Summer			
S1.001	SW-24	15 Winter	30	+0%	100/15 Summer			
S1.002	SW-23	60 Winter	30	+0%	30/15 Winter			
S3.000	SW-27	2160 Winter	30	+0%	100/15 Summer			
S4.000	SW-28	2160 Winter	30	+0%	30/15 Winter			
S1.003	SW-22	2160 Winter	30	+0%	30/15 Summer			
S1.004	SW-21	2160 Winter	30	+0%	1/720 Winter			
S1.005	SW-20	2160 Winter	30	+0%	1/600 Winter			
S1.006	SW-19	2160 Winter	30	+0%	1/480 Winter			
S1.007	SW-18	2160 Winter	30	+0%	1/240 Winter			
S1.008	SW-17	2160 Winter	30	+0%	1/120 Winter			
S1.009	SW-16	2160 Winter	30	+0%	1/120 Winter			
S5.000	SCF-01	360 Winter	30	+0%	30/60 Summer	100/30 Summer		
S5.001	SCF-02	360 Winter	30	+0%	1/2160 Winter	100/30 Summer		
S1.010	SW-15	2160 Winter	30	+0%				
S6.000	SCF-03	2160 Winter	30	+0%	100/720 Winter	100/720 Winter		
©1982-2017 XP Solutions								

Rogers Cory Partnership							Page 49		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>									
PN	US/MH Name	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S1.000	SW-25	4.691	-0.021	0.000	0.48		37.5	OK	
S2.000	SW-26	4.714	-0.125	0.000	0.40		26.5	OK	
S1.001	SW-24	4.666	-0.018	0.000	0.67		76.8	OK	
S1.002	SW-23	4.598	0.061	0.000	0.61		65.4	SURCHARGED	
S3.000	SW-27	4.581	-0.089	0.000	0.02		0.9	OK	
S4.000	SW-28	4.581	0.056	0.000	0.02		0.8	SURCHARGED	
S1.003	SW-22	4.580	0.198	0.000	0.05		7.9	SURCHARGED	
S1.004	SW-21	4.579	0.385	0.000	0.09		9.2	SURCHARGED	
S1.005	SW-20	4.578	0.414	0.000	0.10		9.2	SURCHARGED	
S1.006	SW-19	4.578	0.436	0.000	0.08		9.3	SURCHARGED	
S1.007	SW-18	4.577	0.481	0.000	0.07		9.3	SURCHARGED	
S1.008	SW-17	4.575	0.558	0.000	0.10		10.4	SURCHARGED	
S1.009	SW-16	4.574	0.589	0.000	0.10		10.4	SURCHARGED	
S5.000	SCF-01	4.634	0.334	0.000	0.13		7.1	SURCHARGED	26
S5.001	SCF-02	4.629	0.369	0.000	0.15		7.1	SURCHARGED	26
S1.010	SW-15	4.574	-0.626	0.000	0.00		12.4	OK	
S6.000	SCF-03	4.607	-0.493	0.000	0.00		3.1	OK	7
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 50			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>									
PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surcharge	First (Y) Flood	First (Z) Overflow		
S6.001	SCF-04	2160 Winter	30	+0%	100/720 Winter	100/720 Winter			
S1.011	SW-14	2160 Winter	30	+0%					
S1.012	SW-13	2160 Winter	30	+0%					
S1.013	SW-12	2160 Winter	30	+0%	1/15 Summer				
S1.014	SW-11	2160 Winter	30	+0%					
S1.015	SW-10	2160 Winter	30	+0%	1/15 Summer		30/480 Winter		
S1.016	SW-9	2160 Winter	30	+0%	100/2880 Winter	100/1440 Winter			
S1.017	SW-8	2160 Winter	30	+0%	100/4320 Winter	100/1440 Winter			
S7.000	SW-39	2160 Winter	30	+0%	30/360 Winter	100/15 Summer			
S7.001	SW-38	2160 Winter	30	+0%	1/720 Winter	100/15 Winter			
S7.002	SW-37	2160 Winter	30	+0%	1/360 Winter				
S7.003	SW-36	2160 Winter	30	+0%	1/180 Winter				
S8.000	S26	2160 Winter	30	+0%	30/180 Winter				
S7.004	SW-35	2160 Winter	30	+0%	1/60 Winter				
S7.005	SW-34	2160 Winter	30	+0%	1/60 Summer				
S7.006	SW-33	2160 Winter	30	+0%	1/30 Summer				
S9.000	SW-42	2160 Winter	30	+0%	1/120 Winter				
S9.001	SW-41	2160 Winter	30	+0%	1/120 Summer				
S9.002	SW-40	2160 Winter	30	+0%	1/60 Summer				
S7.007	SW-32	2160 Winter	30	+0%					
S7.008	SW-31	2160 Winter	30	+0%	1/15 Summer				
S7.009	SW-30	2160 Winter	30	+0%	1/15 Summer				
S7.010	SW-29	2160 Winter	30	+0%	1/15 Summer				
S1.018	SW-7	2160 Winter	30	+0%	100/2160 Winter	100/1440 Winter			
S1.019	SW-6	2160 Winter	30	+0%		100/1440 Winter			
S10.000	SW-44	2160 Winter	30	+0%	1/15 Summer				
S10.001	SW-43	2160 Winter	30	+0%	1/15 Summer				
S1.020	SW-5	2160 Winter	30	+0%					
S11.000	SW-45	2160 Winter	30	+0%	1/120 Winter				
S1.021	SW-4	2160 Winter	30	+0%					
S1.022	SW-2	2160 Winter	30	+0%	1/15 Summer		100/1440 Winter		
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Pipe Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status
S6.001	SCF-04		4.607	-0.493	0.000	0.00		1.2	OK
S1.011	SW-14		4.574	-0.626	0.000	0.00		10.1	OK
S1.012	SW-13		4.574	-0.626	0.000	0.00		10.1	OK
S1.013	SW-12		4.573	0.737	0.000	0.23		9.6	SURCHARGED
S1.014	SW-11		4.570	-0.630	0.000	0.00		9.6	OK
S1.015	SW-10	50	4.570	0.775	0.000	0.03	7.3	4.3	SURCHARGED
S1.016	SW-9		4.555	-0.545	0.000	0.00		9.5	OK
S1.017	SW-8		4.554	-0.546	0.000	0.00		9.5	OK
S7.000	SW-39		4.560	0.168	0.000	0.02		0.9	SURCHARGED
S7.001	SW-38		4.560	0.391	0.000	0.04		1.4	SURCHARGED
S7.002	SW-37		4.559	0.468	0.000	0.04		1.4	SURCHARGED
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 51	
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>									
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Pipe Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status
S7.003	SW-36		4.559	0.556	0.000	0.04		2.5	SURCHARGED
S8.000	S26		4.557	0.257	0.000	0.02		1.8	SURCHARGED
S7.004	SW-35		4.557	0.747	0.000	0.06		5.8	SURCHARGED
S7.005	SW-34		4.556	0.863	0.000	0.07		8.3	SURCHARGED
S7.006	SW-33		4.556	0.908	0.000	0.08		8.3	SURCHARGED
S9.000	SW-42		4.556	0.603	0.000	0.01		0.3	SURCHARGED
S9.001	SW-41		4.556	0.682	0.000	0.03		1.1	SURCHARGED
S9.002	SW-40		4.556	0.792	0.000	0.03		1.4	SURCHARGED
S7.007	SW-32		4.555	-0.645	0.000	0.00		9.7	OK
S7.008	SW-31		4.555	0.965	0.000	0.06		7.4	SURCHARGED
S7.009	SW-30		4.554	0.991	0.000	0.05		7.4	SURCHARGED
S7.010	SW-29		4.554	1.004	0.000	0.05		7.4	SURCHARGED
S1.018	SW-7		4.554	-0.546	0.000	0.00		10.4	OK
S1.019	SW-6		4.553	-0.547	0.000	0.00		9.2	OK
S10.000	SW-44		4.552	1.009	0.000	0.02		0.6	SURCHARGED
S10.001	SW-43		4.552	1.098	0.000	0.03		1.0	SURCHARGED
S1.020	SW-5		4.552	-0.548	0.000	0.00		11.9	OK
S11.000	SW-45		4.552	0.635	0.000	0.05		1.9	SURCHARGED
S1.021	SW-4		4.555	-0.545	0.000	0.00		13.7	OK
S1.022	SW-2	4	4.561	1.158	0.000	0.19	0.0	7.9	SURCHARGED
PN	US/MH Name		Level Exceeded						
S6.001	SCF-04		7						
S1.011	SW-14								
S1.012	SW-13								
S1.013	SW-12								
S1.014	SW-11								
S1.015	SW-10								
S1.016	SW-9		2						
S1.017	SW-8		1						
S7.000	SW-39		4						
S7.001	SW-38		1						
S7.002	SW-37								
S7.003	SW-36								
S8.000	S26								
S7.004	SW-35								
S7.005	SW-34								
S7.006	SW-33								
S9.000	SW-42								
S9.001	SW-41								
S9.002	SW-40								
S7.007	SW-32								
S7.008	SW-31								
S7.009	SW-30								
©1982-2017 XP Solutions									

Rogers Cory Partnership		Page 52																														
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham																															
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX	Designed by Terry Seymour Checked by Terry Seymour																															
Innovyze	Network 2017.1.2																															
<u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>																																
	<table><thead><tr><th>PN</th><th>US/MH Name</th><th>Level Exceeded</th></tr></thead><tbody><tr><td>S7.010</td><td>SW-29</td><td></td></tr><tr><td>S1.018</td><td>SW-7</td><td>1</td></tr><tr><td>S1.019</td><td>SW-6</td><td></td></tr><tr><td>S10.000</td><td>SW-44</td><td></td></tr><tr><td>S10.001</td><td>SW-43</td><td></td></tr><tr><td>S1.020</td><td>SW-5</td><td></td></tr><tr><td>S11.000</td><td>SW-45</td><td></td></tr><tr><td>S1.021</td><td>SW-4</td><td></td></tr><tr><td>S1.022</td><td>SW-2</td><td></td></tr></tbody></table>	PN	US/MH Name	Level Exceeded	S7.010	SW-29		S1.018	SW-7	1	S1.019	SW-6		S10.000	SW-44		S10.001	SW-43		S1.020	SW-5		S11.000	SW-45		S1.021	SW-4		S1.022	SW-2		
PN	US/MH Name	Level Exceeded																														
S7.010	SW-29																															
S1.018	SW-7	1																														
S1.019	SW-6																															
S10.000	SW-44																															
S10.001	SW-43																															
S1.020	SW-5																															
S11.000	SW-45																															
S1.021	SW-4																															
S1.022	SW-2																															
©1982-2017 XP Solutions																																

Rogers Cory Partnership				Page 53				
The Old School Old School Road Hook Hampshire RG27 9NJ			Summer Lane Pagham					
Date 25/06/2019 15:38			Designed by Terry Seymour					
File SW1-with Crayfern site.MDX			Checked by Terry Seymour					
Innovyze			Network 2017.1.2					
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>								
<u>Simulation Criteria</u>								
Areal Reduction Factor		1.000	Additional Flow - % of Total Flow		10.000			
Hot Start (mins)		0	MADD Factor * 10m³/ha Storage		2.000			
Hot Start Level (mm)		0	Inlet Coefficient		0.800			
Manhole Headloss Coeff (Global)		0.500	Flow per Person per Day (l/per/day)		0.000			
Foul Sewage per hectare (l/s)		0.000						
Number of Input Hydrographs		0	Number of Storage Structures		6			
Number of Online Controls		4	Number of Time/Area Diagrams		0			
Number of Offline Controls		2	Number of Real Time Controls		0			
<u>Synthetic Rainfall Details</u>								
Rainfall Model		FSR	Ratio R		0.350			
Region England and Wales Cv (Summer)		0.750						
M5-60 (mm)		19.000	Cv (Winter)		0.840			
Margin for Flood Risk Warning (mm)					300.0			
Analysis Timestep		2.5 Second Increment (Extended)						
DTS Status					OFF			
DVD Status					ON			
Inertia Status					ON			
Profile(s)					Summer and Winter			
Duration(s) (mins)		15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080						
Return Period(s) (years)					1, 30, 100			
Climate Change (%)					0, 0, 40			
PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surchage	First (Y) Flood	First (Z) Overflow	Overflow Act.
S1.000	SW-25	30 Winter	100	+40%	100/15 Summer			
S2.000	SW-26	15 Winter	100	+40%	100/15 Summer			
S1.001	SW-24	15 Winter	100	+40%	100/15 Summer			
S1.002	SW-23	15 Winter	100	+40%	30/15 Winter			
S3.000	SW-27	15 Winter	100	+40%	100/15 Summer			
S4.000	SW-28	15 Winter	100	+40%	30/15 Winter			
S1.003	SW-22	2160 Winter	100	+40%	30/15 Summer			
S1.004	SW-21	2160 Winter	100	+40%	1/720 Winter			
S1.005	SW-20	2160 Winter	100	+40%	1/600 Winter			
S1.006	SW-19	2160 Winter	100	+40%	1/480 Winter			
S1.007	SW-18	2160 Winter	100	+40%	1/240 Winter			
S1.008	SW-17	2160 Winter	100	+40%	1/120 Winter			
S1.009	SW-16	2160 Winter	100	+40%	1/120 Winter			
S5.000	SCF-01	240 Winter	100	+40%	30/60 Summer	100/30 Summer		
S5.001	SCF-02	240 Winter	100	+40%	1/2160 Winter	100/30 Summer		
S1.010	SW-15	2160 Winter	100	+40%				
S6.000	SCF-03	2160 Winter	100	+40%	100/720 Winter	100/720 Winter		
©1982-2017 XP Solutions								

Rogers Cory Partnership							Page 54		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>									
PN	US/MH Name	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S1.000	SW-25	5.208	0.496	0.000	0.45		34.9	FLOOD RISK	
S2.000	SW-26	5.341	0.502	0.000	0.66		43.7	FLOOD RISK	
S1.001	SW-24	5.188	0.504	0.000	0.66		75.4	SURCHARGED	
S1.002	SW-23	5.193	0.656	0.000	0.97		102.9	SURCHARGED	
S3.000	SW-27	5.253	0.583	0.000	1.03		37.7	FLOOD RISK	
S4.000	SW-28	5.217	0.692	0.000	0.89		32.5	FLOOD RISK	
S1.003	SW-22	5.130	0.748	0.000	0.08		12.9	SURCHARGED	
S1.004	SW-21	5.128	0.934	0.000	0.15		15.1	FLOOD RISK	
S1.005	SW-20	5.126	0.962	0.000	0.16		15.2	FLOOD RISK	
S1.006	SW-19	5.125	0.983	0.000	0.12		15.3	FLOOD RISK	
S1.007	SW-18	5.123	1.027	0.000	0.11		15.2	FLOOD RISK	
S1.008	SW-17	5.121	1.104	0.000	0.17		17.0	FLOOD RISK	
S1.009	SW-16	5.119	1.134	0.000	0.17		17.0	SURCHARGED	
S5.000	SCF-01	5.146	0.846	10.568	0.52		28.4	FLOOD	26
S5.001	SCF-02	5.140	0.880	39.797	0.17		8.0	FLOOD	26
S1.010	SW-15	5.118	-0.082	0.000	0.00		22.8	FLOOD RISK	
S6.000	SCF-03	5.127	0.027	3.803	0.00		6.6	FLOOD	7
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 55			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 15:38				Designed by Terry Seymour					
File SW1-with Crayfern site.MDX				Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>									
PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surcharge	First (Y) Flood	First (Z) Overflow		
S6.001	SCF-04	2160 Winter	100	+40%	100/720 Winter	100/720 Winter			
S1.011	SW-14	2160 Winter	100	+40%					
S1.012	SW-13	2160 Winter	100	+40%					
S1.013	SW-12	2160 Winter	100	+40%	1/15 Summer				
S1.014	SW-11	2160 Winter	100	+40%					
S1.015	SW-10	2160 Winter	100	+40%	1/15 Summer		30/480 Winter		
S1.016	SW-9	2880 Winter	100	+40%	100/2880 Winter	100/1440 Winter			
S1.017	SW-8	4320 Winter	100	+40%	100/4320 Winter	100/1440 Winter			
S7.000	SW-39	15 Winter	100	+40%	30/360 Winter	100/15 Summer			
S7.001	SW-38	15 Winter	100	+40%	1/720 Winter	100/15 Winter			
S7.002	SW-37	15 Winter	100	+40%	1/360 Winter				
S7.003	SW-36	15 Winter	100	+40%	1/180 Winter				
S8.000	S26	2880 Winter	100	+40%	30/180 Winter				
S7.004	SW-35	2880 Winter	100	+40%	1/60 Winter				
S7.005	SW-34	2880 Winter	100	+40%	1/60 Summer				
S7.006	SW-33	2880 Winter	100	+40%	1/30 Summer				
S9.000	SW-42	2880 Winter	100	+40%	1/120 Winter				
S9.001	SW-41	2880 Winter	100	+40%	1/120 Summer				
S9.002	SW-40	2880 Winter	100	+40%	1/60 Summer				
S7.007	SW-32	2880 Winter	100	+40%					
S7.008	SW-31	2880 Winter	100	+40%	1/15 Summer				
S7.009	SW-30	2160 Winter	100	+40%	1/15 Summer				
S7.010	SW-29	2160 Winter	100	+40%	1/15 Summer				
S1.018	SW-7	2160 Winter	100	+40%	100/2160 Winter	100/1440 Winter			
S1.019	SW-6	2160 Winter	100	+40%		100/1440 Winter			
S10.000	SW-44	2880 Winter	100	+40%	1/15 Summer				
S10.001	SW-43	2880 Winter	100	+40%	1/15 Summer				
S1.020	SW-5	2880 Winter	100	+40%					
S11.000	SW-45	2880 Winter	100	+40%	1/120 Winter				
S1.021	SW-4	2880 Winter	100	+40%					
S1.022	SW-2	2880 Winter	100	+40%	1/15 Summer		100/1440 Winter		
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Pipe Flow (1/s)	Overflow (1/s)	Status
S6.001	SCF-04		5.127	0.027	27.495	0.00		2.9	FLOOD
S1.011	SW-14		5.113	-0.087	0.000	0.01		21.5	FLOOD RISK
S1.012	SW-13		5.112	-0.088	0.000	0.01		21.1	FLOOD RISK
S1.013	SW-12		5.110	1.274	0.000	0.35		14.7	FLOOD RISK
S1.014	SW-11		5.106	-0.094	0.000	0.00		14.7	FLOOD RISK
S1.015	SW-10	50	5.105	1.310	0.000	0.03	11.8	4.8	FLOOD RISK
S1.016	SW-9		5.100	0.000	0.000	0.00		14.1	FLOOD
S1.017	SW-8		5.100	0.000	0.000	0.00		12.7	FLOOD
S7.000	SW-39		5.204	0.812	4.040	1.11		41.9	FLOOD
S7.001	SW-38		5.200	1.031	0.066	1.42		48.8	FLOOD
S7.002	SW-37		5.178	1.087	0.000	1.42		49.7	FLOOD RISK
©1982-2017 XP Solutions									

Rogers Cory Partnership							Page 56			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham						
Date 25/06/2019 15:38				Designed by Terry Seymour						
File SW1-with Crayfern site.MDX				Checked by Terry Seymour						
Innovyze				Network 2017.1.2						
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>										
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	
S7.003	SW-36		5.120	1.117	0.000	1.07		70.9	FLOOD RISK	
S8.000	S26		5.110	0.810	0.000	0.02		2.5	FLOOD RISK	
S7.004	SW-35		5.109	1.299	0.000	0.08		8.1	FLOOD RISK	
S7.005	SW-34		5.107	1.414	0.000	0.10		11.5	FLOOD RISK	
S7.006	SW-33		5.105	1.457	0.000	0.11		11.5	FLOOD RISK	
S9.000	SW-42		5.106	1.153	0.000	0.01		0.4	FLOOD RISK	
S9.001	SW-41		5.106	1.232	0.000	0.04		1.5	FLOOD RISK	
S9.002	SW-40		5.105	1.341	0.000	0.04		2.0	FLOOD RISK	
S7.007	SW-32		5.104	-0.096	0.000	0.00		13.4	FLOOD RISK	
S7.008	SW-31		5.102	1.512	0.000	0.07		8.5	FLOOD RISK	
S7.009	SW-30		5.101	1.538	0.000	0.06		10.2	FLOOD RISK	
S7.010	SW-29		5.101	1.551	0.000	0.07		10.2	FLOOD RISK	
S1.018	SW-7		5.100	0.000	0.011	0.00		14.5	FLOOD	
S1.019	SW-6		5.100	0.000	0.000	0.00		12.1	FLOOD	
S10.000	SW-44		5.093	1.550	0.000	0.02		0.9	FLOOD RISK	
S10.001	SW-43		5.092	1.638	0.000	0.04		1.4	FLOOD RISK	
S1.020	SW-5		5.092	-0.008	0.000	0.00		11.4	FLOOD RISK	
S11.000	SW-45		5.071	1.154	0.000	0.06		2.4	FLOOD RISK	
S1.021	SW-4		5.070	-0.030	0.000	0.00		13.1	FLOOD RISK	
S1.022	SW-2	4	5.065	1.662	0.000	0.19	5.0	7.9	FLOOD RISK	
PN	US/MH Name	Level Exceeded								
S6.001	SCF-04	7								
S1.011	SW-14									
S1.012	SW-13									
S1.013	SW-12									
S1.014	SW-11									
S1.015	SW-10									
S1.016	SW-9	2								
S1.017	SW-8	1								
S7.000	SW-39	4								
S7.001	SW-38	1								
S7.002	SW-37									
S7.003	SW-36									
S8.000	S26									
S7.004	SW-35									
S7.005	SW-34									
S7.006	SW-33									
S9.000	SW-42									
S9.001	SW-41									
S9.002	SW-40									
S7.007	SW-32									
S7.008	SW-31									
S7.009	SW-30									
©1982-2017 XP Solutions										

Rogers Cory Partnership		Page 57																														
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham																															
Date 25/06/2019 15:38 File SW1-with Crayfern site.MDX	Designed by Terry Seymour Checked by Terry Seymour																															
Innovyze	Network 2017.1.2																															
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>																																
	<table><thead><tr><th>PN</th><th>US/MH Name</th><th>Level Exceeded</th></tr></thead><tbody><tr><td>S7.010</td><td>SW-29</td><td></td></tr><tr><td>S1.018</td><td>SW-7</td><td>1</td></tr><tr><td>S1.019</td><td>SW-6</td><td></td></tr><tr><td>S10.000</td><td>SW-44</td><td></td></tr><tr><td>S10.001</td><td>SW-43</td><td></td></tr><tr><td>S1.020</td><td>SW-5</td><td></td></tr><tr><td>S11.000</td><td>SW-45</td><td></td></tr><tr><td>S1.021</td><td>SW-4</td><td></td></tr><tr><td>S1.022</td><td>SW-2</td><td></td></tr></tbody></table>	PN	US/MH Name	Level Exceeded	S7.010	SW-29		S1.018	SW-7	1	S1.019	SW-6		S10.000	SW-44		S10.001	SW-43		S1.020	SW-5		S11.000	SW-45		S1.021	SW-4		S1.022	SW-2		
PN	US/MH Name	Level Exceeded																														
S7.010	SW-29																															
S1.018	SW-7	1																														
S1.019	SW-6																															
S10.000	SW-44																															
S10.001	SW-43																															
S1.020	SW-5																															
S11.000	SW-45																															
S1.021	SW-4																															
S1.022	SW-2																															
©1982-2017 XP Solutions																																

Rogers Cory Partnership		Page 0
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 16:32 File SW1.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		

STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for SW-1.SWS

Pipe Sizes SW-1 Manhole Sizes SW-1

FSR Rainfall Model - England and Wales

Return Period (years)	2	PIMP (%)	100
M5-60 (mm)	19.000	Add Flow / Climate Change (%)	10
Ratio R	0.350	Minimum Backdrop Height (m)	0.200
Maximum Rainfall (mm/hr)	50	Maximum Backdrop Height (m)	0.000
Maximum Time of Concentration (mins)	30	Min Design Depth for Optimisation (m)	1.200
Foul Sewage (l/s/ha)	0.000	Min Vel for Auto Design only (m/s)	0.75
Volumetric Runoff Coeff.	0.750	Min Slope for Optimisation (1:X)	500

Designed with Level Soffits

Network Design Table for SW-1.SWS

« - Indicates pipe capacity < flow

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	n	HYD SECT	DIA (mm)	Section Type	Auto Design
S1.000	30.250	0.178	169.9	0.141	5.00	0.0	0.600		o	300	Pipe/Conduit	
S2.000	19.464	0.380	51.2	0.078	5.00	0.0	0.600		o	225	Pipe/Conduit	
S1.001	35.964	0.147	244.7	0.054	0.00	0.0	0.600		o	375	Pipe/Conduit	
S1.002	19.565	0.080	244.6	0.104	0.00	0.0	0.600		o	375	Pipe/Conduit	
S3.000	24.269	0.143	169.7	0.066	5.00	0.0	0.600		o	225	Pipe/Conduit	
S4.000	25.210	0.148	170.3	0.057	5.00	0.0	0.600		o	225	Pipe/Conduit	

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
S1.000	50.00	5.42	4.412	0.141	0.0	0.0	1.9	1.20	85.0	21.0
S2.000	50.00	5.18	4.614	0.078	0.0	0.0	1.1	1.83	72.8	11.6
S1.001	50.00	5.94	4.309	0.273	0.0	0.0	3.7	1.15	127.4	40.7
S1.002	50.00	6.22	4.162	0.377	0.0	0.0	5.1	1.15	127.5	56.2
S3.000	50.00	5.40	4.445	0.066	0.0	0.0	0.9	1.00	39.8	9.8
S4.000	50.00	5.42	4.300	0.057	0.0	0.0	0.8	1.00	39.7	8.5

©1982-2017 XP Solutions

Rogers Cory Partnership											Page 1	
The Old School Old School Road Hook Hampshire RG27 9NJ						Summer Lane Pagham						
Date 25/06/2019 16:32 File SW1.MDX						Designed by Terry Seymour Checked by Terry Seymour						
Innovyze						Network 2017.1.2						
Network Design Table for SW-1.SWS												
PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	n	HYD SECT	DIA (mm)	Section Type	Auto Design
S1.003	36.592	0.113	323.8	0.079	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.004	12.233	0.030	407.8	0.095	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.005	8.977	0.022	408.0	0.007	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.006	18.565	0.046	403.6	0.007	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.007	31.963	0.079	404.6	0.041	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.008	13.143	0.032	410.7	0.080	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.009	6.866	0.017	403.9	0.000	0.00	0.0	0.600		o	450	Pipe/Conduit	
S1.010	43.627	0.087	501.5	0.000	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
S1.011	5.353	0.011	486.6	0.000	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
S1.012	17.096	0.034	502.8	0.000	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
S1.013	13.810	0.028	493.2	0.000	0.00	0.0		0.045	o	525	Pipe/Conduit	
S1.014	6.683	0.013	514.1	0.000	0.00	0.0		0.045	1 _ /	525	1:1 Ditch	
S1.015	4.615	0.009	512.8	0.000	0.00	0.0	0.600		o	525	Pipe/Conduit	
S1.016	27.468	0.055	499.4	0.000	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
S1.017	70.410	0.141	499.4	0.087	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
S5.000	37.874	0.223	169.8	0.067	5.00	0.0	0.600		o	225	Pipe/Conduit	
S5.001	13.335	0.078	171.0	0.039	0.00	0.0	0.600		o	225	Pipe/Conduit	
S5.002	15.006	0.088	170.5	0.000	0.00	0.0	0.600		o	225	Pipe/Conduit	
S5.003	47.205	0.193	244.6	0.085	0.00	0.0	0.600		o	300	Pipe/Conduit	
S6.000	46.917	0.456	102.9	0.137	5.00	0.0	0.600		o	300	Pipe/Conduit	
Network Results Table												
PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)		
S1.003	50.00	6.76	3.932	0.579		0.0	0.0	7.8	1.12	178.8	86.2	
S1.004	50.00	6.97	3.744	0.674		0.0	0.0	9.1	1.00	159.1	100.4	
S1.005	50.00	7.12	3.714	0.681		0.0	0.0	9.2	1.00	159.1	101.4	
S1.006	50.00	7.42	3.692	0.688		0.0	0.0	9.3	1.01	160.0	102.5	
S1.007	50.00	7.95	3.646	0.729		0.0	0.0	9.9	1.00	159.8	108.6	
S1.008	50.00	8.17	3.567	0.809		0.0	0.0	11.0	1.00	158.5	120.5	
S1.009	49.71	8.29	3.535	0.809		0.0	0.0	11.0	1.01	159.9	120.5	
S1.010	48.39	8.75	3.443	0.809		0.0	0.0	11.0	1.57	867.7	120.5	
S1.011	48.24	8.81	3.356	0.809		0.0	0.0	11.0	1.60	881.0	120.5	
S1.012	47.75	8.99	3.345	0.809		0.0	0.0	11.0	1.57	866.6	120.5	
S1.013	45.51	9.88	3.311	0.809		0.0	0.0	11.0	0.26	55.9	120.5	
S1.014	44.88	10.15	3.283	0.809		0.0	0.0	11.0	0.41	228.1	120.5	
S1.015	44.70	10.23	3.270	0.809		0.0	0.0	11.0	0.98	212.6	120.5	
S1.016	44.05	10.52	3.261	0.809		0.0	0.0	11.0	1.58	869.5	120.5	
S1.017	42.49	11.26	3.206	0.896		0.0	0.0	11.0	1.58	869.6	120.5	
S5.000	50.00	5.63	4.167	0.067		0.0	0.0	0.9	1.00	39.8	10.0	
S5.001	50.00	5.85	3.944	0.106		0.0	0.0	1.4	1.00	39.6	15.8	
S5.002	50.00	6.10	3.866	0.106		0.0	0.0	1.4	1.00	39.7	15.8	
S5.003	50.00	6.89	3.703	0.191		0.0	0.0	2.6	1.00	70.7	28.5	
S6.000	50.00	5.50	4.000	0.137		0.0	0.0	1.9	1.55	109.6	20.4	
©1982-2017 XP Solutions												

Rogers Cory Partnership											Page 2	
The Old School Old School Road Hook Hampshire RG27 9NJ						Summer Lane Pagham						
Date 25/06/2019 16:32 File SW1.MDX						Designed by Terry Seymour Checked by Terry Seymour						
Innovyze						Network 2017.1.2						
<u>Network Design Table for SW-1.SWS</u>												
PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	n	HYD SECT	DIA (mm)	Section Type	Auto Design
S5.004	37.876	0.117	323.7	0.114	0.00	0.0	0.600		o	375	Pipe/Conduit	
S5.005	18.226	0.045	405.0	0.183	0.00	0.0	0.600		o	450	Pipe/Conduit	
S5.006	10.518	0.027	389.6	0.000	0.00	0.0	0.600		o	450	Pipe/Conduit	
S7.000	13.486	0.079	170.7	0.020	5.00	0.0	0.600		o	225	Pipe/Conduit	
S7.001	18.636	0.110	169.4	0.062	0.00	0.0	0.600		o	225	Pipe/Conduit	
S7.002	13.429	0.143	93.9	0.026	0.00	0.0	0.600		o	225	Pipe/Conduit	
S5.007	15.587	0.031	502.8	0.000	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
S5.008	13.290	0.027	492.2	0.000	0.00	0.0	0.600		o	525	Pipe/Conduit	
S5.009	5.199	0.013	399.9	0.000	0.00	0.0	0.600		o	525	Pipe/Conduit	
S5.010	6.968	0.017	409.9	0.000	0.00	0.0	0.600		o	525	Pipe/Conduit	
S1.018	38.980	0.078	499.7	0.000	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
S1.019	48.609	0.111	437.9	0.000	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
S8.000	15.057	0.089	169.2	0.046	5.00	0.0	0.600		o	225	Pipe/Conduit	
S8.001	12.781	0.093	137.4	0.031	0.00	0.0	0.600		o	225	Pipe/Conduit	
S1.020	14.254	0.036	396.0	0.000	0.00	0.0	0.600	1 _ /		525	1:1 Ditch	
<u>Network Results Table</u>												
PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)		
S5.004	50.00	7.52	3.435	0.442	0.0	0.0	6.0	1.00	110.6	65.8		
S5.005	50.00	7.82	3.243	0.625	0.0	0.0	8.5	1.00	159.7	93.1		
S5.006	50.00	7.99	3.198	0.625	0.0	0.0	8.5	1.02	162.9	93.1		
S7.000	50.00	5.23	3.728	0.020	0.0	0.0	0.3	1.00	39.7	3.0		
S7.001	50.00	5.54	3.649	0.082	0.0	0.0	1.1	1.00	39.8	12.2		
S7.002	50.00	5.70	3.539	0.108	0.0	0.0	1.5	1.35	53.7	16.1		
S5.007	50.00	8.16	3.096	0.733	0.0	0.0	9.9	1.57	866.6	109.2		
S5.008	49.44	8.38	3.065	0.733	0.0	0.0	9.9	1.00	217.1	109.2		
S5.009	49.21	8.46	3.038	0.733	0.0	0.0	9.9	1.11	241.1	109.2		
S5.010	48.91	8.56	3.025	0.733	0.0	0.0	9.9	1.10	238.1	109.2		
S1.018	41.69	11.67	3.065	1.629	0.0	0.0	18.4	1.58	869.2	202.3		
S1.019	40.81	12.15	2.987	1.629	0.0	0.0	18.4	1.69	929.0	202.3		
S8.000	50.00	5.25	3.318	0.046	0.0	0.0	0.6	1.00	39.9	6.9		
S8.001	50.00	5.44	3.229	0.077	0.0	0.0	1.0	1.11	44.3	11.5		
S1.020	40.57	12.29	2.876	1.706	0.0	0.0	18.7	1.77	977.4	206.2		
©1982-2017 XP Solutions												

Rogers Cory Partnership											Page 3	
The Old School Old School Road Hook Hampshire RG27 9NJ						Summer Lane Pagham						
Date 25/06/2019 16:32						Designed by Terry Seymour						
File SW1.MDX						Checked by Terry Seymour						
Innovyze						Network 2017.1.2						

Network Design Table for SW-1.SWS

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	Base Flow (l/s)	k (mm)	n	HYD SECT	DIA (mm)	Section Type	Auto Design
S9.000	19.401	0.048	404.2	0.120	5.00	0.0		0.045	o	450	Pipe/Conduit	
S1.021	2.098	0.029	72.4	0.000	0.00	0.0		0.045	1 _ /	525	1:1 Ditch	
S1.022	27.502	0.006	4583.7	0.000	0.00	0.0		0.045	o	600	Pipe/Conduit	

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL Σ (m)	I.Area (ha)	Σ Base Flow (l/s)	Foul (l/s)	Add Flow (l/s)	Vel (m/s)	Cap (l/s)	Flow (l/s)
S9.000	50.00	6.26	3.467	0.120	0.0	0.0	1.6	0.26	41.0	17.9
S1.021	40.51	12.32	2.840	1.826	0.0	0.0	20.0	1.10	607.9	220.4
S1.022	33.57	17.26	2.803	1.826	0.0	0.0	20.0	0.09	26.2«	220.4

Simulation Criteria for SW-1.SWS

Volumetric Runoff Coeff	0.840	Additional Flow - % of Total Flow	10.000
Areal Reduction Factor	1.000	MADD Factor * 10m³/ha Storage	2.000
Hot Start (mins)	0	Inlet Coefficient	0.800
Hot Start Level (mm)	0	Flow per Person per Day (l/per/day)	0.000
Manhole Headloss Coeff (Global)	0.500	Run Time (mins)	2880
Foul Sewage per hectare (l/s)	0.000	Output Interval (mins)	24

Number of Input Hydrographs	0	Number of Storage Structures	4
Number of Online Controls	2	Number of Time/Area Diagrams	0
Number of Offline Controls	2	Number of Real Time Controls	0

Synthetic Rainfall Details

Rainfall Model	FSR	Profile Type	Winter
Return Period (years)	100	Cv (Summer)	0.750
Region	England and Wales	Cv (Winter)	0.840
M5-60 (mm)	19.000	Storm Duration (mins)	1440
Ratio R	0.350		

©1982-2017 XP Solutions

Rogers Cory Partnership		Page 4
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 16:32 File SW1.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		

Online Controls for SW-1.SWS

Hydro-Brake® Optimum Manhole: SW-10, DS/PN: S1.015, Volume (m³): 27.7

Unit Reference	MD-SHE-0192-2000-1500-2000
Design Head (m)	1.500
Design Flow (l/s)	20.0
Flush-Flo™	Calculated
Objective	Minimise upstream storage
Application	Surface
Sump Available	Yes
Diameter (mm)	192
Invert Level (m)	3.270
Minimum Outlet Pipe Diameter (mm)	225
Suggested Manhole Diameter (mm)	1500

Control Points	Head (m)	Flow (l/s)
Design Point (Calculated)	1.500	20.0
Flush-Flo™	0.452	20.0
Kick-Flo®	0.984	16.4
Mean Flow over Head Range	-	17.3

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)
0.100	6.7	1.200	18.0	3.000	27.8	7.000	41.9
0.200	17.7	1.400	19.3	3.500	30.0	7.500	43.3
0.300	19.4	1.600	20.6	4.000	32.0	8.000	44.7
0.400	19.9	1.800	21.8	4.500	33.8	8.500	46.0
0.500	20.0	2.000	22.9	5.000	35.6	9.000	47.3
0.600	19.7	2.200	24.0	5.500	37.3	9.500	48.6
0.800	18.8	2.400	25.0	6.000	38.9		
1.000	16.5	2.600	26.0	6.500	40.4		

Hydro-Brake® Optimum Manhole: SW-2, DS/PN: S1.022, Volume (m³): 8.0

Unit Reference	MD-SHE-0124-7900-1450-7900
Design Head (m)	1.450
Design Flow (l/s)	7.9
Flush-Flo™	Calculated
Objective	Minimise upstream storage
Application	Surface
Sump Available	Yes
Diameter (mm)	124
Invert Level (m)	2.803
Minimum Outlet Pipe Diameter (mm)	150
Suggested Manhole Diameter (mm)	1200

©1982-2017 XP Solutions

Rogers Cory Partnership		Page 6
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 16:32 File SW1.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		
<u>Offline Controls for SW-1.SWS</u> <u>Weir Manhole: SW-10, DS/PN: S1.015, Loop to PN: S1.016</u> Discharge Coef 0.544 Width (m) 1.500 Invert Level (m) 4.500 <u>Weir Manhole: SW-2, DS/PN: S1.022, Loop to PN: None</u> Discharge Coef 0.544 Width (m) 10.000 Invert Level (m) 5.050		
©1982-2017 XP Solutions		

Rogers Cory Partnership		Page 7
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 16:32 File SW1.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze Network 2017.1.2		

Storage Structures for SW-1.SWS

Porous Car Park Manhole: SW-25, DS/PN: S1.000

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	5.5
Membrane Percolation (mm/hr)	1000	Length (m)	51.0
Max Percolation (l/s)	77.9	Slope (1:X)	100.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	4.412	Cap Volume Depth (m)	0.600

Porous Car Park Manhole: SW-18, DS/PN: S1.007

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	10.0
Membrane Percolation (mm/hr)	1000	Length (m)	10.0
Max Percolation (l/s)	27.8	Slope (1:X)	500.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	4.333	Cap Volume Depth (m)	0.450

Tank or Pond Manhole: SW-12, DS/PN: S1.013

Invert Level (m) 4.200

Depth (m)	Area (m ²)	Depth (m)	Area (m ²)
0.000	153.3	1.000	353.2

Tank or Pond Manhole: SW-31, DS/PN: S5.008

Invert Level (m) 4.200

Depth (m)	Area (m ²)	Depth (m)	Area (m ²)
0.000	130.1	0.700	311.4

©1982-2017 XP Solutions

Rogers Cory Partnership								Page 8	
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>									
<u>Simulation Criteria</u>									
Areal Reduction Factor		1.000	Additional Flow - % of Total Flow		10.000				
Hot Start (mins)		0	MADD Factor * 10m³/ha Storage		2.000				
Hot Start Level (mm)		0	Inlet Coeffiecient		0.800				
Manhole Headloss Coeff (Global)		0.500	Flow per Person per Day (l/per/day)		0.000				
Foul Sewage per hectare (l/s)		0.000							
Number of Input Hydrographs		0	Number of Storage Structures		4				
Number of Online Controls		2	Number of Time/Area Diagrams		0				
Number of Offline Controls		2	Number of Real Time Controls		0				
<u>Synthetic Rainfall Details</u>									
Rainfall Model		FSR		Ratio R		0.350			
Region England and Wales Cv (Summer)		0.750							
M5-60 (mm)		19.000 Cv (Winter)		0.840					
Margin for Flood Risk Warning (mm)		300.0							
Analysis Timestep		2.5 Second Increment (Extended)							
DTS Status		OFF							
DVD Status		ON							
Inertia Status		ON							
Profile(s)		Summer and Winter							
Duration(s) (mins)		15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080							
Return Period(s) (years)		1, 30, 100							
Climate Change (%)		0, 0, 40							
	US/MH		Return	Climate	First (X)	First (Y)	First (Z)	Overflow	Water
PN	Name	Storm	Period	Change	Surcharge	Flood	Overflow	Act.	Level
									(m)
S1.000	SW-25	15 Winter	1	+0%	100/15 Summer				4.512
S2.000	SW-26	15 Winter	1	+0%	100/15 Summer				4.675
S1.001	SW-24	15 Winter	1	+0%	100/15 Summer				4.449
S1.002	SW-23	15 Winter	1	+0%	30/15 Winter				4.331
S3.000	SW-27	15 Winter	1	+0%	100/15 Summer				4.522
S4.000	SW-28	15 Winter	1	+0%	30/15 Winter				4.371
S1.003	SW-22	4320 Winter	1	+0%	30/15 Summer				4.277
S1.004	SW-21	4320 Winter	1	+0%	1/960 Winter				4.276
S1.005	SW-20	4320 Winter	1	+0%	1/600 Winter				4.275
S1.006	SW-19	4320 Winter	1	+0%	1/600 Winter				4.275
S1.007	SW-18	4320 Winter	1	+0%	1/480 Winter				4.274
S1.008	SW-17	4320 Winter	1	+0%	1/240 Winter				4.274
S1.009	SW-16	4320 Winter	1	+0%	1/180 Winter				4.273
S1.010	SW-15	4320 Winter	1	+0%					4.272
S1.011	SW-14	4320 Winter	1	+0%					4.272
S1.012	SW-13	4320 Winter	1	+0%					4.272
S1.013	SW-12	4320 Winter	1	+0%	1/15 Winter				4.272
©1982-2017 XP Solutions									

Rogers Cory Partnership						Page 9		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham				
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour				
Innovyze				Network 2017.1.2				
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>								
PN	US/MH Name	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S1.000	SW-25	-0.200	0.000	0.23		18.1	OK	
S2.000	SW-26	-0.164	0.000	0.16		10.8	OK	
S1.001	SW-24	-0.235	0.000	0.30		33.9	OK	
S1.002	SW-23	-0.206	0.000	0.41		44.1	OK	
S3.000	SW-27	-0.148	0.000	0.25		9.1	OK	
S4.000	SW-28	-0.154	0.000	0.21		7.8	OK	
S1.003	SW-22	-0.105	0.000	0.02		2.5	OK	
S1.004	SW-21	0.082	0.000	0.03		2.9	SURCHARGED	
S1.005	SW-20	0.111	0.000	0.03		2.9	SURCHARGED	
S1.006	SW-19	0.133	0.000	0.02		3.0	SURCHARGED	
S1.007	SW-18	0.178	0.000	0.02		3.1	SURCHARGED	
S1.008	SW-17	0.257	0.000	0.03		3.4	SURCHARGED	
S1.009	SW-16	0.288	0.000	0.03		3.4	SURCHARGED	
S1.010	SW-15	-0.928	0.000	0.00		3.3	OK	
S1.011	SW-14	-0.928	0.000	0.00		2.8	OK	
S1.012	SW-13	-0.928	0.000	0.00		2.8	OK	
S1.013	SW-12	0.436	0.000	0.05		2.1	SURCHARGED	
©1982-2017 XP Solutions								

Rogers Cory Partnership						Page 10			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>									
PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surcharge	First (Y) Flood	First (Z) Overflow		
S1.014	SW-11	4320 Winter	1	+0%					
S1.015	SW-10	4320 Winter	1	+0%	1/15 Summer		30/360 Winter		
S1.016	SW-9	4320 Winter	1	+0%					
S1.017	SW-8	4320 Winter	1	+0%					
S5.000	SW-39	15 Winter	1	+0%	30/360 Winter	100/15 Summer			
S5.001	SW-38	4320 Winter	1	+0%	1/960 Winter	100/15 Winter			
S5.002	SW-37	4320 Winter	1	+0%	1/480 Winter				
S5.003	SW-36	4320 Winter	1	+0%	1/360 Summer				
S6.000	S26	4320 Winter	1	+0%	30/180 Winter				
S5.004	SW-35	4320 Winter	1	+0%	1/120 Summer				
S5.005	SW-34	4320 Winter	1	+0%	1/60 Summer				
S5.006	SW-33	4320 Winter	1	+0%	1/30 Winter				
S7.000	SW-42	4320 Winter	1	+0%	1/240 Winter				
S7.001	SW-41	4320 Winter	1	+0%	1/120 Winter				
S7.002	SW-40	4320 Winter	1	+0%	1/60 Winter				
S5.007	SW-32	4320 Winter	1	+0%					
S5.008	SW-31	4320 Winter	1	+0%	1/15 Winter				
S5.009	SW-30	4320 Winter	1	+0%	1/15 Summer				
S5.010	SW-29	4320 Winter	1	+0%	1/15 Summer				
S1.018	SW-7	4320 Winter	1	+0%					
S1.019	SW-6	4320 Winter	1	+0%					
S8.000	SW-44	4320 Winter	1	+0%	1/15 Summer				
S8.001	SW-43	4320 Winter	1	+0%	1/15 Summer				
S1.020	SW-5	4320 Winter	1	+0%					
S9.000	SW-45	4320 Winter	1	+0%	1/180 Winter				
S1.021	SW-4	4320 Winter	1	+0%					
S1.022	SW-2	4320 Winter	1	+0%	1/15 Summer				
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Pipe Flow / Overflow Cap.	Pipe Flow (l/s)	Status	Level Exceeded
S1.014	SW-11		4.271	-0.929	0.000	0.00	2.1	OK	
S1.015	SW-10	49	4.271	0.476	0.000	0.01	0.0	SURCHARGED	
S1.016	SW-9		4.235	-0.865	0.000	0.00	2.1	OK	
S1.017	SW-8		4.235	-0.865	0.000	0.00	2.3	OK	
S5.000	SW-39		4.243	-0.149	0.000	0.24	9.1	OK	4
S5.001	SW-38		4.239	0.070	0.000	0.01	0.4	SURCHARGED	1
S5.002	SW-37		4.238	0.147	0.000	0.01	0.4	SURCHARGED	
S5.003	SW-36		4.238	0.235	0.000	0.01	0.7	SURCHARGED	
S6.000	S26		4.238	-0.062	0.000	0.01	0.6	OK	
S5.004	SW-35		4.238	0.428	0.000	0.02	1.7	SURCHARGED	
S5.005	SW-34		4.237	0.544	0.000	0.02	2.4	SURCHARGED	
S5.006	SW-33		4.237	0.589	0.000	0.02	2.4	SURCHARGED	
S7.000	SW-42		4.237	0.284	0.000	0.00	0.1	SURCHARGED	
S7.001	SW-41		4.237	0.363	0.000	0.01	0.3	SURCHARGED	
S7.002	SW-40		4.237	0.473	0.000	0.01	0.4	SURCHARGED	
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 11		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham						
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour						
Innovyze				Network 2017.1.2						
<u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>										
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S5.007	SW-32		4.236	-0.964	0.000	0.00		2.9	OK	
S5.008	SW-31		4.236	0.646	0.000	0.02		2.7	SURCHARGED	
S5.009	SW-30		4.236	0.673	0.000	0.02		2.7	SURCHARGED	
S5.010	SW-29		4.236	0.686	0.000	0.02		2.7	SURCHARGED	
S1.018	SW-7		4.235	-0.865	0.000	0.00		4.2	OK	
S1.019	SW-6		4.235	-0.865	0.000	0.00		4.2	OK	
S8.000	SW-44		4.235	0.692	0.000	0.01		0.2	SURCHARGED	
S8.001	SW-43		4.235	0.781	0.000	0.01		0.4	SURCHARGED	
S1.020	SW-5		4.235	-0.865	0.000	0.00		10.9	OK	
S9.000	SW-45		4.234	0.317	0.000	0.02		0.8	SURCHARGED	
S1.021	SW-4		4.239	-0.861	0.000	0.00		11.7	OK	
S1.022	SW-2	0	4.242	0.839	0.000	0.11	0.0	4.6	SURCHARGED	
©1982-2017 XP Solutions										

Rogers Cory Partnership										Page 12
The Old School Old School Road Hook Hampshire RG27 9NJ					Summer Lane Pagham					
Date 25/06/2019 16:32 File SW1.MDX					Designed by Terry Seymour Checked by Terry Seymour					
Innovyze					Network 2017.1.2					
<u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>										
<u>Simulation Criteria</u>										
Areal Reduction Factor 1.000 Additional Flow - % of Total Flow 10.000										
Hot Start (mins) 0 MADD Factor * 10m³/ha Storage 2.000										
Hot Start Level (mm) 0 Inlet Coeffiecient 0.800										
Manhole Headloss Coeff (Global) 0.500 Flow per Person per Day (l/per/day) 0.000										
Foul Sewage per hectare (l/s) 0.000										
Number of Input Hydrographs 0 Number of Storage Structures 4										
Number of Online Controls 2 Number of Time/Area Diagrams 0										
Number of Offline Controls 2 Number of Real Time Controls 0										
<u>Synthetic Rainfall Details</u>										
Rainfall Model FSR Ratio R 0.350										
Region England and Wales Cv (Summer) 0.750										
M5-60 (mm) 19.000 Cv (Winter) 0.840										
Margin for Flood Risk Warning (mm) 300.0										
Analysis Timestep 2.5 Second Increment (Extended)										
DTS Status OFF										
DVD Status ON										
Inertia Status ON										
Profile(s) Summer and Winter										
Duration(s) (mins) 15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080										
Return Period(s) (years) 1, 30, 100										
Climate Change (%) 0, 0, 40										

Rogers Cory Partnership						Page 13	
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham			
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour			
Innovyze				Network 2017.1.2			
<u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>							

Rogers Cory Partnership		Page 14
The Old School Old School Road Hook Hampshire RG27 9NJ	Summer Lane Pagham	
Date 25/06/2019 16:32 File SW1.MDX	Designed by Terry Seymour Checked by Terry Seymour	
Innovyze	Network 2017.1.2	

30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)
for SW-1.SWS

PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surchage	First (Y) Flood	First (Z) Overflow
S1.014	SW-11	2160 Winter	30	+0%			
S1.015	SW-10	2160 Winter	30	+0%	1/15 Summer		30/360 Winter
S1.016	SW-9	2160 Winter	30	+0%			
S1.017	SW-8	2160 Winter	30	+0%			
S5.000	SW-39	2160 Winter	30	+0%	30/360 Winter	100/15 Summer	
S5.001	SW-38	2160 Winter	30	+0%	1/960 Winter	100/15 Winter	
S5.002	SW-37	2160 Winter	30	+0%	1/480 Winter		
S5.003	SW-36	2160 Winter	30	+0%	1/360 Summer		
S6.000	S26	2160 Winter	30	+0%	30/180 Winter		
S5.004	SW-35	2160 Winter	30	+0%	1/120 Summer		
S5.005	SW-34	2160 Winter	30	+0%	1/60 Summer		
S5.006	SW-33	2160 Winter	30	+0%	1/30 Winter		
S7.000	SW-42	2160 Winter	30	+0%	1/240 Winter		
S7.001	SW-41	2160 Winter	30	+0%	1/120 Winter		
S7.002	SW-40	2160 Winter	30	+0%	1/60 Winter		
S5.007	SW-32	2160 Winter	30	+0%			
S5.008	SW-31	2160 Winter	30	+0%	1/15 Winter		
S5.009	SW-30	2160 Winter	30	+0%	1/15 Summer		
S5.010	SW-29	2160 Winter	30	+0%	1/15 Summer		
S1.018	SW-7	2160 Winter	30	+0%			
S1.019	SW-6	2160 Winter	30	+0%			
S8.000	SW-44	2160 Winter	30	+0%	1/15 Summer		
S8.001	SW-43	2160 Winter	30	+0%	1/15 Summer		
S1.020	SW-5	2160 Winter	30	+0%			
S9.000	SW-45	2160 Winter	30	+0%	1/180 Winter		
S1.021	SW-4	2160 Winter	30	+0%			
S1.022	SW-2	2160 Winter	30	+0%	1/15 Summer		

PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Pipe Flow / Overflow Cap. (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S1.014	SW-11		4.539	-0.661	0.000	0.00	6.4	OK	
S1.015	SW-10	49	4.539	0.744	0.000	0.03	4.2	SURCHARGED	
S1.016	SW-9		4.521	-0.579	0.000	0.00	6.4	OK	
S1.017	SW-8		4.521	-0.579	0.000	0.00	6.6	OK	
S5.000	SW-39		4.529	0.137	0.000	0.02	0.9	SURCHARGED	4
S5.001	SW-38		4.528	0.359	0.000	0.04	1.4	SURCHARGED	1
S5.002	SW-37		4.527	0.436	0.000	0.04	1.3	SURCHARGED	
S5.003	SW-36		4.526	0.523	0.000	0.04	2.5	SURCHARGED	
S6.000	S26		4.526	0.226	0.000	0.02	1.9	SURCHARGED	
S5.004	SW-35		4.525	0.715	0.000	0.06	5.8	SURCHARGED	
S5.005	SW-34		4.523	0.830	0.000	0.07	8.3	SURCHARGED	
S5.006	SW-33		4.522	0.874	0.000	0.08	8.2	SURCHARGED	
S7.000	SW-42		4.523	0.570	0.000	0.01	0.3	SURCHARGED	
S7.001	SW-41		4.523	0.649	0.000	0.03	1.1	SURCHARGED	
S7.002	SW-40		4.523	0.759	0.000	0.03	1.4	SURCHARGED	

©1982-2017 XP Solutions

Rogers Cory Partnership								Page 15		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham						
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour						
Innovyze				Network 2017.1.2						
<u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u> <u>for SW-1.SWS</u>										
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S5.007	SW-32		4.522	-0.678	0.000	0.00		9.6	OK	
S5.008	SW-31		4.522	0.932	0.000	0.06		7.5	SURCHARGED	
S5.009	SW-30		4.521	0.958	0.000	0.05		7.5	SURCHARGED	
S5.010	SW-29		4.521	0.971	0.000	0.05		7.5	SURCHARGED	
S1.018	SW-7		4.520	-0.580	0.000	0.00		9.3	OK	
S1.019	SW-6		4.519	-0.581	0.000	0.00		8.4	OK	
S8.000	SW-44		4.519	0.976	0.000	0.02		0.6	SURCHARGED	
S8.001	SW-43		4.519	1.065	0.000	0.03		1.0	SURCHARGED	
S1.020	SW-5		4.519	-0.581	0.000	0.00		11.2	OK	
S9.000	SW-45		4.519	0.602	0.000	0.05		1.8	SURCHARGED	
S1.021	SW-4		4.521	-0.579	0.000	0.00		13.3	OK	
S1.022	SW-2	0	4.528	1.125	0.000	0.19	0.0	7.9	SURCHARGED	
©1982-2017 XP Solutions										

Rogers Cory Partnership								Page 16																																																																																																																																																																																																									
The Old School Old School Road Hook Hampshire RG27 9NJ					Summer Lane Pagham																																																																																																																																																																																																												
Date 25/06/2019 16:32 File SW1.MDX					Designed by Terry Seymour Checked by Terry Seymour																																																																																																																																																																																																												
Innovyze					Network 2017.1.2																																																																																																																																																																																																												
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>																																																																																																																																																																																																																	
<u>Simulation Criteria</u>																																																																																																																																																																																																																	
Areal Reduction Factor		1.000		Additional Flow - % of Total Flow		10.000																																																																																																																																																																																																											
Hot Start (mins)		0		MADD Factor * 10m³/ha Storage		2.000																																																																																																																																																																																																											
Hot Start Level (mm)		0		Inlet Coeffiecient		0.800																																																																																																																																																																																																											
Manhole Headloss Coeff (Global)		0.500		Flow per Person per Day (l/per/day)		0.000																																																																																																																																																																																																											
Foul Sewage per hectare (l/s)		0.000																																																																																																																																																																																																															
Number of Input Hydrographs		0		Number of Storage Structures		4																																																																																																																																																																																																											
Number of Online Controls		2		Number of Time/Area Diagrams		0																																																																																																																																																																																																											
Number of Offline Controls		2		Number of Real Time Controls		0																																																																																																																																																																																																											
<u>Synthetic Rainfall Details</u>																																																																																																																																																																																																																	
Rainfall Model		FSR		Ratio R		0.350																																																																																																																																																																																																											
Region England and Wales Cv (Summer)		0.750																																																																																																																																																																																																															
M5-60 (mm)		19.000		Cv (Winter)		0.840																																																																																																																																																																																																											
Margin for Flood Risk Warning (mm)		300.0																																																																																																																																																																																																															
Analysis Timestep		2.5 Second Increment (Extended)																																																																																																																																																																																																															
DTS Status		OFF																																																																																																																																																																																																															
DVD Status		ON																																																																																																																																																																																																															
Inertia Status		ON																																																																																																																																																																																																															
Profile(s)		Summer and Winter																																																																																																																																																																																																															
Duration(s) (mins)		15, 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440, 2160, 2880, 4320, 5760, 7200, 8640, 10080																																																																																																																																																																																																															
Return Period(s) (years)		1, 30, 100																																																																																																																																																																																																															
Climate Change (%)		0, 0, 40																																																																																																																																																																																																															
<table><tr><th></th><th>US/MH</th><th></th><th>Return</th><th>Climate</th><th>First (X)</th><th>First (Y)</th><th>First (Z)</th><th>Overflow</th><th>Water</th></tr><tr><th>PN</th><th>Name</th><th>Storm</th><th>Period</th><th>Change</th><th>Surcharge</th><th>Flood</th><th>Overflow</th><th>Act.</th><th>Level</th></tr><tr><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>(m)</th></tr><tr><td>S1.000</td><td>SW-25</td><td>30 Winter</td><td>100</td><td>+40%</td><td>100/15 Summer</td><td></td><td></td><td></td><td>5.202</td></tr><tr><td>S2.000</td><td>SW-26</td><td>15 Winter</td><td>100</td><td>+40%</td><td>100/15 Summer</td><td></td><td></td><td></td><td>5.341</td></tr><tr><td>S1.001</td><td>SW-24</td><td>15 Winter</td><td>100</td><td>+40%</td><td>100/15 Summer</td><td></td><td></td><td></td><td>5.188</td></tr><tr><td>S1.002</td><td>SW-23</td><td>15 Winter</td><td>100</td><td>+40%</td><td>30/15 Winter</td><td></td><td></td><td></td><td>5.193</td></tr><tr><td>S3.000</td><td>SW-27</td><td>15 Winter</td><td>100</td><td>+40%</td><td>100/15 Summer</td><td></td><td></td><td></td><td>5.253</td></tr><tr><td>S4.000</td><td>SW-28</td><td>15 Winter</td><td>100</td><td>+40%</td><td>30/15 Winter</td><td></td><td></td><td></td><td>5.217</td></tr><tr><td>S1.003</td><td>SW-22</td><td>15 Winter</td><td>100</td><td>+40%</td><td>30/15 Summer</td><td></td><td></td><td></td><td>5.102</td></tr><tr><td>S1.004</td><td>SW-21</td><td>2160 Winter</td><td>100</td><td>+40%</td><td>1/960 Winter</td><td></td><td></td><td></td><td>5.036</td></tr><tr><td>S1.005</td><td>SW-20</td><td>2160 Winter</td><td>100</td><td>+40%</td><td>1/600 Winter</td><td></td><td></td><td></td><td>5.035</td></tr><tr><td>S1.006</td><td>SW-19</td><td>2160 Winter</td><td>100</td><td>+40%</td><td>1/600 Winter</td><td></td><td></td><td></td><td>5.034</td></tr><tr><td>S1.007</td><td>SW-18</td><td>2160 Winter</td><td>100</td><td>+40%</td><td>1/480 Winter</td><td></td><td></td><td></td><td>5.033</td></tr><tr><td>S1.008</td><td>SW-17</td><td>2160 Winter</td><td>100</td><td>+40%</td><td>1/240 Winter</td><td></td><td></td><td></td><td>5.032</td></tr><tr><td>S1.009</td><td>SW-16</td><td>2160 Winter</td><td>100</td><td>+40%</td><td>1/180 Winter</td><td></td><td></td><td></td><td>5.031</td></tr><tr><td>S1.010</td><td>SW-15</td><td>2160 Winter</td><td>100</td><td>+40%</td><td></td><td></td><td></td><td></td><td>5.030</td></tr><tr><td>S1.011</td><td>SW-14</td><td>2160 Winter</td><td>100</td><td>+40%</td><td></td><td></td><td></td><td></td><td>5.030</td></tr><tr><td>S1.012</td><td>SW-13</td><td>2160 Winter</td><td>100</td><td>+40%</td><td></td><td></td><td></td><td></td><td>5.029</td></tr><tr><td>S1.013</td><td>SW-12</td><td>2160 Winter</td><td>100</td><td>+40%</td><td>1/15 Winter</td><td></td><td></td><td></td><td>5.029</td></tr></table>											US/MH		Return	Climate	First (X)	First (Y)	First (Z)	Overflow	Water	PN	Name	Storm	Period	Change	Surcharge	Flood	Overflow	Act.	Level										(m)	S1.000	SW-25	30 Winter	100	+40%	100/15 Summer				5.202	S2.000	SW-26	15 Winter	100	+40%	100/15 Summer				5.341	S1.001	SW-24	15 Winter	100	+40%	100/15 Summer				5.188	S1.002	SW-23	15 Winter	100	+40%	30/15 Winter				5.193	S3.000	SW-27	15 Winter	100	+40%	100/15 Summer				5.253	S4.000	SW-28	15 Winter	100	+40%	30/15 Winter				5.217	S1.003	SW-22	15 Winter	100	+40%	30/15 Summer				5.102	S1.004	SW-21	2160 Winter	100	+40%	1/960 Winter				5.036	S1.005	SW-20	2160 Winter	100	+40%	1/600 Winter				5.035	S1.006	SW-19	2160 Winter	100	+40%	1/600 Winter				5.034	S1.007	SW-18	2160 Winter	100	+40%	1/480 Winter				5.033	S1.008	SW-17	2160 Winter	100	+40%	1/240 Winter				5.032	S1.009	SW-16	2160 Winter	100	+40%	1/180 Winter				5.031	S1.010	SW-15	2160 Winter	100	+40%					5.030	S1.011	SW-14	2160 Winter	100	+40%					5.030	S1.012	SW-13	2160 Winter	100	+40%					5.029	S1.013	SW-12	2160 Winter	100	+40%	1/15 Winter				5.029
	US/MH		Return	Climate	First (X)	First (Y)	First (Z)	Overflow	Water																																																																																																																																																																																																								
PN	Name	Storm	Period	Change	Surcharge	Flood	Overflow	Act.	Level																																																																																																																																																																																																								
									(m)																																																																																																																																																																																																								
S1.000	SW-25	30 Winter	100	+40%	100/15 Summer				5.202																																																																																																																																																																																																								
S2.000	SW-26	15 Winter	100	+40%	100/15 Summer				5.341																																																																																																																																																																																																								
S1.001	SW-24	15 Winter	100	+40%	100/15 Summer				5.188																																																																																																																																																																																																								
S1.002	SW-23	15 Winter	100	+40%	30/15 Winter				5.193																																																																																																																																																																																																								
S3.000	SW-27	15 Winter	100	+40%	100/15 Summer				5.253																																																																																																																																																																																																								
S4.000	SW-28	15 Winter	100	+40%	30/15 Winter				5.217																																																																																																																																																																																																								
S1.003	SW-22	15 Winter	100	+40%	30/15 Summer				5.102																																																																																																																																																																																																								
S1.004	SW-21	2160 Winter	100	+40%	1/960 Winter				5.036																																																																																																																																																																																																								
S1.005	SW-20	2160 Winter	100	+40%	1/600 Winter				5.035																																																																																																																																																																																																								
S1.006	SW-19	2160 Winter	100	+40%	1/600 Winter				5.034																																																																																																																																																																																																								
S1.007	SW-18	2160 Winter	100	+40%	1/480 Winter				5.033																																																																																																																																																																																																								
S1.008	SW-17	2160 Winter	100	+40%	1/240 Winter				5.032																																																																																																																																																																																																								
S1.009	SW-16	2160 Winter	100	+40%	1/180 Winter				5.031																																																																																																																																																																																																								
S1.010	SW-15	2160 Winter	100	+40%					5.030																																																																																																																																																																																																								
S1.011	SW-14	2160 Winter	100	+40%					5.030																																																																																																																																																																																																								
S1.012	SW-13	2160 Winter	100	+40%					5.029																																																																																																																																																																																																								
S1.013	SW-12	2160 Winter	100	+40%	1/15 Winter				5.029																																																																																																																																																																																																								
©1982-2017 XP Solutions																																																																																																																																																																																																																	

Rogers Cory Partnership						Page 17		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham				
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour				
Innovyze				Network 2017.1.2				
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>								
PN	US/MH Name	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S1.000	SW-25	0.490	0.000	0.45		35.2	FLOOD RISK	
S2.000	SW-26	0.502	0.000	0.66		43.7	FLOOD RISK	
S1.001	SW-24	0.504	0.000	0.66		75.4	SURCHARGED	
S1.002	SW-23	0.656	0.000	0.97		103.0	SURCHARGED	
S3.000	SW-27	0.583	0.000	1.03		37.7	FLOOD RISK	
S4.000	SW-28	0.692	0.000	0.89		32.5	FLOOD RISK	
S1.003	SW-22	0.720	0.000	1.09		172.3	SURCHARGED	
S1.004	SW-21	0.842	0.000	0.16		15.6	SURCHARGED	
S1.005	SW-20	0.871	0.000	0.17		15.7	FLOOD RISK	
S1.006	SW-19	0.892	0.000	0.13		15.8	FLOOD RISK	
S1.007	SW-18	0.937	0.000	0.11		15.8	FLOOD RISK	
S1.008	SW-17	1.015	0.000	0.18		17.7	SURCHARGED	
S1.009	SW-16	1.046	0.000	0.17		17.6	SURCHARGED	
S1.010	SW-15	-0.170	0.000	0.00		17.6	FLOOD RISK	
S1.011	SW-14	-0.170	0.000	0.00		16.1	FLOOD RISK	
S1.012	SW-13	-0.171	0.000	0.00		16.0	FLOOD RISK	
S1.013	SW-12	1.193	0.000	0.32		13.7	FLOOD RISK	
©1982-2017 XP Solutions								

Rogers Cory Partnership						Page 18			
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham					
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour					
Innovyze				Network 2017.1.2					
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>									
PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surcharge	First (Y) Flood	First (Z) Overflow		
S1.014	SW-11	2160 Winter	100	+40%					
S1.015	SW-10	2160 Winter	100	+40%	1/15 Summer		30/360 Winter		
S1.016	SW-9	2160 Winter	100	+40%					
S1.017	SW-8	2160 Winter	100	+40%					
S5.000	SW-39	15 Winter	100	+40%	30/360 Winter	100/15 Summer			
S5.001	SW-38	15 Winter	100	+40%	1/960 Winter	100/15 Winter			
S5.002	SW-37	15 Winter	100	+40%	1/480 Winter				
S5.003	SW-36	15 Winter	100	+40%	1/360 Summer				
S6.000	S26	15 Winter	100	+40%	30/180 Winter				
S5.004	SW-35	2160 Winter	100	+40%	1/120 Summer				
S5.005	SW-34	2160 Winter	100	+40%	1/60 Summer				
S5.006	SW-33	2160 Winter	100	+40%	1/30 Winter				
S7.000	SW-42	2160 Winter	100	+40%	1/240 Winter				
S7.001	SW-41	2160 Winter	100	+40%	1/120 Winter				
S7.002	SW-40	2160 Winter	100	+40%	1/60 Winter				
S5.007	SW-32	2160 Winter	100	+40%					
S5.008	SW-31	2160 Winter	100	+40%	1/15 Winter				
S5.009	SW-30	2160 Winter	100	+40%	1/15 Summer				
S5.010	SW-29	2160 Winter	100	+40%	1/15 Summer				
S1.018	SW-7	2160 Winter	100	+40%					
S1.019	SW-6	2160 Winter	100	+40%					
S8.000	SW-44	2160 Winter	100	+40%	1/15 Summer				
S8.001	SW-43	2160 Winter	100	+40%	1/15 Summer				
S1.020	SW-5	2160 Winter	100	+40%					
S9.000	SW-45	2160 Winter	100	+40%	1/180 Winter				
S1.021	SW-4	2160 Winter	100	+40%					
S1.022	SW-2	2160 Winter	100	+40%	1/15 Summer				
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Pipe Flow / Overflow Cap.	Pipe Flow (l/s)	Status	Level Exceeded
S1.014	SW-11		5.027	-0.173	0.000	0.00	13.7	FLOOD RISK	
S1.015	SW-10	49	5.027	1.232	0.000	0.03	10.9	5.0 FLOOD RISK	
S1.016	SW-9		5.023	-0.077	0.000	0.00	13.5	FLOOD RISK	
S1.017	SW-8		5.023	-0.077	0.000	0.00	13.0	FLOOD RISK	
S5.000	SW-39		5.204	0.812	4.038	1.11	41.9	FLOOD	4
S5.001	SW-38		5.200	1.031	0.066	1.42	48.8	FLOOD	1
S5.002	SW-37		5.178	1.087	0.000	1.42	49.7	FLOOD RISK	
S5.003	SW-36		5.120	1.117	0.000	1.07	70.9	FLOOD RISK	
S6.000	S26		5.081	0.781	0.000	0.67	69.0	FLOOD RISK	
S5.004	SW-35		5.025	1.215	0.000	0.10	10.2	FLOOD RISK	
S5.005	SW-34		5.023	1.330	0.000	0.12	14.5	FLOOD RISK	
S5.006	SW-33		5.023	1.375	0.000	0.14	14.5	FLOOD RISK	
S7.000	SW-42		5.023	1.070	0.000	0.01	0.4	FLOOD RISK	
S7.001	SW-41		5.023	1.149	0.000	0.05	1.9	FLOOD RISK	
S7.002	SW-40		5.023	1.259	0.000	0.05	2.5	FLOOD RISK	
©1982-2017 XP Solutions									

Rogers Cory Partnership								Page 19		
The Old School Old School Road Hook Hampshire RG27 9NJ				Summer Lane Pagham						
Date 25/06/2019 16:32 File SW1.MDX				Designed by Terry Seymour Checked by Terry Seymour						
Innovyze				Network 2017.1.2						
<u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for SW-1.SWS</u>										
PN	US/MH Name	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)	Status	Level Exceeded
S5.007	SW-32		5.022	-0.178	0.000	0.00		16.9	FLOOD RISK	
S5.008	SW-31		5.022	1.432	0.000	0.09		10.3	FLOOD RISK	
S5.009	SW-30		5.021	1.458	0.000	0.06		10.3	FLOOD RISK	
S5.010	SW-29		5.021	1.471	0.000	0.07		10.2	FLOOD RISK	
S1.018	SW-7		5.020	-0.080	0.000	0.00		14.2	FLOOD RISK	
S1.019	SW-6		5.016	-0.084	0.000	0.00		10.7	FLOOD RISK	
S8.000	SW-44		5.011	1.468	0.000	0.03		1.1	FLOOD RISK	
S8.001	SW-43		5.011	1.557	0.000	0.05		1.8	FLOOD RISK	
S1.020	SW-5		5.011	-0.089	0.000	0.00		11.0	FLOOD RISK	
S9.000	SW-45		5.009	1.092	0.000	0.08		3.0	FLOOD RISK	
S1.021	SW-4		5.009	-0.091	0.000	0.00		13.4	FLOOD RISK	
S1.022	SW-2	0	5.004	1.601	0.000	0.19	0.0	7.9	FLOOD RISK	
©1982-2017 XP Solutions										

Appendix (G)

SuDS Maintenance Strategy

Land North of Summer Lane

Pagham, West Sussex

OWNERS MANUAL

Relating to Surface Water Drainage Maintenance

The site has been designed in accordance with Sustainable Drainage Systems (SuDS) techniques.

An extract from the SuDS Manual (CIRIA C753) states “Sedimentation is one of the primary removal mechanisms in SUDS. Most pollution in runoff is attached to sediment particles and therefore removal of sediment results in a significant reduction in pollutant loads..”.

In order to remove sedimentation the surface water drainage design utilises deep seal trapped gullies throughout, catchpit manholes upstream of the surface water granular filter drains and bio-retention areas in attenuation ponds.

CONTENTS

- 1) Explanation of the Surface Water Drainage System
- 2) Operating and Maintenance Responsibility
- 3) Maintenance Schedule for catchpits, control chambers, flow control devices and gullies
- 4) Maintenance of permeable paving and distribution tanks
- 5) Maintenance Schedule for attenuation basins, bioretention areas and swales
- 6) Maintenance Schedule for filter trenches and porous pipework
- 7) Maintenance Schedule for solid wall pipes
- 8) Reasons for Maintenance

1) Explanation of the Surface Water Drainage System

The Principle of SUDs has been adopted for the whole of the site, calculations have been carried out using MicroDrainage with a storm return period of 100 years and an allowance of 40% for climate change and 10% allowance for urban creep.

Generally roof water drains direct to the domestic drainage system within each curtilage and from there will be directed to the below ground surface water network

Hardstanding areas and access roads or drives, drain to trapped gullies. Parking bays constructed of permeable paving will drain to ground, but will also contain an overflow provision which connects to the new below ground surface water network. All of these systems outfall to the surface water drainage system within the site.

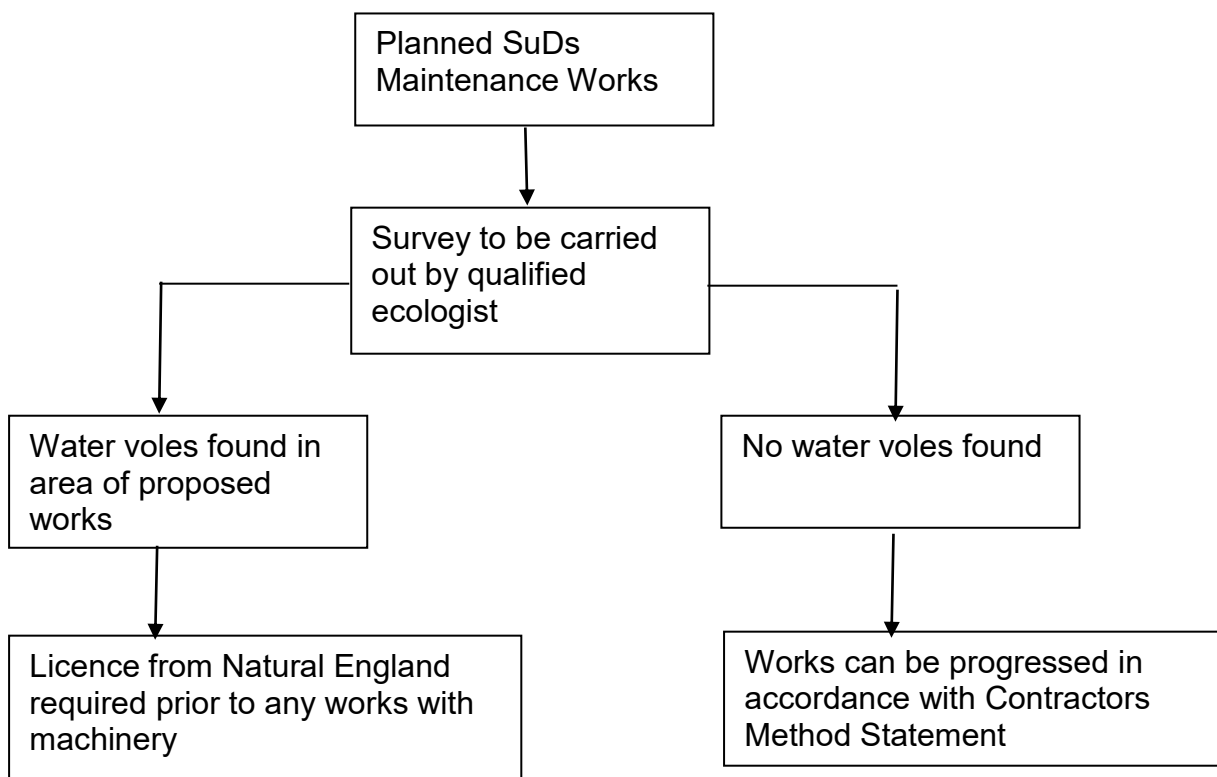
.

2) Operating and Maintenance Responsibility

Drew Smith Homes are responsible for maintaining the surface water drainage systems on this site during the construction period. A management company nominated by Drew Smith Homes which during the construction period will have DSM as the sole directors. Upon handover and occupation a Maintenance Company will be handed over to residents who will take over as Directors.

The Management Company will appoint a managing agent who will ensure that the SuDS are maintained as set out in this document. The maintenance and operation will be funded through contributions from the residents to the maintenance company.

As part of the maintenance responsibility of the SuDS and drainage system, it is important that all future maintenance works consider the presence of water voles and other ecological sensitive receptors. As such prior to any intrusive maintenance works (which includes the use of heavy machinery where soils/ground is disturbed) to the new swales, ditches and basins an ecological survey should be carried out to determine the proposed method statements and if any licences are required ahead of the works. A simple flow chart has been provided below to describe the approach which needs to be considered:



3) Maintenance Schedule for catchpits, control chambers, flow control devices and gullies

Flow Control Maintenance

Normally, little maintenance is required as there are no moving parts within the Flow Control. The Flow Control is fitted with pivoting by-pass door, which allows the manhole to be drained down should blockage occur. It is recommended that the unit be inspected at six monthly intervals with hose down if required. All flow controls are typically manufactured from grade 304 Stainless Steel which has an estimated life span in excess of the design life of drainage systems.

Maintenance Schedule	Required Action	Recommended Frequency
Regular maintenance	Inspect and identify any areas that are not operating correctly. If required, take remedial action.	Monthly for 3 months, then six monthly
	Debris removal from catchment surface (where may cause risks to performance)	Monthly
	Remove sediment and oil deposits from all trapped gullies.	Annually, or as required.
	Remove sediment from structures upstream of the cellular storage tanks.	Annually, or as required.
Remedial actions	Repair/rehabilitation of inlets, outlets, overflows and vents.	As required
Monitoring	Inspect/check all inlets, outlets, vents and overflows to ensure that they are in good condition and operating as designed.	Annually and after large storms

4) Maintenance Schedule for Permeable Paving and Distribution Tanks

Maintenance Schedule	Required Action	Frequency
Regular maintenance	Brushing & vacuuming	Three times/year at end of winter, mid-summer, after autumn leaf fall, or as required based on site-specific observations of clogging or manufacturers' recommendations.
Occasional maintenance	Stabilise and mow contributing and adjacent areas.	As required.
	Removal of weed.	As required.
Remedial Actions	Remediate any landscaping which, through vegetation maintenance or soil slip, has been raised to within 50mm of the level of the paving.	As required.
	Remedial work to any depression's, rutting and cracked or broken blocks considered detrimental to the structural performance or a hazard to users.	As required.
	Rehabilitation of surface and upper sub-structure.	As required (if infiltration performance is reduced as a result of significant clogging).
Monitoring	Initial Inspection	Monthly for 3 months after installation.
	Inspect for evidence of poor operation and/or weed growth.	3-monthly, 48h after large storms.
	If required take remedial action.	
	Inspect silt accumulation rates and establish appropriate brushing frequencies.	Annually.
	Monitor inspection chambers.	Annually.

5) Maintenance Schedule for Attenuation basins , bio-retention areas and swales

Maintenance Schedule	Required Action	Recommended Frequency
Regular maintenance	Litter and debris removal.	Monthly
	Grass cutting – for spillways and access routes.	Monthly (during growing season), or as required.
	Grass cutting – meadow grass in and around basin. Ensure that the meadow grass is not cut lower than 10cm. No vehicle should track within 3-5m of the toe of the bank	50% of the area annually during late autumn period (eg 1 side/bank of the system each year or 50% in area terms spread out amongst the system). Adjust as required should any survey show Water voles are present.
	Manage other vegetation and remove nuisance plants.	Monthly (at start, then as required).
	Tidy all dead growth before start of growing season.	Annually.
	Remove sediment from inlets, outlet and forebay.	Annually (or as required).
Occasional maintenance	Check for poor vegetation growth due to lack of sunlight or leaf dropping litter and cut back adjacent vegetation where possible/	Annually
	Re-seed areas of poor vegetation growth. Alter plant types to better suit conditions, if required	Annually, or if bare soil is exposed over 10% or more of the basin/swale treatment area
	Prune and trim trees and remove cuttings.	2 years (or as required). Ensure this is undertaken outside of bird nesting season.

Remedial actions	Repair of erosion or other damage by re-turfing or reseeding.	As required
	Re-level uneven surfaces and reinstate design levels.	As required.
	Repair/rehabilitation of inlets, outlets and overflows.	As required.
	Remove and dispose of oils or petrol residues using safe standard practices	As required
Monitoring	Inspect inlets, outlets and overflows for blockages, and clear if required.	Monthly/ after large storms.
	Inspect banksides, structures, pipework etc. for evidence of physical damage.	Monthly/ after large storms.
	Inspect inlets and facility surface for silt accumulation. Establish appropriate silt removal frequencies.	Half yearly.
	Check flow control device and other mechanical devices.	Half yearly.

6) Maintenance Schedule for Filter trenches and porous pipework

Maintenance Schedule	Required Action	Recommended Frequency
Regular maintenance	Litter and debris removal from trench surface, access chambers and pre-treatment devices.	Monthly (or as required).
	Removal and washing of exposed stones on the trench surface.	Annual (bi-annual the first year) or when silt is evident on the surface.
	Trimming of any roots that may be causing blockages.	Annual (semi-annual the first year).
	Remove weeds on the trench surface.	Monthly (at start, then as required).
Occasional maintenance	Removal of sediment from pre-treatment devices.	Six monthly
	Remove tree roots or trees that grow close to the trench.	As required.
	At locations with high pollution loads, remove surface geotextile and replace, and wash or replace filter media.	Five yearly.
Remedial actions	Clear perforated pipework of blockages.	As required.
	Rehabilitate infiltration or filtration surfaces.	As required.
	Replace geotextiles and clean and replace filter media, if clogging occurs.	As required.
	Inspect inlets, outlets and inspection points for blockages, clogging, standing water and structural damage.	As required.
Monitoring	Inspect pre-treatment systems, inlets, trench surfaces and perforated pipework for silt accumulation. Establish appropriate silt removal frequencies.	Half yearly.

7) Maintenance Schedule for Grilles

Maintenance Schedule	Required Action	Recommended Frequency
Regular maintenance	Litter and debris removal.	Monthly (or as required).
Occasional maintenance	Check moving parts and locks. Oil and ensure free moving. Replace when necessary.	As required.
Remedial actions	Remove build-up of sediment.	As required.
Monitoring	Inspect for blockages, and clear if required.	Monthly
	Inspect inlets and facility surface for silt accumulation. Establish appropriate silt removal frequencies.	Half yearly.

8) Maintenance Schedule for solid wall pipes

Maintenance Schedule	Required Action	Recommended Frequency
Regular maintenance	Inspect and identify any areas that are not operating correctly. If required, take remedial action.	Monthly for 3 months, then six monthly.
	Debris removal from catchment surface (where may cause risks to performance)	Monthly
	Inspect chambers and manholes for evidence of pipes operating correctly and take remedial action if necessary, to include jetting of pipework.	Monthly for 3 months, then annually

9) Reasons for Maintenance

Surface water contains variable amounts of sediment which settles out at certain locations and could cause blockages if left. Road gullies also trap oil and prevent it entering the surface water sewer system.